



## TESTING AND DIAGNOSTIC OUT OF THE SERVICE POWER TRANSFORMER USING A SWEEP FREQUENCY RESPONSE ANALYSIS (SFRA) COMPARING WITH CHINA STANDARD

Salim DJERIOU<sup>1,2,\*</sup> , Riyadh ROUABHI<sup>1</sup> , Ilies AYAD<sup>1</sup> ,  
Mohamed BOUCHAHDANE<sup>3</sup> , Mounir DIF<sup>3</sup> 

<sup>1</sup> Laboratory of Electrical Engineering LGE, University of M'sila, Algeria

<sup>2</sup> Department of Electrical Engineering, Faculty of Technology, University of M'sila, Algeria

<sup>3</sup> Institute of Electrical and Electronic Engineering, University M'hamed Bougara, Boumerdes, Algeria

\* Corresponding author, e-mail: [salim.djeriou@univ-msila.dz](mailto:salim.djeriou@univ-msila.dz)

### Abstract

A several diagnostic methods used to evaluate and detect any potential issues or faults in the transformer before they cause significant problems. The research proposal focuses on employing the SFRA (Sweep Frequency Response Analysis) technique, renowned for its exceptional sensitivity and diagnostic capabilities. This method serves to identify the mechanical integrity of the transformer's core, winding distortion, and clamping structures by analyzing their electrical transfer functions across a broad frequency spectrum. By utilizing SFRA, the study aims to accurately predict the internal physical condition of the transformer, making it a highly effective and reliable indicator for assessing its overall health. The motivation of this present work is using all experiments of SFRA were conducted and validated on a three-phase 30kV/0.4KV voltage transformer with 50kVA at the laboratory of Msila university. The result of these experiments is presented and discussed in terms of interpretation the analyses based on different standards.

Keywords: power transformer; diagnostics; sweep frequency response analysis (SFRA)

## 1. INTRODUCTION

Electrical transformers are one of the most important parts of the electrical system because of their significant role in increasing the reliability of the electrical grid and the durability of the power supply. The power transformer is an essential element of an electrical power system because it regulates the voltage level to set the best possible system operation [1]. In order to ensure a long, useful service life, it is critical that a power transformer and its ancillary components are tested regularly for incipient fault modes. Sweep Frequency Response Analysis (SFRA) test is considered one of the tests that are relied upon to detect deformations that occur in transformer windings those that are difficult to detect by traditional tests such as the Turns Ratio test, Winding Resistance test, or Excitation current test. Furthermore, The SFRA methods are founded on comparing the characteristics of power transformers before and after the test [2]. Each of these tests has a set of advantages and disadvantages that distinguish it from the others[3].In some cases, any failure of these transformers will result in the

system's failure as a whole [4].The SFRA test offers highly potent diagnostic capabilities.

However, to derive true value from the tests, two critical aspects must be carefully considered: first, the proper application of the test must adhere to acceptable standards, ensuring its accuracy and reliability. Second, the interpretation of the test results requires meticulous attention to detail, allowing for meaningful insights to be extracted from the gathered data. By addressing both these aspects diligently, the SFRA test can deliver valuable and insightful information[5],[6].

In case of a mechanical change in the coils or iron core, the system of resistances, inductances, and capacitances of the transformer will differ according to a specific pattern depending on the type of fault, which is reflected in the result of this test and indicates the presence of this type of faults, where the frequency response is indicative of the compounds that make up the transformer system and any difference in these compounds will affect this frequency response [7],[8]. In this test (SFRA), a low-voltage wave with a variable frequency is applied to one end of the coil, and this wave is

measured at the other end of the same coil or another coil according to the adopted test pattern.

The interpretation of SFRA results is performed by visualization of images obtained using specialized devices [8]. In our case, the distribution transformer of rating 50 kV A, 30V/0.4KV, three phase, 50 Hz has been specially used in laboratory of Msila university by the authors and his team for carrying out SFRA testing by practically using FRAX101 instrument of megger company to detect winding displacements in power transformers or faults in the magnetic core.

The main work of this research is the detection of winding deformations and to extend the guideline approach for analysis and interpretation of results based by visualization of images on experiences according to China standards.

## 2. EXPERIMENTAL WORK

The laboratory, as depicted in Fig. 1, is dedicated to the design and development of a specialized 50 kVA power transformer. This transformer serves as the subject of study for analyzing SFRA (Sweep Frequency Response Analysis) using FRAX101 traces through practical testing. The hardware of the SFRA system is meticulously engineered to identify winding displacements and potential faults in the magnetic core of power transformers.

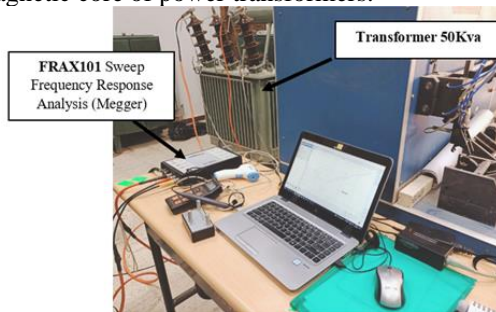


Fig. 1. Details of experiment materials using FRAX101 in the lab

In the philosophy of testing, a voltage wave is applied to one of the transformer coils, where this wave is a small amplitude sinusoidal wave (2-15V) and variable frequency (from 20 Hz to 2 MHz) [9],[10], [11], according to the standards of the International Electrotechnical Commission [12]. Then, this applied voltage is measured to serve as a reference wave, and the output voltage is measured to be the response wave as shown in Fig. 2, which illustrates a transformer testing circuit using coaxial cables.

With the help of the model's function, one can compute nearly any parameter by utilizing the measured or stored data [12].

### 2.1. Characteristics of power transformer

In the absence of the transformer's fingerprint (time based), the study will be based on a comparison between the three phases, which is one

of the methods relied upon in the absence of the fingerprint (time based), taking into account some differences in the location of the files in the iron core. The table 1 shows the transformer's characteristics for testing.

