

Using SMATH software for the analysis of steady states in electric circuits

Miroslaw Woloszyn, Joanna Woloszyn

Gdansk University of Technology

80-233 Gdańsk, ul. Narutowicza 11/12, e-mail: miroslaw.woloszyn@pg.gda.pl

This paper presents software that can be used for educational purposes – teaching students to perform the analysis of electric circuits [1]. Programmes created in the SMATH system [2] make it possible to solve exercises on electric circuits and constitute an interesting tool supporting the teaching process. The fact that the students can form their own electric circuit structures, with a preview of the equations and the solutions of these calculations, offers to them an interesting learning alternative.

KEYWORDS: electric circuits, computer, SMATH software

1. Introduction

Contemporary computer programmes supporting the analysis of electric and circuits, such as, for instance, PSpice, MATLAB Simulink or TCAD, are an extremely helpful engineering tool. The programmes are also used to teach electrical engineering and electronics basics. However, they do not allow the students to learn the methods of solving electric circuits. The MathCad program is a very good tool for solving electric circuits with the use of classic methods. In this programme formulas are entered in the graphic panel, and the programme does automatic calculations. Coding ability is not required, which is a considerable advantage of the tool. A relatively high price of the MathCad programme is its disadvantage. The SMATH system is an alternative, free programme which is very similar in terms of its application to MathCad. Undoubtedly, its calculation capacity is much smaller in comparison with MathCad, however, it can be successfully used for performing engineering calculations. SMATH can also be used for teaching electrical engineering basics. Students who take the advantage of the ready examples of electric circuits solutions can in a simple way create their own electric circuits models and verify the results of their calculations against numeric results. The programmes developed in the SMATH system make it possible to analyse the methodology of solving electric circuits with the use of various methods (nodal analysis, superposition and similarity method).

2. Electric circuits Analysis in SMATH

This paper presents a number of examples of the SMATH programme application to solve linear electric circuits of direct and alternating current with the use of node voltage analysis method. It describes the method of creating one's own electric circuits scheme with imposed structure, which can be simplified by eliminating selected branches.

2.1. Analysis of direct current steady state

The model of the element E_i (i – element number) of the direct current circuit used in the SMATH programme includes a voltage source E_i , a resistance R_i , a current source I_{pi} and a resistance R_{pi} (Fig. 1).

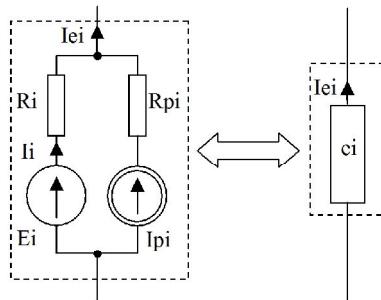


Fig. 1. Model of the direct current circuit element

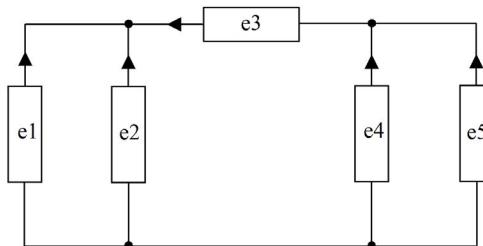


Fig. 2. Structure of a sample electric circuit

The structure of a sample direct current circuit is shown in Fig. 2. In the event when there is only an ideal voltage source for a given branch, the following values should be entered for the remaining elements of the branches: $I_{pi} = 0 \text{ A}$, $R_{pi} = ?$ (any value can be entered) and $R_i = 10^{-4} \Omega$ (four orders smaller value than the lowest resistance in the circuit). If the resistance R_i and the source voltage E_i are not present in the branch model, the following values

should be entered: $R_i = 10^6 \Omega$ and $E_i = 0 \text{ V}$. Figure 3 shows an electric circuit model with the following parameters: $E_1 = 40 \text{ V}$, $R_1 = 5 \Omega$, $E_2 = 50 \text{ V}$, $R_2 = 10 \Omega$, $I_{p3} = 2 \text{ A}$, $R_3 = 10 \Omega$, $I_{p4} = 0.5 \text{ A}$, $E_5 = 10 \text{ V}$, $R_5 = 15 \Omega$.

