

Influence of Grain Size and Feed Rate on Selected Aspects of Corundum Ceramic Grinding Using Spherical Diamond Heads

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ABSTRACT

The article presents the results of experimental research on the grinding of corundum ceramics in the pre-sintered state, with spherical diamond heads. The aim of the experiment was to determine the effect of grain size and feed rate on selected aspects of the grinding process of corundum ceramics with the use of spherical diamond heads. In the experiment, grinding wheels with a ball diameter of 3 mm and different grain sizes were used; the grain numbers were D64, D91, D126 and D181. The tests were carried out on the Ultrasonic 20 Linear machining center at a constant rotational rate of the grinding wheel $n = 38,000$ rpm and a grinding depth of 30 μm . The feed rate was set on 3 values: 200, 400 and 600 mm / min. During the research, the process temperature was recorded with a thermal imaging camera. The topography of grinding wheels before and after the grinding process and the topography of the ground surface were also measured. The parameters Sa and $\hat{S}z$ ($\hat{S}z = S_{pk} + S_k + S_{vk}$) were used to characterize the grinding heads. The conducted analyses showed the dependence of the parameters Sa and $\hat{S}z$ of new grinding heads on the grain size described by the quadratic function ($R^2 \geq 0.94$). Statistically significant changes in the parameters Sa and $\hat{S}z$ on the cutting surface of the grinding wheel, which occurred as a result of its wear, were observed. There was no significant relationship between the feed rate and the wear of grinding heads, probably due to the relatively small volume of the material removed. A positive correlation between the Sa and $\hat{S}z$ parameters of the ground object and the grain size was observed. The research also showed an increase in the process temperature with an increase in the feed rate and an increase in the grain size.

Keywords: grinding, corundum ceramic, spherical diamond head, grinding-wheel wear.

INTRODUCTION

Modern advanced materials, some of which are various types of ceramics, including corundum and zirconium ceramics, belong to the group of difficult-to-machine materials that cause problems when shaping the surface. Ceramic materials are widely used in the aviation, automotive and energy industries as well as in medical engineering as materials for bone and dental implants. Their specific properties, such as high hardness and high brittleness, mean that sometimes the only way to shape elements made of ceramics is grinding with diamond grinding Hades. Therefore, grinding is considered to be the basic method of finishing type of machining for ceramic products [1–4].

The authors of the studies [5–6] emphasize the influence of the grinding process on the surface quality of ceramic products. They consider the surface roughness parameters to be an important factor in the analysis of the surface quality after grinding ceramic elements.

Machining of geometrically complex surfaces made of materials such as ceramics is possible thanks to the use of spherical grinding heads and multi-axis CNC machines, which allow the tool to be tilted in two directions. Such kinematics of machines in combination with a high-speed spindle allows for any surface shaping of parts made of this type of materials [7–9].

The authors of the article [10] conducted a study of the influence of the lead angle and the tilt

angle of the spherical diamond head on selected parameters of the machined surface topography. They determined for which tool setting angles a lower surface roughness value can be obtained. They also determined the influence of the tool orientation on the grinding force values. The authors also showed a relationship between the 5-axis grinding and milling process in relation to the tool setting and the obtained force values.

In the article [11], the authors referred to the tool positioning angles in relation to the machined surface. The issues of the participation of the tool tip in the machining process and its influence on the machining surface were verified.

In publication [12], the authors presented the kinematics of 5-axis milling with a spherical mill. They described the orientation angles of the tool axis and determined their influence on the machining accuracy and surface quality. They also analyzed 3-axis, 3+2-axis and 5-axis machining in terms of accuracy and parameters of the machined surface.

Articles [13–15] discuss the issues of grinding pre-sintered ceramics with spherical diamond heads. They raise issues related to the influence of technological parameters on surface quality. The works determined the dependence of grinding parameters on selected parameters of surface roughness. Another aspect described is the influence of the positioning of the tool axis on the machined surface. The authors also determined the correlations of the tool axis positioning angle values on the technological parameters of the grinding process.

In the articles [16, 17], the authors discussed the roughness parameters of ceramic materials after grinding. They developed models predicting the surface roughness, taking into account the topography of the grinding wheel, grain size and technological parameters of grinding. The authors of the publication [18] in their study showed the use of a thermal imaging camera to measure temperature in the grinding process. They demonstrated the usefulness of this solution for improving the temperature distribution models in the machining zone.

The publications [19, 20] describe the method of using a thermal imaging camera to measure the temperature of the machining zone. In both publications, the authors noted the advantages and disadvantages of this method of temperature measurement. The highlighted advantage of the method was the speed of obtaining results from

a large area of the analyzed surface, and the disadvantage - the correct selection of the emissivity coefficients of the surface for which the measurement is performed.

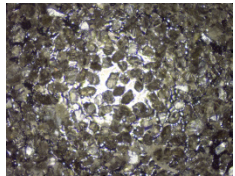
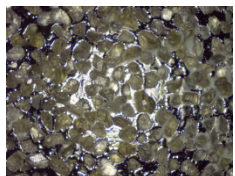
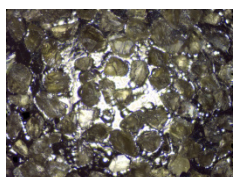
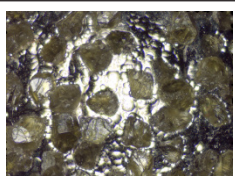
Among the tools that enable the machining of elements made of ceramic materials, diamond heads play a significant role. As in finishing milling of complex surfaces, where a spherical mill is the first choice, the spherical heads are suitable for grinding this type of surface.