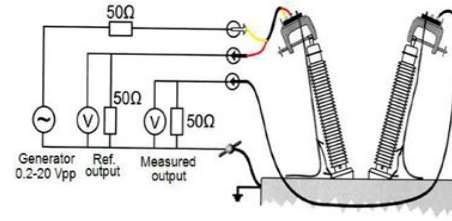


Fig. 2. SFRA test connection using FRAX 101

Table 1. Transformer characteristics

Company	ENEL Azazga-tizi-Algeria
Transformer type	4746C
Number	03525
Years of manufacture	1987
Power capacity	50 kVA
Rating power HV/LV	30 kV /400 V
Frequency	50 Hz
Vector group	Yzn11
Type of cooling	ONAN

### 2.2. Analysis of transformer by SFRA method

There are several connections between the test device and the transformer to be tested through which this test can be performed according to the adopted method. Referring to international standards issued by renowned organizations such as the International Council on Large Electric Power Systems (CIGRE) [13], the International Electrotechnical Commission (IEC) [14], and the Institute of Electrical and Electronics Engineers (IEEE) [15].

Before commencing the test, the FRAX101 device provides the feature of verifying the device's functionality and connection cables. The verification method as shown in Fig.3. and the result should match what is described in the device's user manual [16].



Fig. 3. The connection method of verification test

### 2.3 Type of measurement

In this part, various tests have been used to distribution transformer according to the four typical of the SFRA method:

**1. End-to-end open circuit**

In this experiment six tests have been achieved by connection method as show in Table 2 (Three in HV and three in LV).

Table 2. Connection method for end-to-end open circuit typical

Test type	Test number	Delta – Start
HV open circuit all other terminals floating	1	H <sub>1</sub> -H <sub>3</sub>
	2	H <sub>2</sub> -H <sub>1</sub>
	3	H <sub>3</sub> -H <sub>2</sub>
LV open circuit all other terminals floating	4	X <sub>1</sub> -X <sub>0</sub>
	5	X <sub>2</sub> -X <sub>0</sub>
	6	X <sub>3</sub> -X <sub>0</sub>

**Note:**

(H<sub>1</sub>- H<sub>2</sub>-H<sub>3</sub>): **HV phases**; (X<sub>1</sub>- X<sub>2</sub>- X<sub>3</sub>-X<sub>0</sub>): **LV phases**

Figures 4 and 5, show how the FRAX101 device clamps are connected to the transformer stages (H<sub>3</sub>-H<sub>2</sub>; X<sub>3</sub>-X<sub>0</sub>) In the same way the other tests are according to the table.

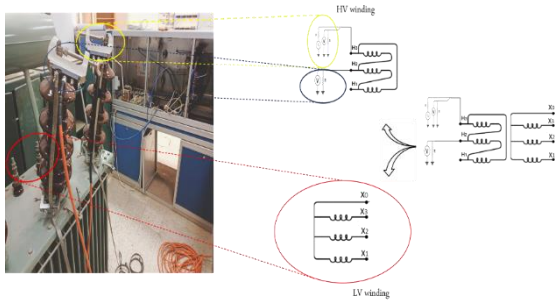


Fig. 4. HV open circuit (H<sub>3</sub>-H<sub>2</sub>) all other terminals floating

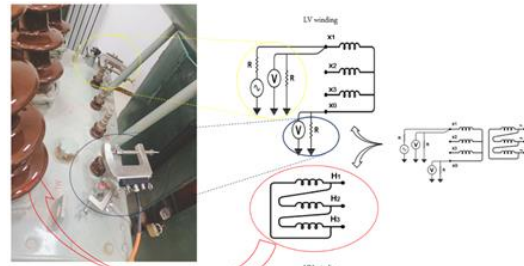


Fig. 5. LV open circuit (X<sub>3</sub>-X<sub>0</sub>) all other terminals floating

The results of the tests according the Table 2 are showing in Fig. 6 and 7.

**2. End-to-end short circuit**

In this test, three tests (generated and measured in HV, short[X<sub>1</sub>-X<sub>2</sub>-X<sub>3</sub>]) are implemented with a different connection as well as show in Table 3.

Table 3. Connection method for end-to-end short circuit typical

Test type	Test number	Delta – Start
End to end short circuit short[X <sub>1</sub> -X <sub>2</sub> -X <sub>3</sub> -X <sub>0</sub> ]	1	H <sub>1</sub> -H <sub>3</sub>
	2	H <sub>2</sub> -H <sub>1</sub>
	3	H <sub>3</sub> -H <sub>2</sub>

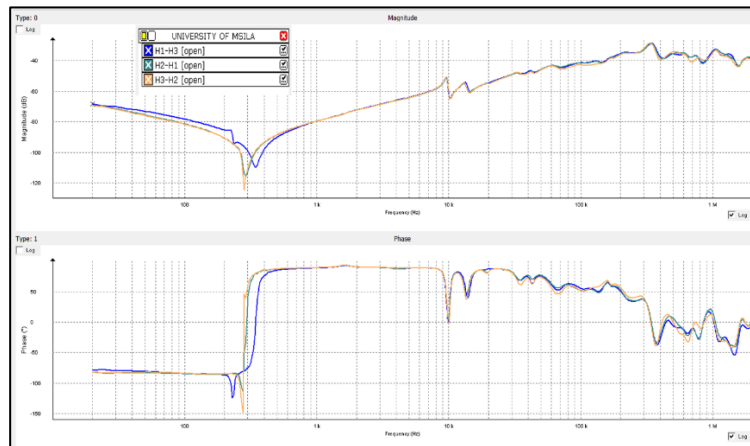


Fig. 6. Results of end-to-end open circuit typical (HV)

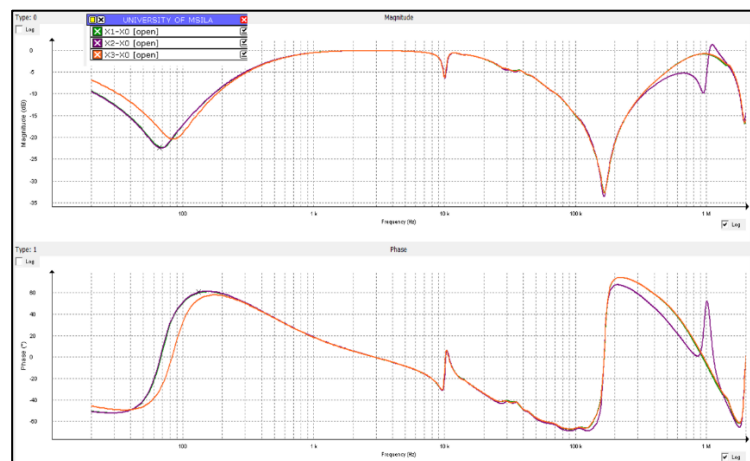


Fig. 7. Results of end-to-end open circuit typical (LV)