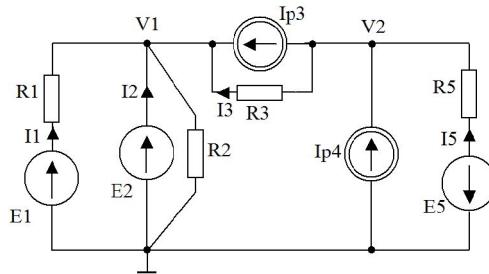


Fig. 3. Direct electric current circuit diagram

SM Math Studio - [Zad_Poznan_1.sm]

File Edit View Insert Calculation Tools Pages Help

E1 := 40 R1 := 5 Ip1 := 0 Rp1 := 0
 E2 := 50 R2 := 10 Ip2 := 0 Rp2 := 10
 E3 := 0 R3 := 10 Ip3 := 2 Rp3 := 0
 E4 := 0 R4 := 10 Ip4 := 0, 5 Rp4 := 0
 E5 := -10 R5 := 15 Ip5 := 0 Rp5 := 0

$V1 \cdot \left(\frac{1}{R1} + \frac{1}{R2} + \frac{1}{R3} \right) - \frac{V2}{R3} = \frac{E1}{R1} + Ip1 + \frac{E2}{R2} + Ip2 + \frac{E3}{R3} + Ip3$
 $V2 \cdot \left(\frac{1}{R3} + \frac{1}{R4} + \frac{1}{R5} \right) - \frac{V1}{R3} = -\frac{E3}{R3} - Ip3 + \frac{E4}{R4} + Ip4 + \frac{E5}{R5} + Ip5$

$A := \begin{pmatrix} \frac{1}{R1} + \frac{1}{R2} + \frac{1}{R3} & -\frac{1}{R3} \\ -\frac{1}{R3} & \frac{1}{R3} + \frac{1}{R4} + \frac{1}{R5} \end{pmatrix} \quad Y := \begin{pmatrix} \frac{E1}{R1} + Ip1 + \frac{E2}{R2} + Ip2 + \frac{E3}{R3} + Ip3 \\ -\frac{E3}{R3} - Ip3 + \frac{E4}{R4} + Ip4 + \frac{E5}{R5} + Ip5 \end{pmatrix}$
 $V := A^{-1} \cdot Y \quad V = \begin{pmatrix} 50 \\ 16,9999 \end{pmatrix}$

$V1 := V_1 \quad V2 := V_2 \quad V1 = 50 \quad V2 = 16,9999$
 $I1 := \frac{E1 - V1}{R1} \quad I1 = -2 \quad Ie1 := I1 + Ip1 \quad Ie1 = -2$
 $I2 := \frac{E2 - V1}{R2} \quad I2 = 3,3 \quad Ie2 := I2 + Ip2 \quad Ie2 = 3,3$
 $I3 := \frac{E3 - V1 + V2}{R3} \quad I3 = -3,3 \quad Ie3 := I3 + Ip3 \quad Ie3 = -1,3$
 $I4 := \frac{E4 - V2}{R4} \quad I4 = 0 \quad Ie4 := I4 + Ip4 \quad Ie4 = 0,5$
 $I5 := \frac{E5 - V2}{R5} \quad I5 = -1,8 \quad Ie5 := I5 + Ip5 \quad Ie5 = -1,8$

Fig. 4. Programme for the direct current circuit analysis – solution part 1 (Fig. 3)

In order to solve the electric circuit the following values were entered in the SMATH programme (Fig. 4, Fig. 5): $E_1 = 40 \text{ V}$, $R_1 = 5 \Omega$, $I_{p1} = 0 \text{ A}$, $R_{p1} = 0 \Omega$, $E_2 = 50 \text{ V}$, $R_2 = 10 \Omega$, $I_{p2} = 0 \text{ A}$, $R_{p2} = 10 \Omega$, $E_3 = 0 \text{ V}$, $R_3 = 10 \Omega$, $I_{p3} = 2 \text{ A}$, $R_{p3} = 0 \Omega$, $E_4 = 0 \text{ V}$, $R_4 = 10^6 \Omega$, $I_{p4} = 0.5 \text{ A}$, $R_{p4} = 0 \Omega$, $E_5 = -10 \text{ V}$, $R_5 = 15 \Omega$, $I_{p5} = 0 \text{ A}$, $R_{p5} = 0 \Omega$. The user can analyse the method of the circuit solving by following the formulas (Fig. 4, 5) included in the programme and verify his/her own calculations against those delivered by the programme (Fig. 5). In the event when only an ideal voltage source was added in the circuit, then the user solving the formula saves a smaller number of equations. Very low current values below μA should be considered as zero values.