There are no studies describing the issues of grinding with spherical grinding heads in the scientific literature. The purpose of this paper is to present the relationship between the feed rate and its influence on tool wear, and the temperature of the machining zone and the condition of the machining surface after grinding corundum ceramics.

MATERIALS AND METHODS

The grinding tests were carried out on the Sauer Ultrasonic 20 Linear 5-axis machining center. Three Pferd DKU-A 3.0 / 3–42 spherical diamond heads with different grain sizes were used for the grinding process, as shown in Table

Table 1. Presentation of grinding heads used for tests

Nº	Tool	Grain number	View of grinding wheel cutting surface
1	DKU-A 3.0/3-42	D64	
2	DKU-A 3.0/3-42	D91	
3	DKU-A 3.0/3-42	D126	
4	DKU-A 3.0/3-42	D181	

1. The tools were mounted in ER16 collet holders. The test object was attached to the machine table with a vice.

The machined material was pre-sintered corundum ceramics prepared in the form of two identical cubes with a side length of 40 mm, divided into zones equal in terms of their surface area (Fig. 1).

During grinding, a single, constant angular position of the grinding head arbor in relation to the machined surface was assumed, described by the lead and tilt angles of 0° and 35° , respectively. This is shown in Figure 2. The applied technological parameters during the grinding tests are shown in Table 2. The grinding width was determined in such a way as to maintain the scallop parameter at $1 \mu\text{m}$.

The temperature in the machining zone was recorded during the grinding tests. For this purpose, a Flir SC5000 thermal imaging camera was used, placed on a tripod in such a way as to obtain the best possible view of the grinding zone. No coolant was used in the grinding tests. This was due to the process temperature recording method. The view of the test stand is shown in Figure 3.

The analysis of the grinding wheel topography before and after the grinding process was carried out on the 3D system InfiniteFocus - Alicona focus variation microscope, while the 3D TalyScan 150 profilometer was used to measure the topography of the ceramic surface after grinding.

Grinding wheel measurements were carried out with a $\times 10$ lens. Three areas ($1.04 \times 1.43 \text{ mm}$) spaced 120° apart were measured on each wheel. The same areas were measured before and after the grinding process. The topography of the grinding surface was measured by the contact

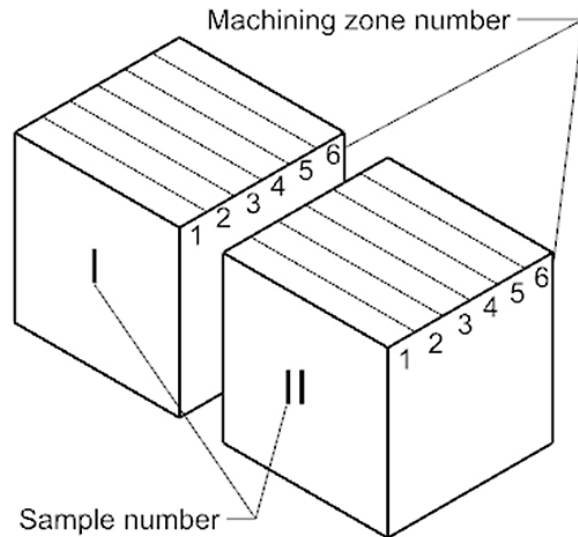


Fig. 1. Samples divided into machining zones

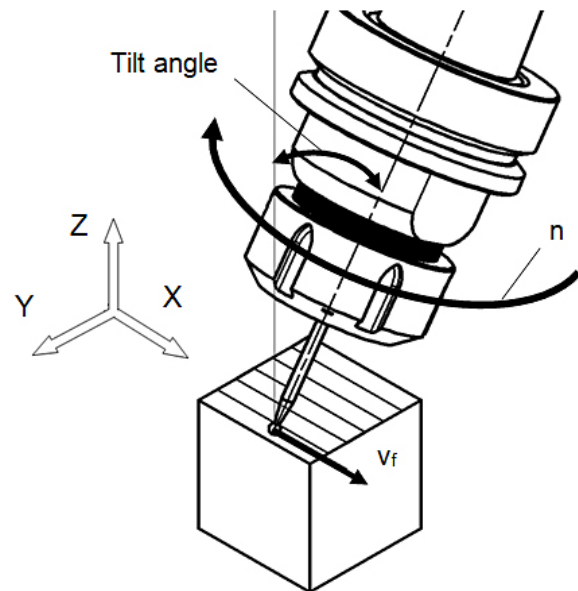


Fig. 2. Diagram showing the kinematics of the grinding tests performed

Table 2. Technological parameters used during machining

N ^o	Grain number	Average grain size d_g [μm]	Feed rate v_f [mm/min]	Other parameters
1	D64	58	200	Spindle speed $n = 38\ 000$ [min^{-1}] Grindind deapth $a_p = 30$ [μm] scallop parameter = 1 [μm] Tilt ange = 35 [$^\circ$] Lead angle = 0 [$^\circ$]
2	D64	58	400	
3	D64	58	600	
4	D91	82.5	200	
5	D91	82.5	400	
6	D91	82.5	600	
7	D126	119.5	200	
8	D126	119.5	400	
9	D126	119.5	600	
10	D181	165	200	
11	D181	165	400	
12	D181	165	600	