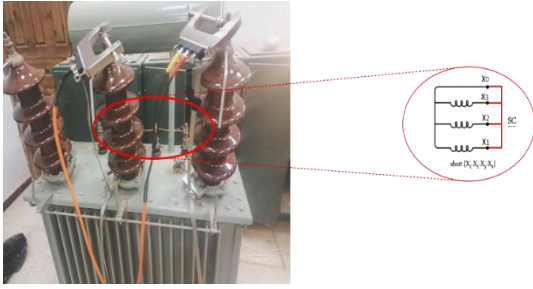


Fig. 8. Typical connection of end-to-end short circuit method (H3-H2)

The result of this test shown in Fig. 9 using Table 3.

**3. Capacitive Inter Winding**

Three tests (generated in HV and measured in LV), connection method as show in Table 4.

The Fig. 10 shows the experiment wiring of the capacitive inter winding test (H1-X1).

Table 4. Typical connection of capacitive inter winding method

Test type	Test number	Delta – Start
Capacitive inter winding all other terminals floating	1	H <sub>1</sub> -X <sub>1</sub>
	2	H <sub>2</sub> -X <sub>2</sub>
	3	H <sub>3</sub> -X <sub>3</sub>

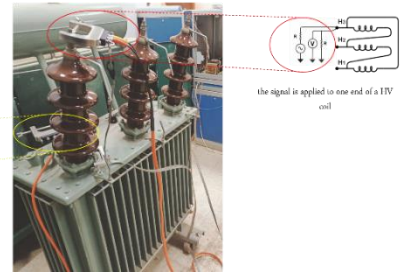


Fig. 10. One of the topicals connection of capacitive inter winding method

The result of this method is presented in Fig. 11.

**4. Inductive Inter Winding**

In this test, we apply three tests (generated in HV and measured in LV, with the other end of both windings being grounded), the connection method as show in Table 5.

Table 5. Typical connection of inductive inter winding method

Test type	Test number	Delta – Start
Inductive inter winding around [U-an-X]	1	H <sub>1</sub> -X <sub>1</sub>
	2	H <sub>2</sub> -X <sub>2</sub>
	3	H <sub>3</sub> -X <sub>3</sub>

The Fig. 12 shows an example of how perform this method.

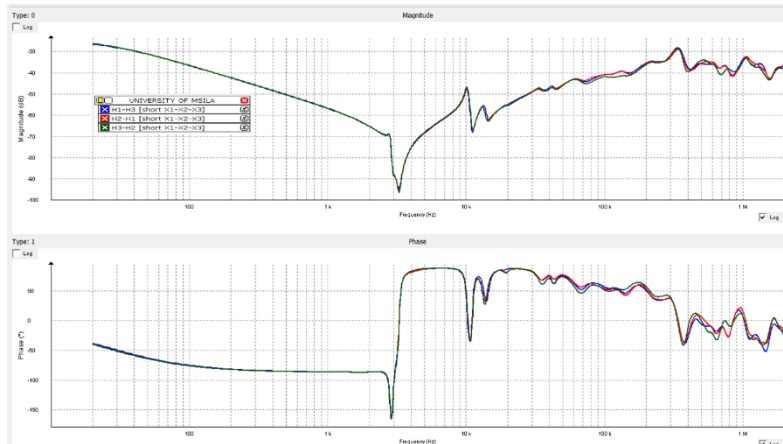


Fig. 9. Results of end-to-end short circuit typical

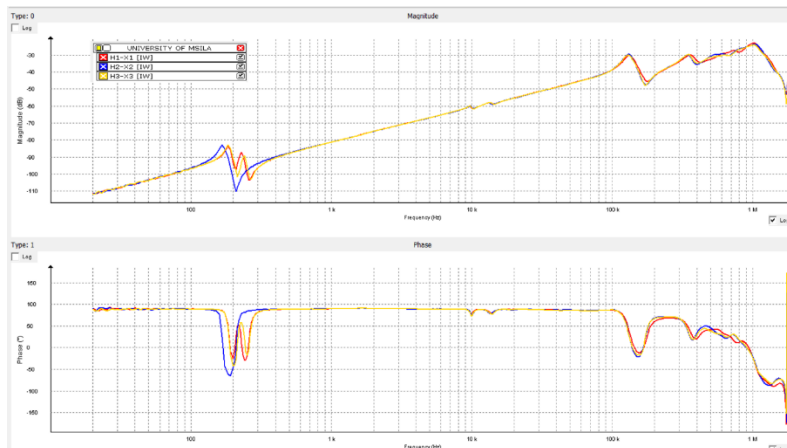


Fig. 11. Results of Capacitive inter winding typical



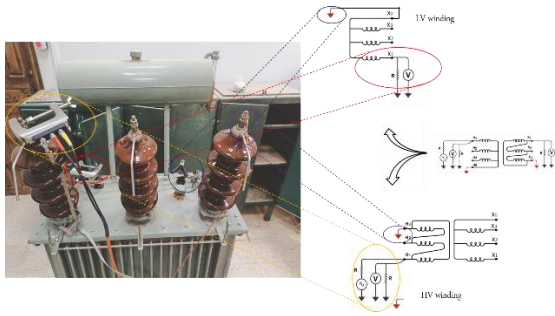


Fig. 12. One of the typical connections of inductive inter winding method (H1-X1)

The result of this typical method is showing in Fig. 13 using Table 5.

### 3. RESULTS AND DISCUSSION

The Chinese standard DL/T911-2004 technique, a pioneering standard globally, was created in China under the management of the Technology Commission for Electric Power Industry & High Voltage Test Technology Standardization. This standard emerged as a result of collaboration among six national power engineering institutes, with its exclusive focus on SFRA measurements. The standard encompasses the test principle, requirements for testing instruments, testing methods, and the analysis of results [17].