SMath Studio - [Zad_Poznan_1.sm*]

File Edit View Insert Calculation Tools Pages Help

napięcia źródeł prądowych

$$Ui1 := V1 + Ip1 \cdot Rp1 \quad Ui1 = 50$$

$$Ui2 := V1 + Ip2 \cdot Rp2 \quad Ui2 = 50$$

$$Ui3 := V1 - V2 + Ip3 \cdot Rp3 \quad Ui3 = 33,0001$$

$$Ui4 := V2 + Ip4 \cdot Rp4 \quad Ui4 = 16,9999$$

$$Ui5 := V2 + Ip5 \cdot Rp5 \quad Ui5 = 16,9999$$

Bilans mocy

Moc źródeł

$$Pz1 := E1 \cdot I1 + Ui1 \cdot Ip1 \quad Pz2 := E2 \cdot I2 + Ui2 \cdot Ip2 \quad Pz5 := E5 \cdot I5 + Ui5 \cdot Ip5$$

$$Pz3 := E3 \cdot I3 + Ui3 \cdot Ip3 \quad Pz4 := E4 \cdot I4 + Ui4 \cdot Ip4 \quad Pz5 = 17,9999$$

$$Pz := Pz1 + Pz2 + Pz3 + Pz4 + Pz5$$

Moc odbiorników

$$Po1 := I1^2 \cdot R1 + Ip1^2 \cdot Rp1 \quad Po2 := I2^2 \cdot R2 + Ip2^2 \cdot Rp2 \quad Po5 := I5^2 \cdot R5 + Ip5^2 \cdot Rp5$$

$$Po3 := I3^2 \cdot R3 + Ip3^2 \cdot Rp3 \quad Po4 := I4^2 \cdot R4 + Ip4^2 \cdot Rp4$$

$$Po := Po1 + Po2 + Po3 + Po4 + Po5$$

$$Ie1 = -2 \quad Ie2 = 3,3 \quad Ie3 = -1,3 \quad Ie4 = 0,5 \quad Ie5 = -1,8$$

Pz = 177,5004

Po = 177,5004

Fig. 5. Programme for the direct current circuit analysis – solution part 2 (Fig. 3)

Figure 6 shows another example of direct current circuit structure. In turn, Fig. 7 shows a circuit diagram with the topology as in Fig. 6, with the following parameters: $E_1 = 100 \text{ V}$, $R_1 = 20 \Omega$, $R_2 = 10 \Omega$, $I_{p3} = 3 \text{ A}$, $R_3 = 2 \Omega$, $E_4 = 40 \text{ V}$, $R_4 = 25 \Omega$, $R_5 = 15 \Omega$, $I_{p6} = 10 \text{ A}$, $R_6 = 20 \Omega$. In order to solve the electric circuit the following values were entered in the SMATH programme:

$E_1 = 100 \text{ V}$, $R_1 = 20 \Omega$, $I_{p1} = 0 \text{ A}$, $R_{p1} = 0 \Omega$, $E_2 = 0 \text{ V}$, $R_2 = 10 \Omega$, $I_{p2} = 0 \text{ A}$, $R_{p2} = 0 \Omega$, $E_3 = 0 \text{ V}$, $R_3 = 10^6 \Omega$, $I_{p3} = 3 \text{ A}$, $R_{p3} = 2 \Omega$, $E_4 = 40 \text{ V}$, $R_4 = 25 \Omega$, $I_{p4} = 0 \text{ A}$, $R_{p4} = 0 \Omega$, $E_5 = 0 \text{ V}$, $R_5 = 15 \Omega$, $I_{p5} = 0 \text{ A}$, $R_{p5} = 0 \Omega$, $E_6 = 0 \text{ V}$, $R_6 = 20 \Omega$, $I_{p6} = 10 \text{ A}$, $R_{p6} = 0 \Omega$. Figure 8 and Fig. 9 show the solution of the electric circuit from Fig. 7.