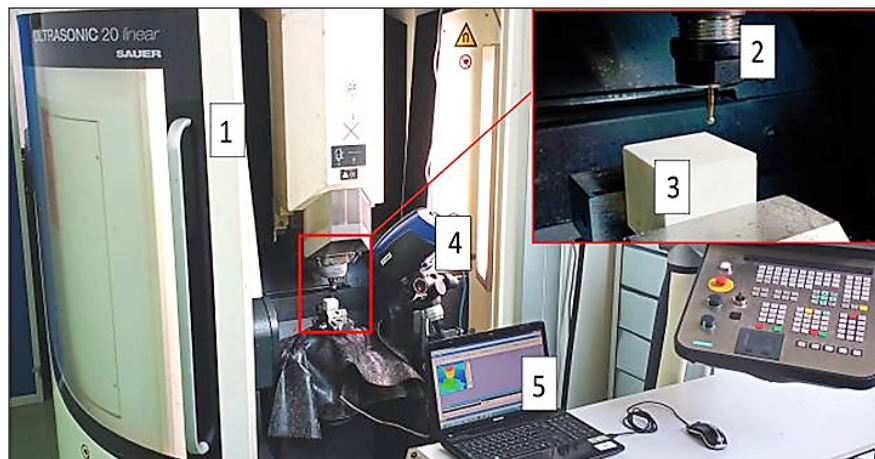


Fig. 3. View of the test stand: 1 – Ultrasonic 20 Linear machine tool, 2 – tool, 3 – workpiece, 4 – thermal imaging camera, 5 – computer

method with a sampling step in the horizontal axes of $5\ \mu\text{m}$. Five areas measuring $1 \times 1\ \text{mm}$ were measured on each surface. The processing of the measurement data with the determination of 3D parameters of the geometric structure of the surface was carried out in the SPIP 6.4.2 program. Two high parameters Sa and $\hat{S}z$ [15] were adopted for the analyses. In the case of the analysis of the topography of the active surfaces of the grinding wheels, due to the occurrence of atypical spikes and cavities that often accompany optical measurements, the directly determined Sz parameter was not taken into account. In order to limit the impact of the above-mentioned peaks, the value of Sz is approximated by the sum of the parameters of the material proportion curve:

$$\hat{S}z = Spk + Sk + Svk \quad (1)$$

Statistical analyses were performed in the JMP 12 program. The significance level was set at 0.05 for all tests.

RESULTS AND DISCUSSION

Topography of new grinding wheels

Figures 4–7 presents exemplary topography maps of measured grinding wheel surfaces before and after grinding. The conducted analyses showed the dependence of the Sa parameters and the $\hat{S}z$ of new grinding wheels on the grain size d_g described by the quadratic function (Fig. 5):

$$Sa = 10.93 - 0.08 \cdot d_g + 11.7 \cdot 10^{-4} \cdot d_g^2 \quad (2)$$

$$\hat{S}z = 26.69 + 0.27 \cdot d_g + 23.2 \cdot 10^{-4} \cdot d_g^2 \quad (3)$$

Analysis of variance showed the equations to be statistically significant ($p < 0.0001$). The coefficient of determination for the model with the variable Sa was $R^2 = 0.94$, and with the variable $\hat{S}z$ $R^2 = 0.95$. The obtained results correspond to the linear relationship determined by Shi [22] linking the grain size d_g with mean