The frequency range evaluated by this standard is between 1 kHz and 1 MHz. This standard is unique in that it provides a rule for judging test results based on a calculation of covariances [18].

Table 6 provides a clear classification of winding deformation degrees based on specific relative

factors in different frequency bands, facilitating understanding and analysis.

Table 6. Relation between relative Factors and degree of transformer winding deformation

Winding Deformation degree	Relative Factors R
Severe Deformation	$R_{LF} < 0.6$
Obvious Deformation	$1.0 > R_{LF} \geq 0.6$ or $R_{MF} < 0.6$
Slight Deformation	$2.0 > R_{LF} \geq 1.0$ or $0.6 \leq R_{MF} < 1.0$
Normal Deformation	$R_{LF} \geq 2.0, R_{MF} \geq 1.0$ and $R_{HF} \geq 0.6$

Note:

$R_{LF}$  represents the relative factor when the curve is in low frequency band (1kHz~100kHz).

$R_{MF}$  represents the relative factor when the curve is in medium frequency band (100kHz~600kHz).

$R_{HF}$  represents the relative factor when the curve is in high frequency band (600kHz~1000kHz).

The terms "normal, Severe, Obvious, Slight " indicates of degree of transformer winding deformation based on relative Factors R

According the Chinese standard DL/T911-2004 technique, this work has been compered all results of curves between the results obtained in previous section and the limits curves of this standard for every typical wiring method, The results and interpretations as a recap in a Table is presented for every method of SFRA application as follow:

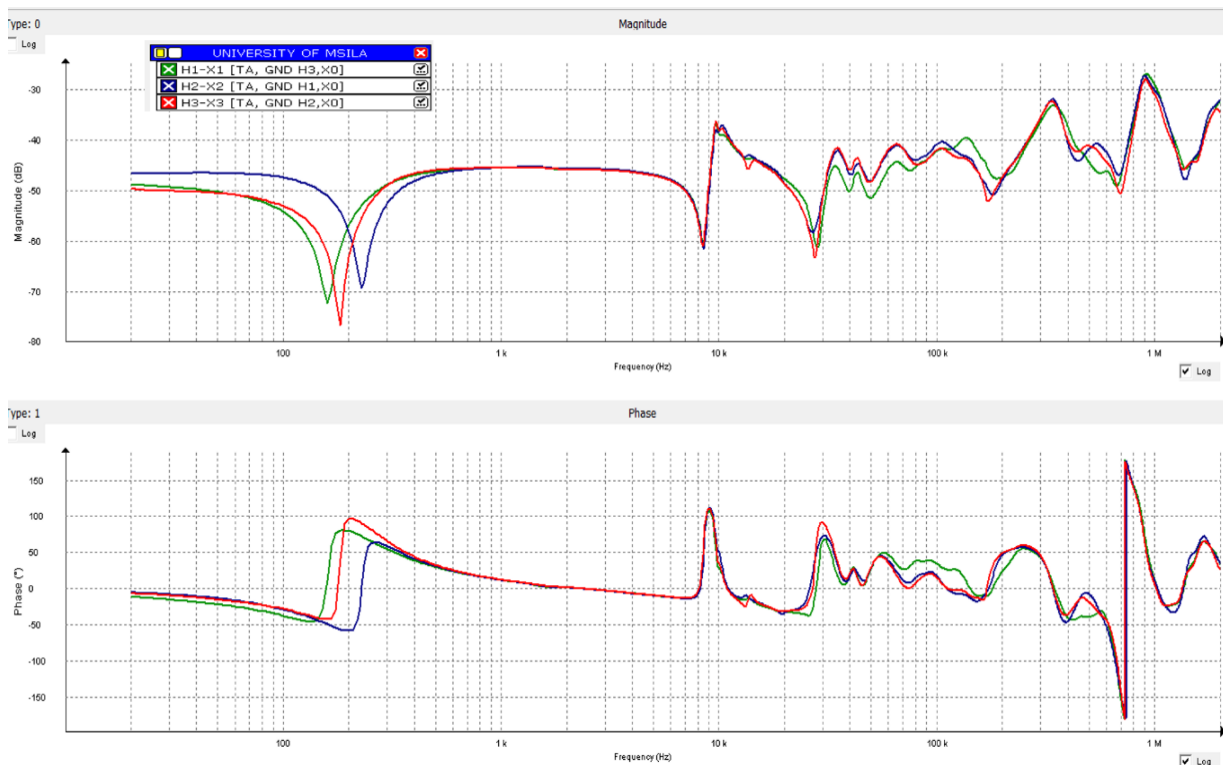


Fig. 13. Results of Inductive inter winding typical

**1. End-to-end open circuit**

The figures (14,15,16) represent the comparison of each pair of curves, where it has three curves related to high-voltage phases as illustrated in Table 2. In general, the comparisons indicate the normal state of the windings and iron core, because End-to-end open circuit method focuses on looking at the winding and core characteristics).

The comparison all of curves, three curves related to low-voltage phases shown in figures (17, 18, 19) and indicate the normal state of the windings and iron core.

Table 7 summarizes the results of curves comparison for end-to-end open circuits, highlighting the interpretation based on the relevant

standards and concluding whether conditions are normal.