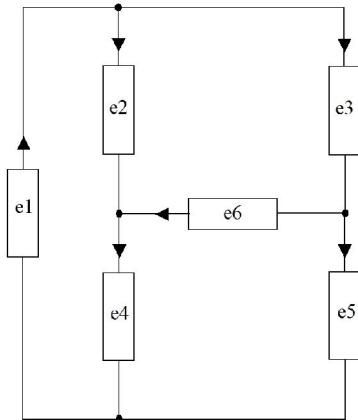


Fig. 6. Topology of a direct current circuit
(second example)

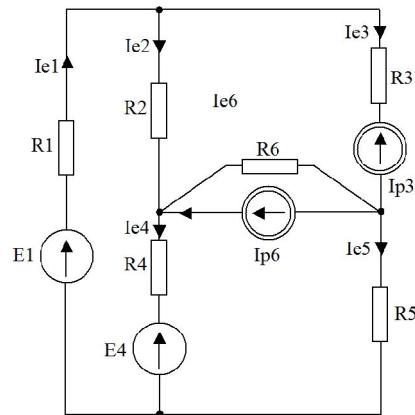


Fig. 7. Direct current circuit diagram
(second example)

SMATH Studio - [Zad_Poznan_N2.sm]

File Edit View Insert Calculation Tools Pages Help

E1 := 100 R1 := 20 I_{p1} := 0 R_{p1} := 0
E2 := 0 R2 := 10 I_{p2} := 0 R_{p2} := 0
E3 := 0 R3 := 10⁶ I_{p3} := 3 R_{p3} := 2
E4 := 40 R4 := 25 I_{p4} := 0 R_{p4} := 0
E5 := 0 R5 := 15 I_{p5} := 0 R_{p5} := 0
E6 := 0 R6 := 5 I_{p6} := 4 R_{p6} := 0

V1 $\left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \right) - \frac{V_2}{R_2} - \frac{V_3}{R_3} = \frac{E_1}{R_1} + I_{p1} - \frac{E_2}{R_2} - I_{p2} - \frac{E_3}{R_3} - I_{p3}$

V2 $\left(\frac{1}{R_2} + \frac{1}{R_4} + \frac{1}{R_6} \right) - \frac{V_1}{R_1} - \frac{V_3}{R_6} = \frac{E_2}{R_2} + I_{p2} - \frac{E_4}{R_4} - I_{p4} + \frac{E_6}{R_6} + I_{p6}$

V3 $\left(\frac{1}{R_3} + \frac{1}{R_5} + \frac{1}{R_6} \right) - \frac{V_1}{R_1} - \frac{V_2}{R_6} = \frac{E_3}{R_3} + I_{p3} - \frac{E_5}{R_5} - I_{p5} - \frac{E_6}{R_6} - I_{p6}$

A := $\begin{pmatrix} \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} & -\frac{1}{R_2} & -\frac{1}{R_3} \\ -\frac{1}{R_2} & \frac{1}{R_2} + \frac{1}{R_4} + \frac{1}{R_6} & -\frac{1}{R_6} \\ -\frac{1}{R_3} & -\frac{1}{R_6} & \frac{1}{R_3} + \frac{1}{R_5} + \frac{1}{R_6} \end{pmatrix}$

Y := $\begin{pmatrix} \frac{E_1}{R_1} + I_{p1} - \frac{E_2}{R_2} - I_{p2} - \frac{E_3}{R_3} - I_{p3} \\ \frac{E_2}{R_2} + I_{p2} - \frac{E_4}{R_4} - I_{p4} + \frac{E_6}{R_6} + I_{p6} \\ \frac{E_3}{R_3} + I_{p3} - \frac{E_5}{R_5} - I_{p5} - \frac{E_6}{R_6} - I_{p6} \end{pmatrix}$