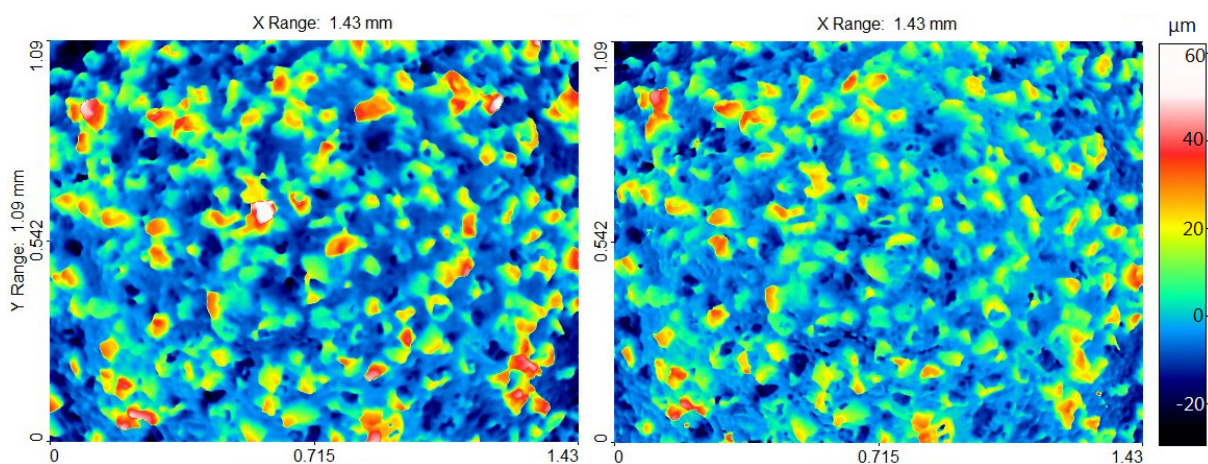


Fig. 4. Topography maps of new (left) and used (right) grinding wheel D64

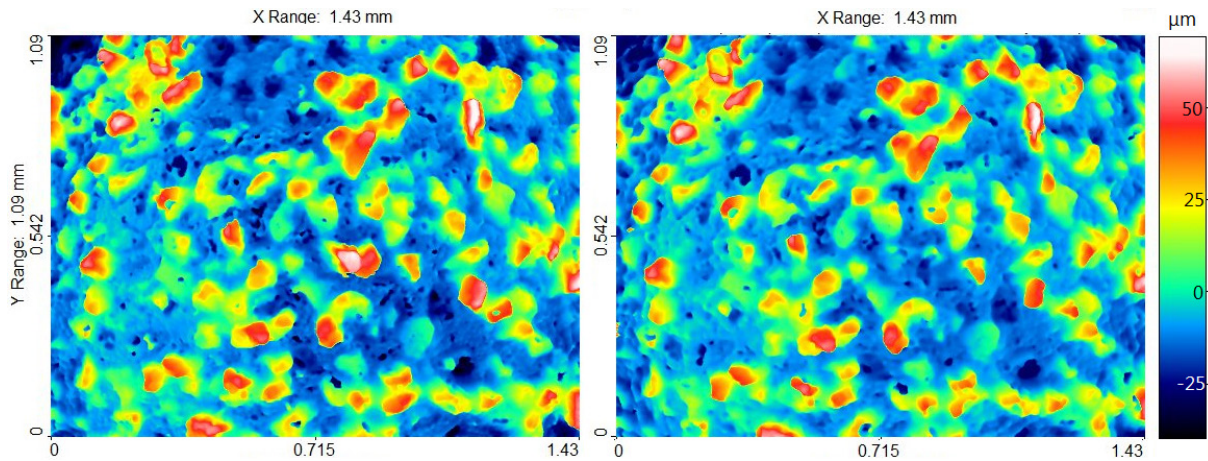


Fig. 5. Topography maps of new (left) and used (right) grinding wheel D91

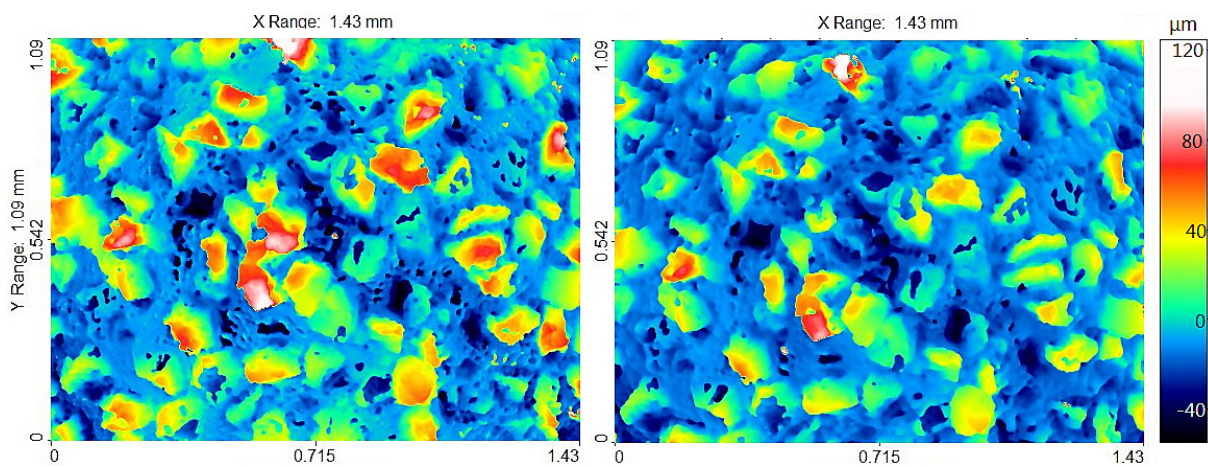


Fig. 6. Topography maps of new (left) and used (right) grinding wheel D126

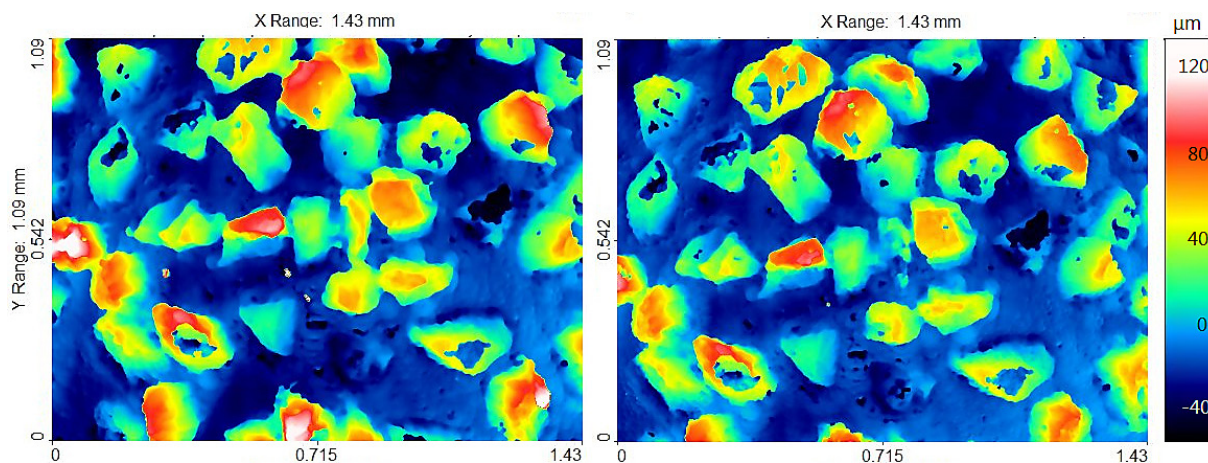


Fig. 7. Topography maps of new (left) and used (right) grinding wheel D181

grain protrusion heights. Determining the S_a or S_z from the measurement of the surface topography, however, is much simpler than the determination of grains protrusion heights.

In Figure 8 it is also visible that with the increase of the grain size the scatter of the results

also increased. It was caused by the deterioration of the measurement conditions. The walls of the abrasive grains had very smooth surfaces, which in some places made it impossible to measure them correctly with the use of a focus variation microscope.