**2. End-to-end short circuit**

The End-to-end short circuit method focuses on the winding’s characteristics, the figures (20, 21, 22) represent the comparison of each pair of curves related to high-voltage phases as illustrated in Table 3. **However, the comparisons indicate the normal state of the windings**

In the table 8, the comparison of curves [H1-H3[short X1-X2-X3]] to [H2-H1[short X1-X2-X3]] indicates normal operation. The curves [H2-H1[short X1-X2-X3]] to [H3-H2[short X1-X2-X3]] show high-frequency resistance (R-HF) above the limit, while low-frequency (R-LF) and medium-

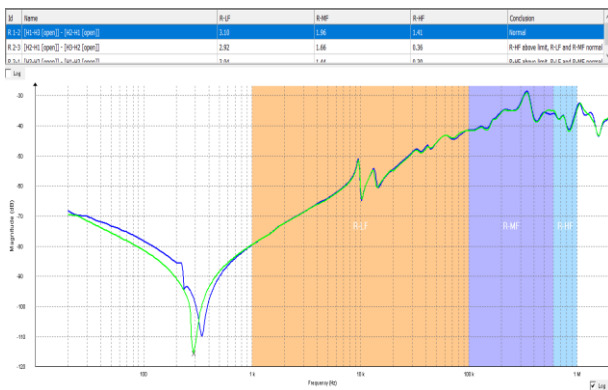


Fig. 14. Result of curves comparison [H1-H3[open]]- [H2-H1[open]]

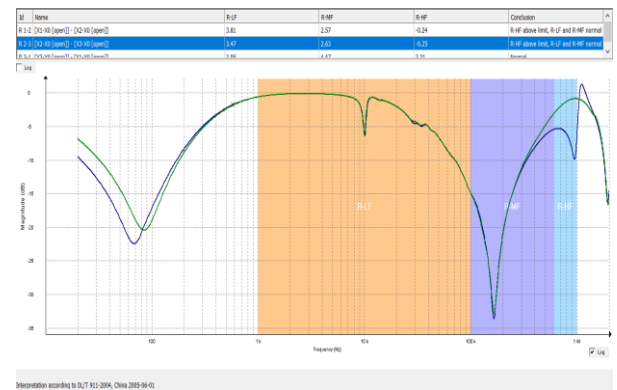


Fig. 17. Result of curves comparison [X1-X0[open]]- [X2-X0[open]]

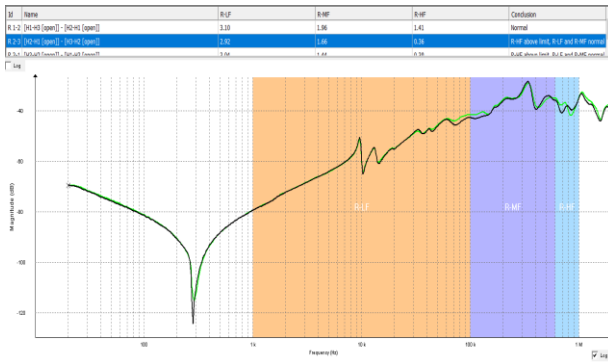


Fig. 15. Result of curves comparison [H2-H1[open]]- [H3-H2[open]]

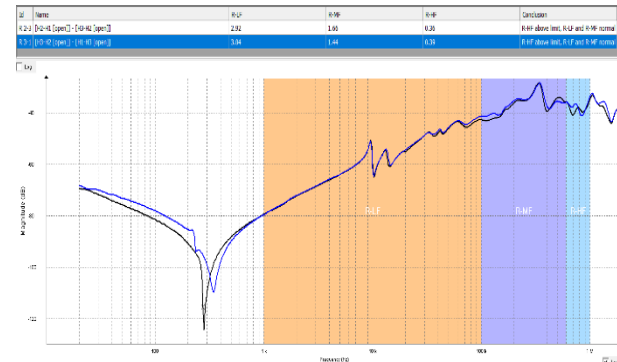


Fig. 18. Result of curves comparison [X2-X0[open]]- [X3-X0[open]]

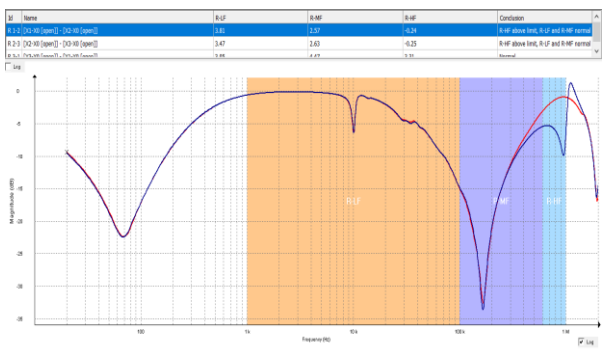


Fig.16. Result of curves comparison [H3-H2[open]]- [H1-H3[open]]

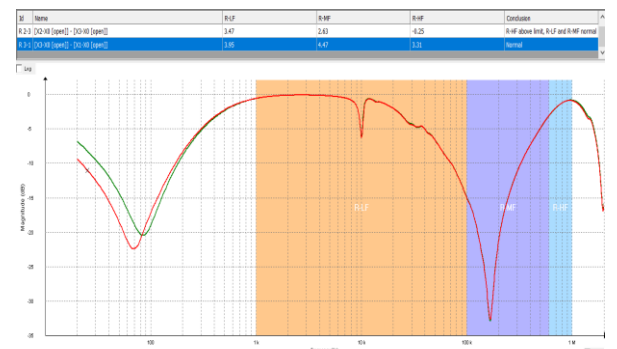


Fig. 19. Result of curves comparison [X3-X0[open]]- [X1-X0[open]]

Table 7. Result of curves comparison end-to-end open circuit typical (HV)

Interpretation according to DL/T 911-2004, China 2005-06-01	
Curves comparison	Conclusion
[H1-H3[open]]- [H2-H1[open]]	Normal
[H2-H1[open]]- [H3-H2[open]]	<b>R-HF above limit, R-LF and R-MF normal</b>
[H3-H2[open]]- [H1-H3[open]]	<b>R-HF above limit, R-LF and R-MF normal</b>
[X1-X0[open]]- [X2-X0[open]]	<b>R-HF above limit, R-LF and R-MF normal</b>
[X2-X0[open]]- [X3-X0[open]]	<b>R-HF above limit, R-LF and R-MF normal</b>
[X3-X0[open]]- [X1-X0[open]]	Normal

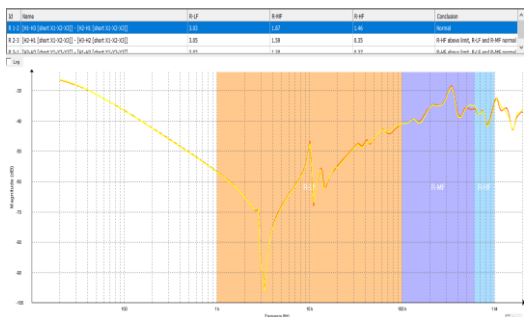


Fig. 20. Result of curves comparison [X3-X0[open]]- [X1-X0[open]]