V := A⁻¹ · Y

V1 := V₁ V2 := V₂ V3 := V₃

V := $\begin{pmatrix} 29,4594 \\ 24,1892 \\ 14,392 \end{pmatrix}$

V1 = 29,4594
V2 = 24,1892
V3 = 14,392

Fig. 8. Programme for the direct current circuit analysis – solution part 1 (example from Fig. 7)

```

SMATH Studio - [Zad_Poznan_N2.sm]
File Edit View Insert Calculation Tools Pages Help
I1 := E1 - V1 / R1           I1 = 3, 527     Ie1 := I1 + Ip1     Ie1 = 3, 527
I2 := E2 - V2 + V1 / R2       I2 = 0, 527     Ie2 := I2 + Ip2     Ie2 = 0, 527
I3 := E3 - V3 + V1 / R3       I3 = 0         Ie3 := I3 + Ip3     Ie3 = 3
I4 := E4 + V2 - 0 / R4        I4 = 2, 5676    Ie4 := I4 + Ip4     Ie4 = 2, 5676
I5 := E5 + V3 - 0 / R5        I5 = 0, 9595    Ie5 := I5 + Ip5     Ie5 = 0, 9595
I6 := E6 - V2 + V3 / R6       I6 = -1, 9594   Ie6 := I6 + Ip6     Ie6 = 2, 0406
napięcia źródła prądowych
Ui1 := V1 + Ipl1 * Rp1       Ui1 = 29, 4594
Ui2 := V2 - V1 + Ipl2 * Rp2   Ui2 = -5, 2702
Ui3 := V3 - V1 + Ipl3 * Rp3   Ui3 = -9, 0674
Ui4 := 0 - V2 + Ipl4 * Rp4   Ui4 = -24, 1892
Ui5 := 0 - V3 + Ipl5 * Rp5   Ui5 = -14, 392
Ui6 := V2 - V3 + Ipl6 * Rp5   Ui6 = 9, 7972
Bilans mocy                  Moc źródła
Pz1 := E1 * Ie1 + Ui1 * Rp1   Pz2 := E2 * Ie2 + Ui2 * Rp2   Pz5 := E5 * Ie5 + Ui5 * Rp5
Pz3 := E3 * Ie3 + Ui3 * Rp3   Pz4 := E4 * Ie4 + Ui4 * Rp4   Pz6 := E6 * Ie6 + Ui6 * Rp6
Pz = Pz1 + Pz2 + Pz3 + Pz4 + Pz5 + Pz6
Moc odbiorników
Po1 := I1^2 * R1 + Ipl1^2 * Rp1   Po2 := I2^2 * R2 + Ipl2^2 * Rp2   Po5 := I5^2 * R5 + Ipl5^2 * Rp5
Po3 := I3^2 * R3 + Ipl3^2 * Rp3   Po4 := I4^2 * R4 + Ipl4^2 * Rp4   Po6 := I6^2 * R6 + Ipl6^2 * Rp6
Po := Po1 + Po2 + Po3 + Po4 + Po5 + Po6
Ie1 = 3, 527      Ie2 = 0, 527      Ie3 = 3
Ie4 = 2, 5676     Ie5 = 0, 9595     Ie6 = 2, 0406
Pz = 467, 3926    Po = 467, 3926

```

Fig. 9. Programme for the direct current circuit analysis – solution part 2
(example from Fig. 7)

2.2. Analysis of alternating current circuit steady state

It is possible to create numerous combinations of various electric circuits in the analysis alternating current electric circuits, by entering relevant values for particular impedance in the branches.

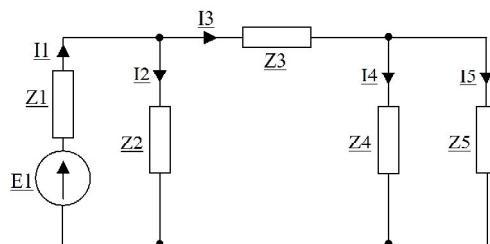


Fig. 10. Structure of a sample alternating current electric circuit

In the case when a given branch is not present in the circuit, a value, e.g. $Z = 10^{15} \Omega$, should be entered. If the impedance value equals zero, then the value $Z = 10^{-6} \Omega$ should be entered. Figure 10 presents an alternating current electric circuit diagram. In order to avoid complications while entering data in the SMATH programme, the number and the type of sources were imposed in the circuit. In the example presented in Fig. 11 there is only one voltage source.