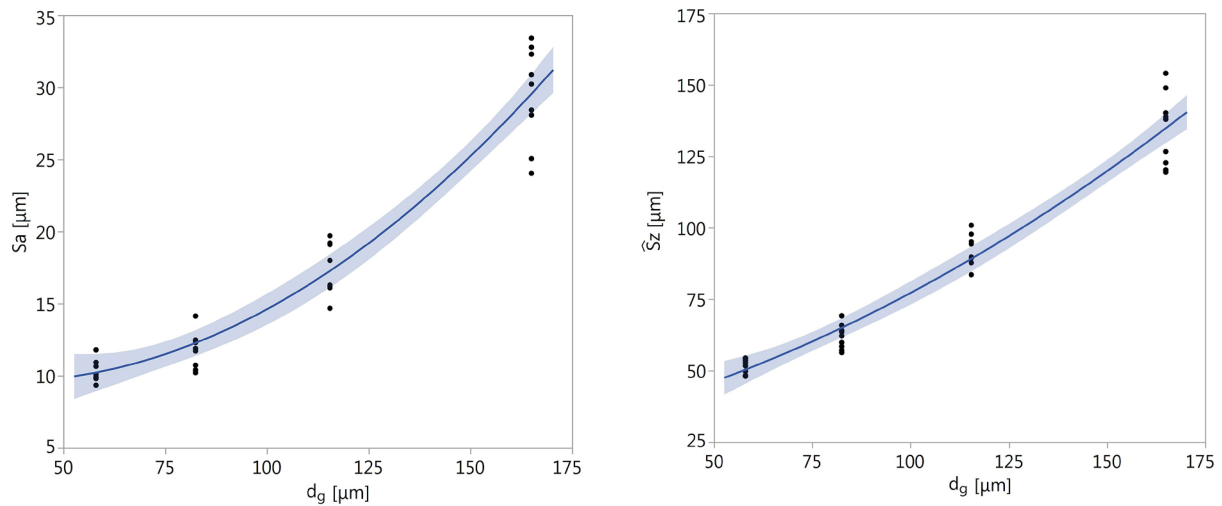


Fig. 8. Correlation of Sa i $\hat{S}z$ parameters of new grinding wheels on grain size with a confidence interval of 0.95

Influence of grain size on the wear of grinding wheel cutting surface

When examining the wear of grinding wheels that occurred during the experiment, it was first checked whether the observed differences in the values of Sa and $\hat{S}z$ parameters of the active surfaces of new grinding wheels and those after the grinding process were statistically significant. For this purpose, Wilcoxon signed rank tests (earlier Levene’s tests showed different variances in the studied groups) for each grain size separately were conducted. For all 4 tested cases, the tests showed that for the new grinding wheels, the values of Sa and $\hat{S}z$ parameters are statistically greater than for the used grinding wheels (Fig. 9).

The tests revealed the linear dependence of the parameters Sa and $\hat{S}z$ from the grinding head

active surfaces after grinding on the parameter values characterizing the new grinding wheels (Fig. 10). Regression models take into account grinding wheels of all tested grain sizes and are expressed by the following formulas:

$$Sa (used) = -0,04 + 0,93 Sa (new) \quad (4)$$

$$\hat{S}z (used) = -1,48 + 0,97 \hat{S}z (new) \quad (5)$$

Analysis of variance showed the equations to be statistically significant ($p < 0.0001$). The coefficient of determination for the model with the variable Sa was $R^2 = 0.98$, and with the variable $\hat{S}z$ $R^2 = 0.99$. The nature of the aforementioned model relationships with a very good fit indicates that the intensity of changes in the values of Sa and $\hat{S}z$ parameters was independent of the grain size. The publication [22] noted that the wear intensity of

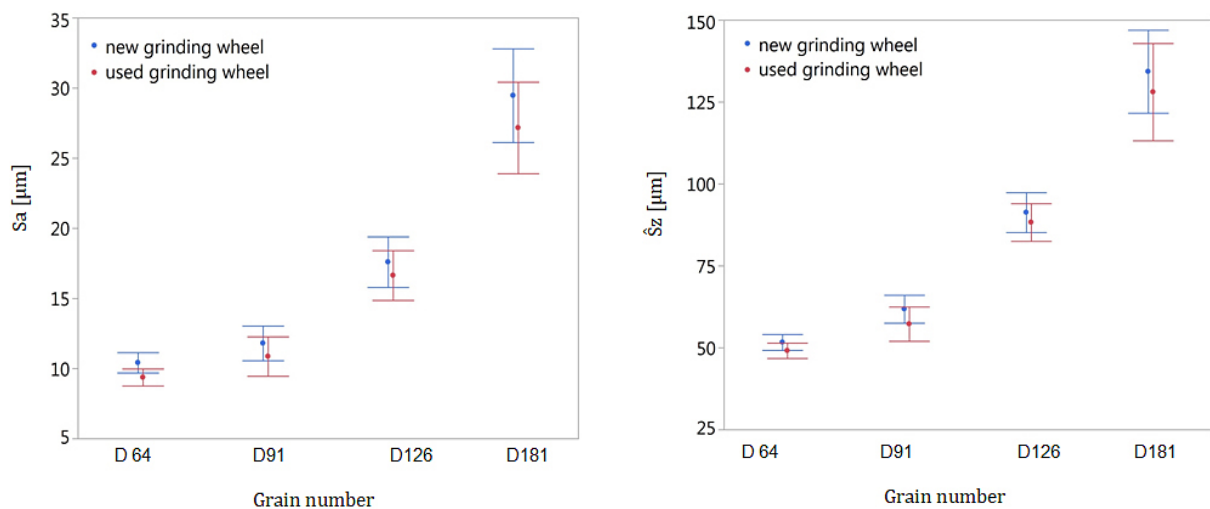


Fig. 9. Values of parameters Sa and $\hat{S}z$ before and after the grinding process