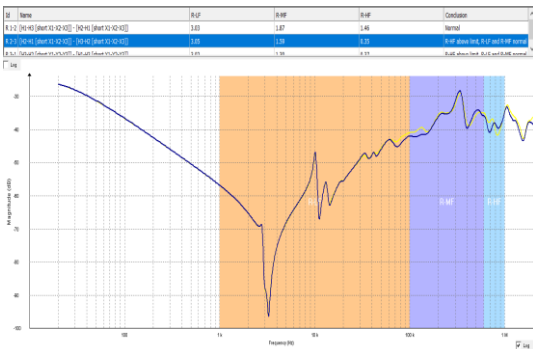


Fig. 21. Result of curves comparison [X3-X0[open]]- [X1-X0[open]]

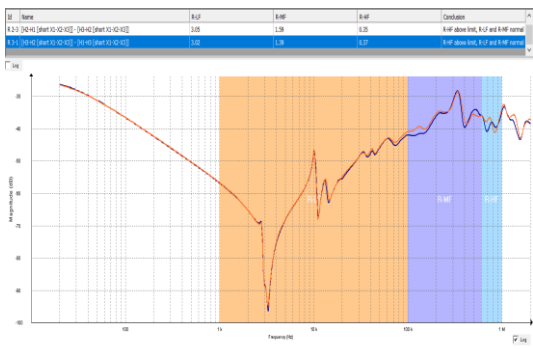


Fig. 22. Result of curves comparison [X3-X0[open]]- [X1-X0[open]]

frequency (R-MF) resistances are within normal limits. In addition, the curves [H3-H2[short X1-X2-X3]] to [H1-H3[short X1-X2-X3]] indicates high-

frequency resistance (R-HF) above the limit, but low-frequency (R-LF) and medium-frequency (R-MF) resistances are within normal limits.

Table 8. Result of curves comparison (end-to-end short circuit typical)

Interpretation according to DL/T 911-2004, China 2005-06-01	
Curves comparison	conclusion
[H1-H3[short X1-X2-X3]]- [H2-H1[short X1-X2-X3]]	Normal
[H2-H1[short X1-X2-X3]]- [H3-H2[short X1-X2-X3]]	<b>R-HF above limit, R-LF and R-MF normal</b>
[H3-H2[short X1-X2-X3]]- [H1-H3[short X1-X2-X3]]	<b>R-HF above limit, R-LF and R-MF normal</b>

### 3. Capacitive inter winding

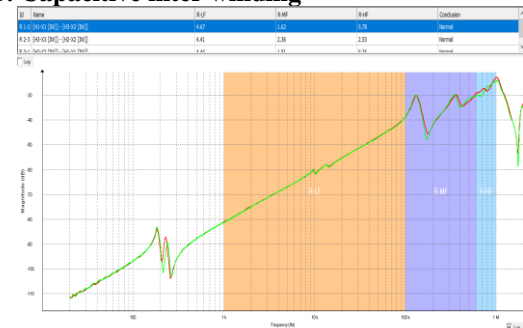


Fig. 23. Result of curves comparison [H1-X1[IW]]- [H3-X3[IW]]

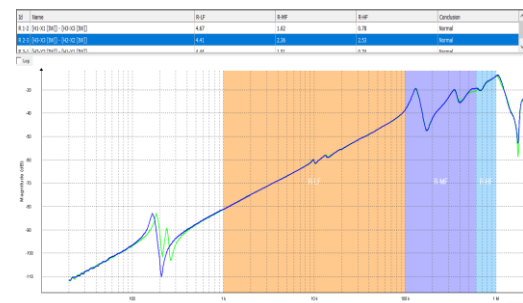


Fig. 24. Result of curves comparison [H3-X3[IW]]- [H2-X2[IW]]

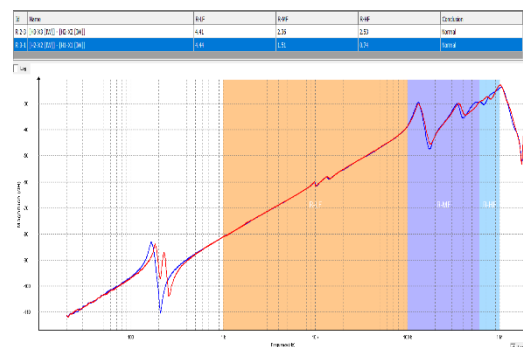


Fig. 25. Result of curves comparison [H2-X2[IW]]- [H1-X1[IW]]

The high-voltage phases as illustrated in Table 4 presented in figures (23, 24, 25). The comparisons

test as shown in Table 9 indicate the normal state of the windings because the capacitive inter-winding method has high sensitivity in detecting radial/diameter deformations in the windings).

Table 9. Result of curves comparison (Capacitive inter winding)

Interpretation according to DL/T 911-2004, China 2005-06-01		
Curves comparison	Conclusion	
[H1-X1[IW]]- [H3-X3[IW]]	Normal	
[H3-X3[IW]]- [H2-X2[IW]]	Normal	
[H2-X2[IW]]- [H1-X1[IW]]	Normal	

4. Inductive inter winding

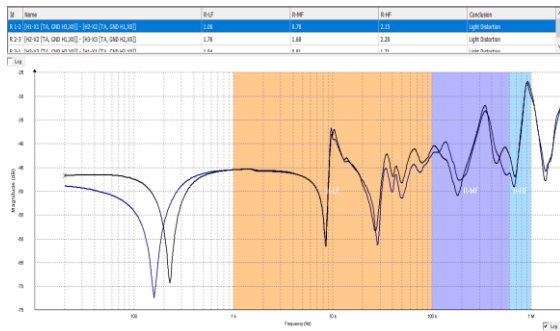


Fig. 26. Result of curves comparison [H1-X1[TA, GND H3, H0]]- [H2-X2[TA, GND H1, H0]]

The low-voltage phases test appears in figures (26,27,28) as illustrated in Table 5. It is clear a light distortion in all curves comparison as well as presented in Table 10. To ensure an optimal analysis of test results, it is necessary to consider certain factors when comparing current results with those of the same or similar transformers, or when comparing different phases, as outlined in the standard.