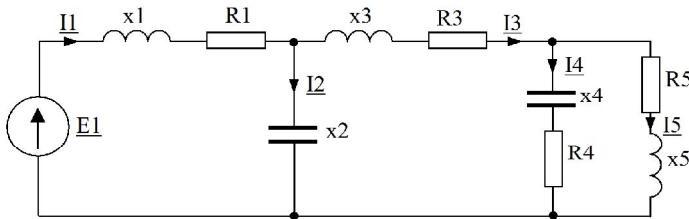


Fig. 11. Alternating current electric circuit diagram

```

SMATH Studio - [Zad_Poznan_N3.sm]
File Edit View Insert Calculation Tools Pages Help
j = √(-1)      rad := π/180      stop := 180/π
E = 240 · e^(j · 30 · rad)      Z1 := 2 + j · 3      E = 207,8461 + 120 · i
Z2 := 0 - j · 20
Z3 := 1, 5 + j · 2, 5
Z4 := 10 - j · 15
Z5 := 18 + j · 25
V1 := (1/Z1 + 1/Z2 + 1/Z3) · V2 = E/Z1
V2 := (1/Z3 + 1/Z4 + 1/Z5) · V1 = 0
A := (1/Z1 + 1/Z2 + 1/Z3)      Y := (E/Z1)
      - 1/Z3
      1/Z3 + 1/Z4 + 1/Z5
V := A · Y      V = (244,4239 + 57,8296 · i)
                  241,4685 + 20,125 · i
V1 := V_1      V2 := V_2      V1 = 244,4239 + 57,8296 · i
                  V2 = 241,4685 + 20,125 · i
I1 := E - V1/Z1      I1 = 8,7197 + 18,0057 · i
                  |I1| = 20,006      arg(I1); stop = 64,1604
I2 := V1/Z2      I2 = -2,8915 + 12,2212 · i
                  |I2| = 12,5586      arg(I2); stop = 103,3112
I3 := V1 - V2/Z3      I3 = 11,6111 + 5,7845 · i
                  |I3| = 12,9722      arg(I3); stop = 26,4819
I4 := V2/Z4      I4 = 6,5011 + 11,7639 · i
                  |I4| = 13,4407      arg(I4); stop = 61,0742
I5 := V2/Z5      I5 = 5,1102 - 5,9794 · i
                  |I5| = 7,8656      arg(I5); stop = -49,4819

```

Fig. 12. Programme for the alternating current circuit analysis – solution part 1 (Fig. 11)

Figure 12 and Fig. 13 show an example of a solution for alternating current electric circuit current (Fig. 11) with the following values: $E = 240e^{j30\text{deg}}$ V, $R_1 = 2 \Omega$, $x_1 = 3 \Omega$, $x_2 = 20 \Omega$, $R_3 = 1.5 \Omega$, $x_3 = 2.5 \Omega$, $x_4 = 15 \Omega$, $R_4 = 10 \Omega$, $R_5 = 18 \Omega$, $x_5 = 25 \Omega$.

```

SMATH Studio - [Zad_Poznan_N3.sm]
File Edit View Insert Calculation Tools Pages Help
Bilans mocy
Moc źródła
Sz := E · I1s
Sz = 3973,0316 - 2696,0595 · i
I1s = 8,7197 + 18,0057 · i
Moc odbiorników
So1 := |I1|2 · z1
So1 = 800,4763 + 1200,7144 · i
So2 := |I2|2 · z2
So2 = - 3154,3663 · i
So3 := |I3|2 · z3
So3 = 252,4186 + 420,6977 · i
So4 := |I4|2 · z4
So4 = 1806,5253 - 2709,7879 · i
So5 := |I5|2 · z5
So5 = 1113,6115 + 1546,6826 · i
So := So1 + So2 + So3 + So4 + So5
Sz = 3973,0316 - 2696,0595 · i
So = 3973,0316 - 2696,0595 · i
I1 = 8,7197 + 18,0057 · i
I2 = - 2,8915 + 12,2212 · i
I3 = 11,6111 + 5,7845 · i
I4 = 6,501 + 11,7639 · i
I5 = 5,1102 - 5,9794 · i

```

Fig. 13. Programme for the alternating current circuit analysis – solution part 2 (Fig. 11)

In the case when there is a condenser in the branches, a minus value should be entered for the imaginary part of the impedance. For the example presented in Fig. 11 the following data were entered in the programme: $E = 240e^{j30\text{deg}}$ V, $Z_1 = 2+j3 \Omega$; $Z_2 = 0-j20 \Omega$, $Z_3 = 1,5+j2,5 \Omega$, $Z_4 = 10-j15 \Omega$, $Z_5 = 18+j25 \Omega$ (in the SMATH programme the underscore is not used in the symbol of the complex number). The programme calculates the current in the branches and the apparent power absorbed by the circuit.