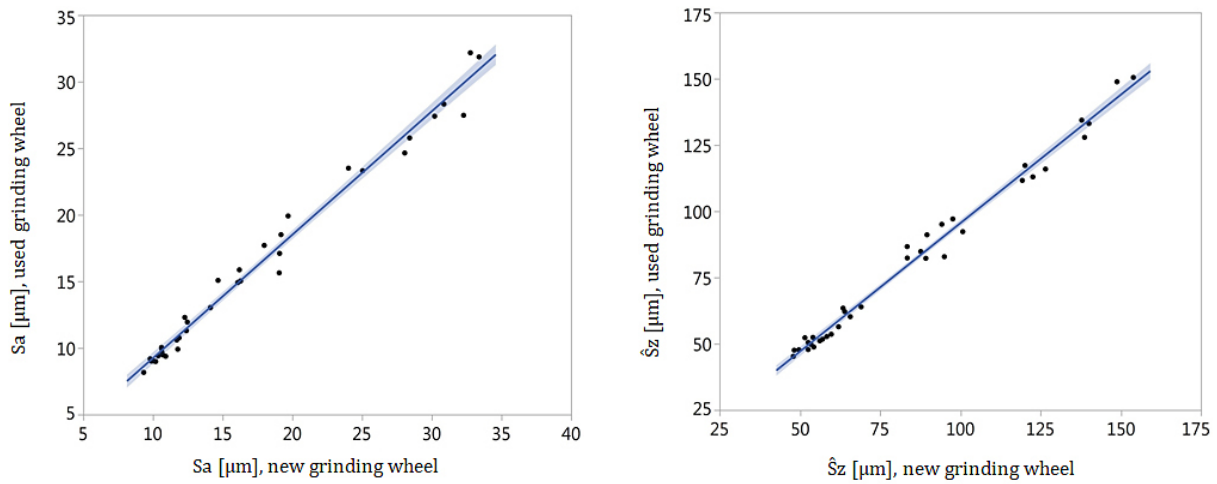


Fig. 10. Dependence of Sa and $\hat{S}z$ parameters of the grinding head active surfaces determined for used grinding wheels on the values of these parameters for new grinding wheels

grains cBN in the stable wear phase during steel grinding depends on their size. Taking into account the fact that in the conducted tests the grinding wheels showed relatively little material (8 mm^3), it can be assumed that the observed wear resulted from the initial stage of wear of the abrasive grains, in which the grains are just lapping. In this phase, the wear is very intense. Afterwards occurs a phase of stable wear. Therefore, in order to verify the effect of grain size on the wear intensity, the research should be continued.

Influence of feed rate on the wear of grinding wheel cutting surface

With an increase in the feed rate, the grinding efficiency and the undeformed

chip thickness, both being are a measure of the load on the grinding wheel – thus, the grinding force and power components also increase. This, in turn, is associated with increased wear of the grinding wheel [23, 24]. However, the analysis of variance did not show any significant dependencies between the feed rate and the wear of grinding wheels (observed through the parameters Sa and $\hat{S}z$ from the active surface of the grinding wheel (Fig. 11) and their change).

Probably only in a phase of stable wear it would be possible to observe the influence of the feed on the different intensity of grain wear. Therefore, in order to verify the influence of the feed rate on the wear of grinding wheels, the research should be continued.

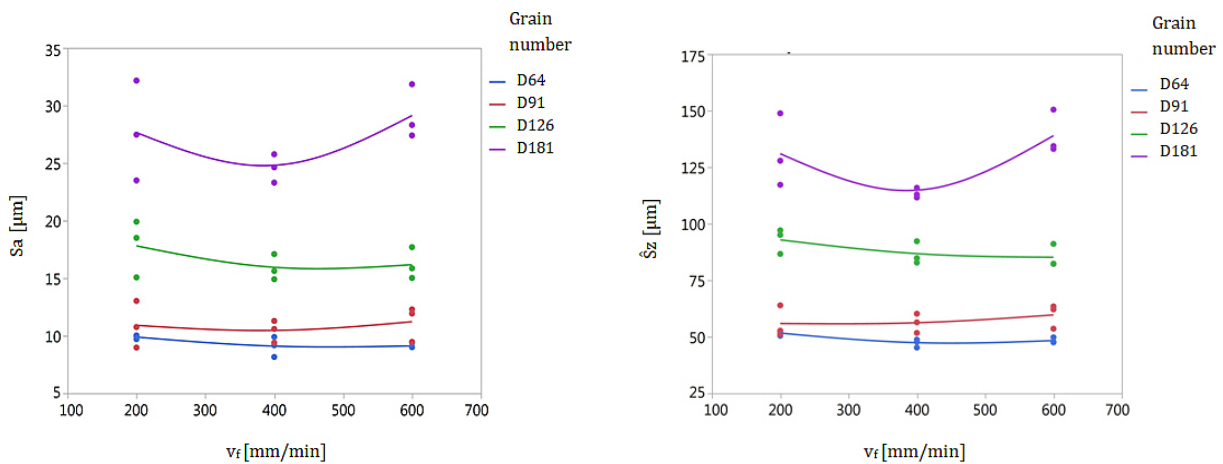


Fig. 11. Influence of the feed rate v_f on the values of the parameters Sa and $\hat{S}z$ from the active surface of the grinding wheel after grinding (the lines are not regression lines, they were introduced for greater clarity)