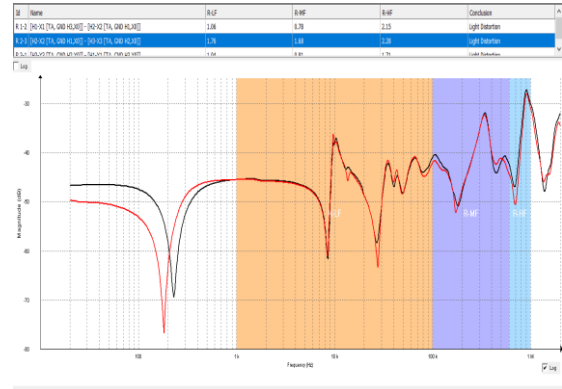


Fig. 27. Result of curves comparison [H2-X2[TA, GND H1, H0]]- [H3-X3[TA, GND H2, H0]]

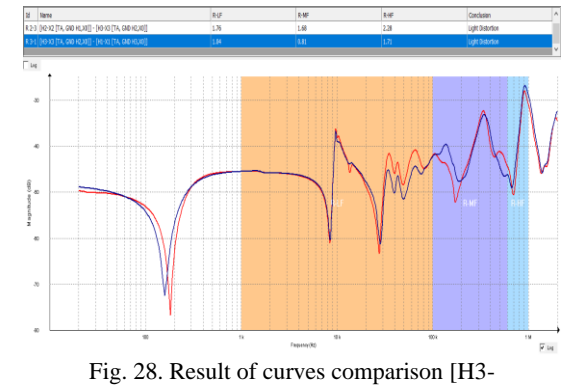


Fig. 28. Result of curves comparison [H3-X3[TA, GND H2, H0]]- [H1-X1[TA, GND H3, H0]]

Table 10. Result of curves comparison (Inductive inter winding)

Interpretation according to DL/T 911-2004, China 2005-06-01		
Curves comparison	conclusion	
[H1-X1[TA, GND H3, H0]]- [H2-X2[TA, GND H1, H0]]	Light Distorsion	
[H2-X2[TA, GND H1, H0]]- [H3-X3[TA, GND H2, H0]]	Light Distorsion	
[H3-X3[TA, GND H2, H0]]- [H1-X1[TA, GND H3, H0]]	Light Distorsion	

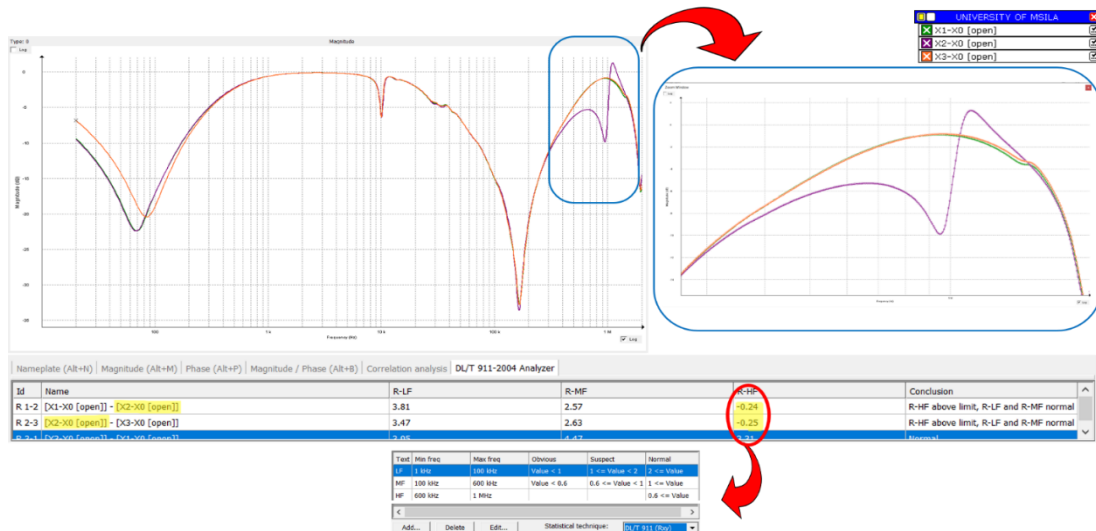


Fig. 29. Analysis of results



## 5. Occurrence of displacement of the waveform

The Fig. 29 indicates the difference in the fingerprint of phase X2-X0 compared to the rest of the phases X1-X0 and X3-X0 in the high-frequency range (end to end open circuit injection in LV)

## 4. CONCLUSION

Experimental testing of the transformer which has been out of the service more than to 7 years, allowed us to conclude that the internal mechanical condition not changed and has a perfect analysis. Upon comparing the frequency responses with the Chinese standard, it has been observed that the open and short circuit responses of the three phases of HV (H) and LV (X) windings exhibit similarities and possess identical shapes in the low and medium frequency ranges, resembling the behavior of two phases. However, further analysis is needed to explore additional aspects, it has abnormal status for last(H) and (X)phase, as analysis, it is greatly affected by the connection of the test, especially the connection of coaxial cables used in the test to the ground and it is greatly affected by the structure of the windings, which take the form of sequential leakages and capacitances in series and in parallel. On the other hand, the capacitive and inductive inter winding are similar with respect to detecting both winding-ground and winding-interlayer short circuits.