2.3. Analysis of a circuit with magnetic couplings

Figure 14 presents the structure of the alternating current circuit with magnetic couplings. Three coils were added in the circuit with reactance x_{s1} , x_{s2} , x_{s3} , respectively, between which magnetic couplings occur. Magnetic couplings are described by reactance of mutual induction x_{12} , x_{13} and x_{23} . When in the analysed circuit magnetic coupling does not occur between the coils, in the SMATH programme the value equal to zero for a given magnetic reactance should be entered (x_{12} , x_{13} or x_{23}). In order to solve a circuit with

magnetic coupling between the selected coils opposite to the one assumed in SMATH, the minus value for the magnetic reactance linked to mutual induction should be entered. It is convenient to solve the electric circuit of this type by replacing the subcircuit with magnetically coupled coils with an equivalent subcircuit without couplings [1]. The programme calculates the values of the induction reactance for the subcircuit without couplings, of the current in the branches and the power balance. Figure 15 presents an example of an electric circuit with magnetic couplings with the following parameters: $E = 240e^{j30\text{deg}} \text{ V}$, $x_1 = 4 \Omega$, $x_3 = 23 \Omega$, $R_4 = 20 \Omega$, $x_5 = 10 \Omega$, $x_{s1} = 20 \Omega$, $x_{s2} = 12 \Omega$, $x_{12} = 8 \Omega$.

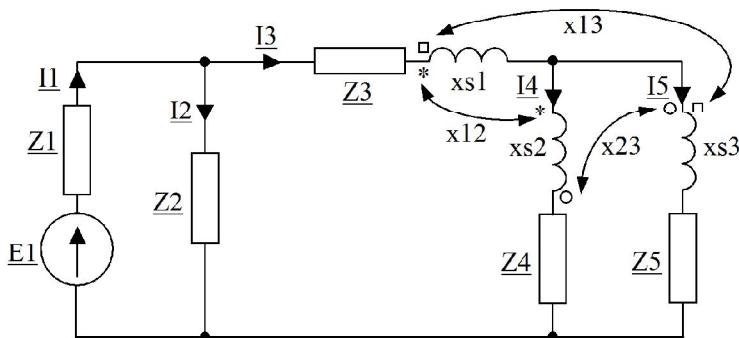


Fig. 14. Structure of a sample alternating current electric circuit with magnetic couplings

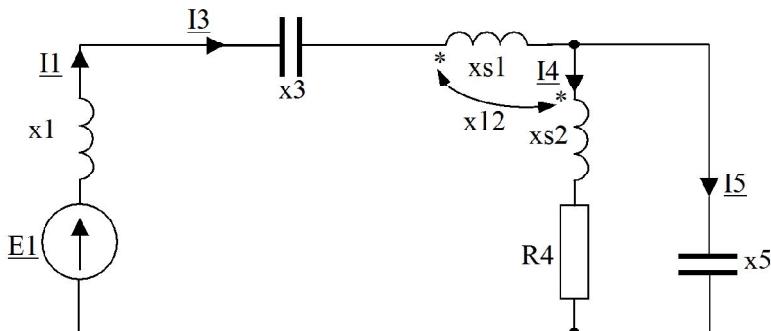


Fig. 15. Diagram of the alternating current electric circuit with magnetic couplings

There is no branch with impedance Z_2 in this circuit, whereas impedance Z_3 equals zero. In this case in the SMATH programme respective values $Z_2 = 10^{15} \Omega$ and $Z_3 = 10^{-6} \Omega$ were entered. Figure 16 and Fig. 17 present the results of calculations r in the SMATH programme. The following data were entered in the programme: $E = 240e^{j30\text{deg}} \text{ V}$, $Z_1 = 0+j4 \Omega$; $Z_2 = 10^{15} \Omega$, $Z_3 = 10^{-4}-j23 \Omega$, $Z_4 = 20-j0 \Omega$, $Z_5 = 0-j10 \Omega$, $x_{s1} = 20 \Omega$, $x_{s2} = 12 \Omega$,