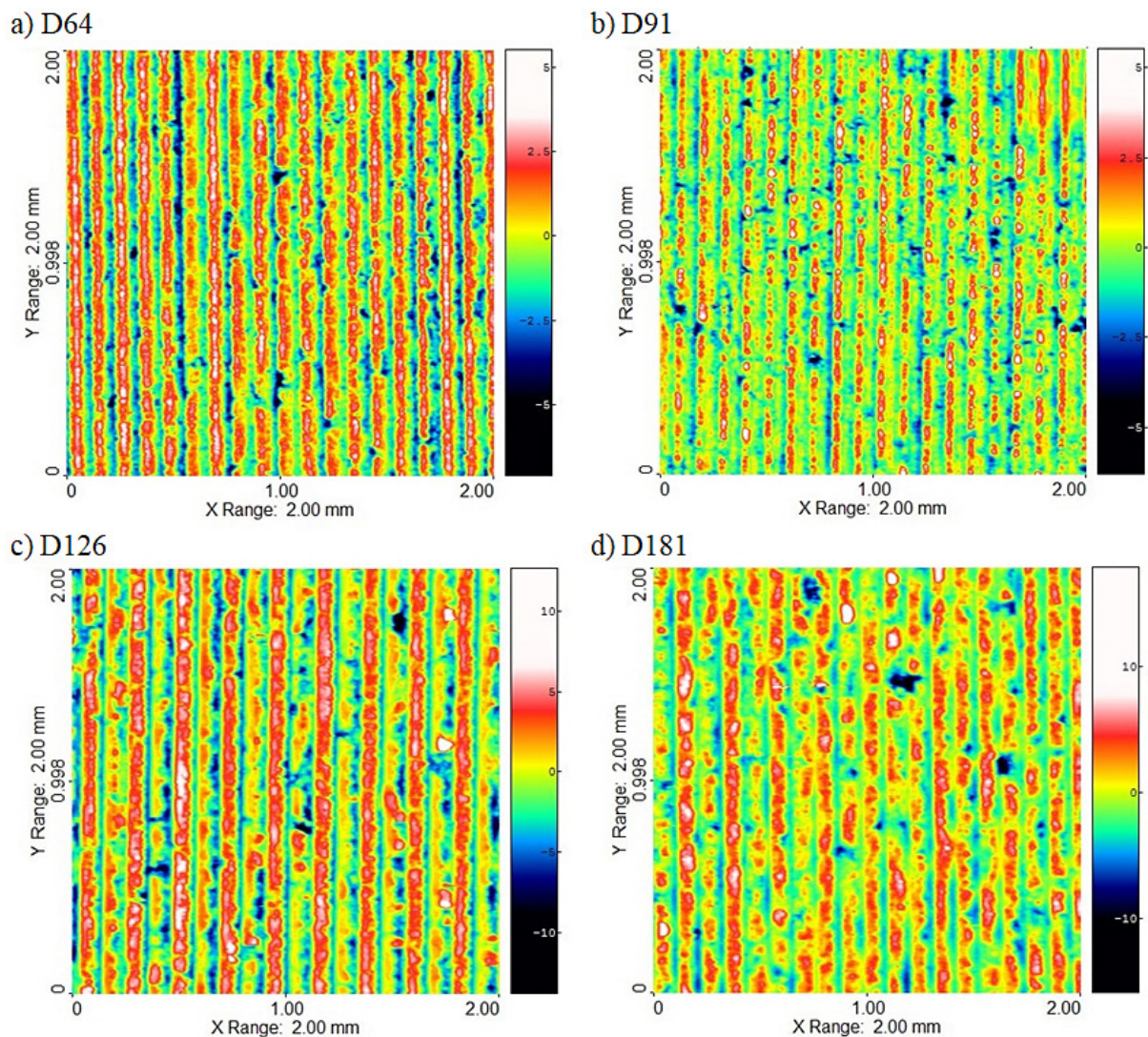


Fig. 12. Topography maps of surfaces ground with grinding wheels with different grain size

Influence of grain size and feed rate on surface roughness

Figures 12 presents exemplary topography maps of the ground surfaces. A positive correlation was observed between the grain size and the roughness parameter of the ground object S_a (Spearman's $\rho = 0.73$) and S_z (Spearman's $\rho = 0.68$) (Fig. 13). Smaller grain size is associated with the presence of a greater number of active grains on the grinding wheel, which favors machining the surface with lower roughness. Similar relationships for single-layer grinding wheels were reported in works [25–30].

In the conducted research it was not shown that the feed rate had a statistically significant influence on the tested parameters of the ground surface.

Influence of grain size and feed rate on grinding zone temperature

In the work, a regression analysis was carried out in order to investigate the effect of grain size and feed rate on the grinding temperature. For this purpose, the classical model of the response surface in the form of a second degree polynomial with two-factor interaction was used. In the determined model, the interaction of the feed rate and the grain size was not statistically significant. The developed model, with the adjusted coefficient of determination $R^2_{adj} = 0.97$, is expressed by the formula:

$$T = 25 + 0.2 \cdot d_g + 0.07 \cdot v_f - 2 \cdot 10^{-3} \cdot (d_g - 105.25)^2 - 9.7 \cdot 10^{-5} \cdot (v_f - 400)^2 \quad (6)$$

Analysis of variance showed the equation to be statistically significant ($p < 0.0001$). The response area is graphically presented in Figure 14.