**Source of funding:** *This research received no external funding.*

**Author contributions:** *research concept and design, S.D., R.R., I.A., M.B., M.D; Collection and/or assembly of data, R.R., I.A., M.B., M.D; Data analysis and interpretation, S.D., R.R., I.A., M.B., M.D; Writing the article, S.D., R.R., I.A., M.B., M.D; Critical revision of the article, R.R., I.A., M.B., M.D; Final approval of the article, R.R., I.A., M.B., M.D.*

**Declaration of competing interest:** *The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.*

## REFERENCES

- Ibrahim KH, Korany NR, Saleh SM. Effects of power transformer high-frequency equivalent circuit parameters non-uniformity on fault diagnosis using SFRA test. *Ain Shams Engineering Journal* 2022; 13(4): 101674. <https://doi.org/10.1016/j.asej.2021.101674>.
- Almehdhar A, Prochazka R, Vanis M. Application of SFRA method for evaluation of short-circuit tests of power transformers. 2022 International Conference on Diagnostics in Electrical Engineering (Diagnostika).
- Islam MM, Lee G, Hettiwatte S. A review of condition monitoring techniques and diagnostic tests for lifetime estimation of power transformers. *Electrical Engineering* 2018; 100: 1–25. <https://doi.org/10.1007/s00202-017-0532-4>.
- Yang Q, Su P, Chen Y. Comparison of Impulse Wave and Sweep Frequency Response Analysis Methods for Diagnosis of Transformer Winding Faults. *Energies* 2017; 10(4): 431. <https://doi.org/10.3390/en10040431>.
- Murugan R, Raju R. Evaluation of in-service power transformer health condition for Inspection, Repair, and Replacement (IRR) maintenance planning in electric utilities. *International Journal of System Assurance Engineering and Management* 2021; 12. <https://doi.org/10.1007/s13198-021-01083-1>.
- Elanien AA. Asset management techniques for transformers. *Electric Power Systems Research* 2010; 80(4): 456-464.
- Secue J, Mombello E. Sweep frequency response analysis (SFRA) for the assessment of winding displacements and deformation in power transformers. *Electric Power Systems Research* 2008; 78: 1119–28. <https://doi.org/10.1016/j.eprsr.2007.08.005>.
- Bjelić M, Brković B, Žarković M, Miljković T. Fault detection in a power transformer based on reverberation time. *International Journal of Electrical Power & Energy Systems* 2022; 137: 107825. <https://doi.org/10.1016/j.ijepes.2021.107825>.
- Khanali M, Hayati-Soloot A, Høidalen HK, Jayaram S. Study on locating transformer internal faults using sweep frequency response analysis. *Electric Power Systems Research* 2017; 145: 55–62. <https://doi.org/10.1016/j.eprsr.2016.11.016>.
- Al Murawwi E, Mardiana R, Su C. Effects of Terminal Connections on Sweep Frequency Response Analysis of Transformers. *IEEE Electrical Insulation Magazine - IEEE ELECTR INSUL MAGAZINE* 2012; 28: 8–13. <https://doi.org/10.1109/MEI.2012.6192362>.
- Gouda O, El-Hoshy S, Salem S. Diagnostic Techniques used in Power Transformer Turn to Turn Faults Identification Based on Sweep Frequency Response Analysis (SFRA). 2016. <https://doi.org/10.1109/MEPCON.2016.7836880>.
- Kaplin AI, Liberman MYu. New International Electrotechnical Commission standards for regulating acoustic noise and vibration of electric machines. *Russian Electrical Engineering* 2009; 80(5): 268–72. <https://doi.org/10.3103/S1068371209050071>.
- Kraetge, A. Aspects of the practical application of sweep frequency response analysis (SFRA) on power transformers. *Cigre 6th Southern Africa Regional Conference, 2009*.
- Cigré W. Mechanical condition assessment of transformer windings using Frequency Response Analysis (FRA). *Electra* 2008; 228.
- IEC 60076 – 18 Ed.1: Power Transformer Part – 18. Measurement of Frequency Response, United Kingdom. July 2012.
- IEEE PC 57.149 Guide for the Application and Interpretation of Frequency Response Analysis for Oil Immersed Transformer. March 2013.
- FRAX 101 Series Sweep Frequency Response Analysers User Manual.
- Kraetge A, Kruger M, Fong P. Frequency response analysis — status of the worldwide standardization activities. 2008 International Conference on Condition Monitoring and Diagnosis 2008:651–4. <https://doi.org/10.1109/CMD.2008.4580370>.



### Salim DJERIOU

was born and raised in ALGERIA, He received his electrical Engineer in Electrical Engineering Department, M'sila University (2003-2008) and The Magister degree in the field of electrical machines, Setif University (2008-2011). He received his PHD degree in electrical engineering and

electronics from Signals and systems laboratory, IGEE ex INELEC, University of Boumerdes (2011-2018). He has been working as a lecturer Professor in the Department of Electrical Engineering at M'sila University since 2018. His scientific interests are Electrical engineering, Renewable energy systems, Power System Analysis and power System Protection. He is member of several research projects at University of Msila.

E-mail address: [salim.djeriou@univ-msila.dz](mailto:salim.djeriou@univ-msila.dz)

University of Boumerdes, Algeria in 2013. Since 2021, he has been a Full Professor with the University of Boumerdes. His areas of research are in power system protection and power system testing and diagnostics.

E-mail: [bouchahdanelec@yahoo.fr](mailto:bouchahdanelec@yahoo.fr)



### Dr. Riyadh ROUABHI

works in the Department of Electrical Engineering at M'sila University. Obtained the Ph.D. Degree in electrical engineering from University of Batna, Algeria in 2016. His current research area includes the control of induction machines and renewable energy.

E-mail:

[riyadh.rouabhi@univ-msila.dz](mailto:riyadh.rouabhi@univ-msila.dz)



### Ilies AYAD

is originally from Algeria and completed his Bachelor's degree in Renewable Energies in Electrotechnical at the University Mohamed Kheider in Biskra, Algeria, spanning from 2018 to 2021. Subsequently, he pursued a Magister degree in electrical networks at M'Sila, Algeria, between 2021 and 2023. His

professional interests lie in the testing and diagnostic equipment related to electrical power.

E-mail: [iliesayad34@gmail.com](mailto:iliesayad34@gmail.com)



### Mohammed BOUCHAHDANE

was born in Chelghoum laid, Algeria in 1985. He received a B.S., M.S. and PhD in Electrotechnics from the Department of Electrotechnics of Constantine University, Algeria, respectively in 2007, 2009 and 2013. He was awarded a scholarship from 2010-2013 provided by the

African Union assistance program for the best African PhD students: MWALIMU NYERERE AFRICAN UNION SCHOLARSHIP. Recently, Dr. Bouchahdane was a Fulbright Scholar at The University of Tennessee at Chattanooga (USA) from 2019-2021. He joined the Institute of Electrical and Electronics Engineering at the