$x_{S3} = 0 \Omega$, $x_{12} = 8 \Omega$, $x_{13} = 0 \Omega$, $x_{23} = 0 \Omega$. After an equivalent subcircuit without magnetic couplings is introduced, resonance of voltages can occur in the branches. If such a branch does not include a resistance element, then the programme sends the divide-by-zero error message. In order to ensure the universal character of the programme solving the circuit, additional impedance $Z_{LC} = 10^{-6} \Omega$ in each branch with reactance x_{S1} , x_{S2} and x_{S3} (Fig. 16) was entered in the equations.

```

S Math Studio - [Zad_Poznan_N4.sm]
File Edit View Insert Calculation Tools Pages Help
j := √(-1)      rad := π / 180      stop := 180 / π
E := 240 · e^(j · 30 · rad)      E := 207,846097 + 120 · i
xS1 := 20      xS2 := 12      xS3 := 30
x12 := 8      x13 := -5      x23 := 0
xa := xS1 + x12 + x13 + x23      xa = 23
xb := xS2 + x12 - x13 - x23      xb = 25
xc := xS3 + x13 - x12 - x23      xc = 17
+
z1 := 0 + j · 4      z2 := 10^(15)
z3 := 10^(-4) - j · 23      z4 := 20 - j · 0      z5 := 0 - j · 10      ZLC := 10^(-6)

v1 := (1/z1 + 1/z2 + 1/(z3 + j · xa)) - (V2 / (z3 + j · xa)) = E/z1
v2 := (1/(z3 + j · xa) + 1/(z4 + j · xb) + 1/(z5 + j · xc)) - (V1 / (z3 + j · xa)) = 0
A := (1/z1 + 1/z2 + 1/(z3 + j · xa + ZLC)      -1/(z3 + j · xa + ZLC)
      -1/(z3 + j · xa + ZLC)      1/(z3 + j · xa + ZLC) + 1/(z4 + j · xb + ZLC) + 1/(z5 + j · xc + ZLC))
      Y := (E/z1
            0)
V := A^-1 · Y
V1 := V[1]      V1 = 127,617945 + 65,9311 · i
V2 := V[2]      V2 = 127,61658 + 65,933125 · i
I1 := (E - V1) / z1      I1 = 13,517225 - 20,057038 · i | I1 | = 24,186776 arg(I1 · stop) = -0,977776
I2 := V1 / z2      I2 = 1,276179 · 10^(-13) + 6,59311 · 10^(-14) · i
      | I2 | = 1,436428 · 10^(-13)      arg(I2 · stop) = 0,476862
I3 := V1 - V2 / (z3 + j · xa + ZLC)

```

Fig. 16. Programme for the analysis of a circuit with magnetic couplings – part 1 (Fig. 15)

```

SMath Studio - [Zad_Poznan_N4.sm]
File Edit View Insert Calculation Tools Pages Help
I3=13,517225-20,057038.i |I3|=24,186776 arg(I3.stop)=-0,977776
I4= V2
Z4+j·xb+ZLC
I4=4,098205-1,826099.i |I4|=4,486638 arg(I4.stop)=-0,419177
I5= V2
Z5+j·xc+ZLC
I5=9,419021-18,230939.i |I5|=20,520357 arg(I5.stop)=-1,093917
spr_I PK
I1-I2-I3=5,20663·10^-11 + 1,38174·10^-10·i
I3-I4-I5=-2,138841·10^-15 - 3,101319·10^-15·i
Bilans mocy
I1s=|I1|·e^{-j·arg(I1)}
Moc źródła
Sz=E·I1s
Sz=402,657919+5790,844071·i
Moc odbiorników
So1=|I1|^2·Z1
So1=2340,000587·i
So2=|I2|^2·Z2
So2=2,063325·10^-11
So3=|I3|^2·(Z3+j·xa)
So3=0,0585
So4=|I4|^2·(Z4+j·xb)
So4=402,598393+503,247991·i
So5=|I5|^2·(Z5+j·xc)
So5=2947,595493·i
So=So1+So2+So3+So4+So5
So=402,656893+5790,844071·i
I1=13,517225-20,057038.i
I2=1,276179·10^-13 + 6,59311·10^-14·i
I3=13,517225-20,057038.i
I4=4,098205-1,826099.i
I5=9,419021-18,230939.i
Sz=402,657919+5790,844071·i
So=402,656893+5790,844071·i

```

Fig. 17. Programme for the analysis of a circuit with magnetic couplings – part 2 (Fig. 15)

3. Summary

The use of computers in the teaching process allows to improve learning capacity. The SMATH programme is a good educational tool, that helps to teach the students to perform analysis of electric circuits. The user, having numerous programmes developed in SMART at his/her disposal, which make it possible to solve circuits of set topology, has the possibility to create his/her own electric schemes and to verify the results of his/her calculations against numeric results. It is also a highly useful educational tool for the teachers.

References

- [1] Bolkowski S., *Elektrotechnika Teoretyczna. Teoria obwodów elektrycznych*, vol. 1, WSiP, Warszawa, 2005, ISBN 978-83-02-09397-5.
- [2] www.smath.com

(Received: 14. 11. 2016, revised: 15. 11. 2016)