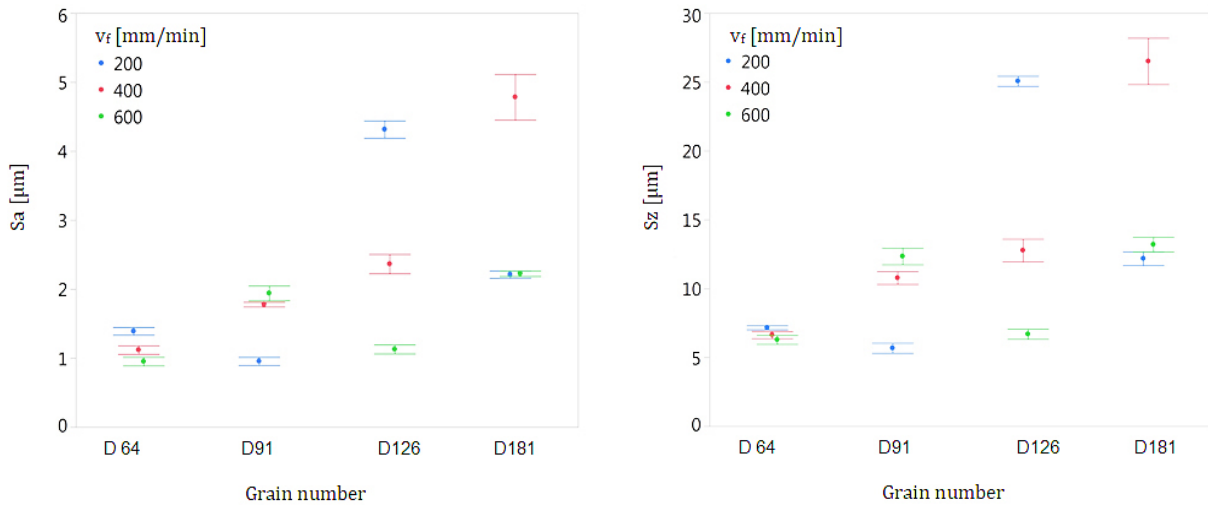


Fig. 13. Influence of grain size and feed rate f on the values of parameters Sa and Sz from the ground surface

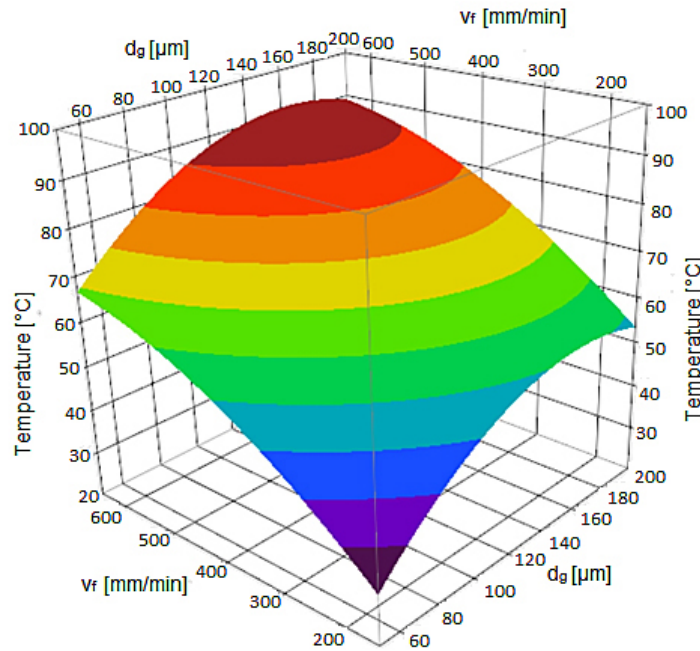


Fig. 14. Influence of grain size d_g and feed rate v_f on grinding temperature T

In the examined state space, the feed rate had a greater influence on the temperature than the grain size. The observed temperature values increased with the increase of the feed rate and the grain size. The tested factors had a greater impact on the temperature with their lower values.

Increasing the feed rate leads to an increase in the undeformed chip thickness and grinding power, and thus to an increase in the grinding temperature. For single-layer grinding wheels, this was confirmed, among others, by research [31, 32]. In the case of wheels with a smaller grain size on the grinding wheel, it can be expected that there were more active edges and the grains had a sharper

shape, which reduced the undeformed chip thickness and grinding temperature [33–35].

CONCLUSIONS

The results of experimental tests presented in this study show that there is a relationship between the set feed rate and grain size and the wear of grinding wheels, surface quality and temperature in the treatment zone. For new grinding wheels, the relationship between the Sa and $\hat{S}z$ parameters on the grain size d_g can be determined by the quadratic function.

Increasing the grain size resulted in greater variability of the grinding wheel topography measurements, resulting from the limitations of the measurement method.

Examinations of the cutting surfaces of grinding wheels showed a linear relationship between Sa and $\hat{S}z$ parameters from worn to a new grinding wheel. The conducted analyses did not show any significant relations linking the feed rate and the wear of the grinding wheel. The reasons for this should be seen in the insufficient amount of material removed by each of the wheels used.

The analysis of the results revealed a positive correlation between the grain size and roughness parameters Sa and $\hat{S}z$. However, there is no clear influence of the feed rate v_f on the discussed parameters of the roughness of the ground surface. The dependence of the grain size and the feed rate on the temperature in the grinding zone was observed. Both the increase in grain size and the increase in the feed rate resulted in an increase in temperature.

The presented study is a starting point for further research on the influence of technological parameters on the wear of spherical diamond heads and the surface condition of ceramic materials after grinding. The scope of research should be extended to increase the machining areas so that greater tool wear could be observed. Another aspect by which the scope of research can be extended are the variable positioning angles of the tool and their impact on the wear of the grinding wheel grains.

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