

Theoretical and mathematical models of the torque of mechanical losses in a hydraulic rotational motor for hydrostatic drive

Zygmunt Paszota, Prof.
Gdansk University of Technology

Abstract



The paper presents theoretical and mathematical models of the torque of mechanical losses in a hydraulic rotational motor with constant capacity q_{Mt} per one shaft revolution (with constant theoretical working volume V_{Mt}) and with variable capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution (with variable geometrical working volume V_{Mgv}). The models are to be used in the laboratory and simulation investigations of motor energy losses aimed at evaluation of the motor energy efficiency and hydrostatic drive efficiency.

Keywords: hydrostatic drive; hydraulic motor; energy efficiency

INTRODUCTION

The paper is a continuation of references [1÷10], aimed at developing a method of evaluation of the losses and energy efficiency of the hydrostatic drives and displacement machines used in them. The method is based on the theoretical and mathematical descriptions of losses in the pumps, hydraulic motors and in other elements of a hydrostatic drive system.

Description of the hydraulic motor losses and energy efficiency is based on the diagram of the direction of increasing power stream in a rotational hydraulic motor, which is introduced instead of the Sankey diagram (Fig.1 [10]).

The aim of the paper is to present theoretical and mathematical models of torque of mechanical losses in the rotational hydraulic motor „shaft – working chambers” assembly. The motor is a displacement machine with constant theoretical capacity q_{Mt} per one shaft revolution (with constant motor theoretical working volume V_{Mt}) or with variable geometrical capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution (with variable motor geometrical working volume V_{Mgv}).

The models are to be used in the laboratory and simulation investigation of the motor energy losses, motor energy efficiency and hydrostatic drive efficiency.

THEORETICAL MODELS OF THE TORQUE M_{Mi} OF MECHANICAL LOSSES IN THE MOTOR „SHAFT – WORKING CHAMBERS” ASSEMBLY

Torque M_{Mi} indicated in the rotational hydraulic motor working chambers must be greater than torque M_M loading the motor shaft (torque required by the driven machine (device)) because of the necessity of balancing also the

torque M_{Mm} of mechanical losses in the „shaft – working chambers” assembly. The assembly connects the shaft with working chambers, forms the working chambers and changes their capacity. Therefore, the torque M_{Mi} indicated in the motor working chambers is a sum of torque M_M loading the shaft and of torque M_{Mm} of mechanical losses:

$$M_{Mi} = M_M + M_{Mm} \quad (1)$$

Torque M_{Mm} of mechanical losses in a rotational hydraulic motor with variable geometrical capacity q_{Mgv} per one shaft revolution is, with maximum value of q_{Mgv} , i.e. with $q_{Mgv} = q_{Mt}$ (with coefficient $b_M = q_{Mgv}/q_{Mt} = 1$), equal to the torque of mechanical losses in the motor working with constant theoretical capacity q_{Mt} per one shaft revolution. The theoretical and mathematical models describing the torque M_{Mm} of mechanical losses in the „shaft – working chambers” assembly of a motor with variable capacity q_{Mgv} per one shaft revolution (with variable b_M coefficient) may be described with reference to models of the torque M_{Mm} of mechanical losses in the assembly of a motor with constant capacity q_{Mt} per one shaft revolution (with $b_M = 1$).

Torque M_{Mm} of mechanical losses in a rotational hydraulic motor is mainly an effect of friction forces between elements of the „shaft – working chambers” assembly, dependent, among others, on the torque M_M loading the shaft.

Friction forces between the elements of the „shaft – working chambers” assembly are, to some extent, an effect of loading those elements by inertia forces from the rotational and reciprocating motion, dependent on the shaft rotational speed n_M and on the motor capacity q_{Mgv} per one shaft revolution (b_M coefficient).

There are also friction forces between the „shaft – working chambers” assembly elements and the working fluid, dependent on the fluid viscosity ν and on the shaft rotational speed n_M and also on the motor capacity q_{Mgv} per one shaft revolution (b_M coefficient). The impact of working fluid viscosity ν on the friction forces between elements of the „shaft – working chambers” assembly and the working fluid is visible mainly in the piston hydraulic motors with casing filled with fluid.

Torque M_M loading the motor shaft and the shaft rotational speed n_M required by the driven machine (device) change in the ($0 \leq \bar{\omega}_M < \bar{\omega}_{Mmax}$, $0 \leq \bar{M}_M < \bar{M}_{Mmax}$) hydrostatic drive operating range. The kinematic viscosity ν of working fluid (hydraulic oil, oil – water emulsion) changes in the $\nu_{min} \leq \nu \leq \nu_{max}$ range.

M_M , n_M and ν are parameters independent of the motor and of the losses in that motor. In models applied to motor with variable capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution, the change of q_{Mgv} (b_M) is assumed in the $0 \leq q_{Mgv} \leq q_{Mt}$ ($0 \leq b_M \leq 1$) range, although in fact b_{Mmin} is of the $0.2 \div 0.3$ order.

Torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses in a hydraulic motor operating with torque M_M and speed n_M required by the driven machine (device) (the motor having capacity q_{Mgv} per one shaft revolution (b_M coefficient) and fed with working fluid of viscosity ν) can be described as a sum of torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ and increase $\Delta M_{Mm|M_M=0, n_M, b_M, \nu}$; torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses occurs in an unloaded motor (when the torque M_M required of the motor is equal to zero – $M_M = 0$) and the increase $\Delta M_{Mm|M_M=0, n_M, b_M, \nu}$ of the torque of mechanical losses is an effect of loading the „shaft – working chambers” assembly elements by the increasing shaft loading torque M_M :

$$\Delta M_{Mm|M_M=0, n_M, b_M, \nu} = M_{Mm|M_M=0, n_M, b_M, \nu} + \Delta M_{Mm|M_M=0, n_M, b_M, \nu} \quad (2)$$

In constructing the theoretical and mathematical models describing the torque $\Delta M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses in a rotational hydraulic motor, an assumption is made that the increase $\Delta M_{Mm|M_M=0, n_M, b_M, \nu}$ of the torque of the mechanical losses in the „shaft – working chambers” assembly, as an effect of the increasing required torque M_M loading the motor shaft, is practically independent of:

- required shaft rotational speed n_M ,
- value of the $b_M = q_{Mgv}/q_{Mt}$ coefficient of capacity per one shaft revolution,
- working fluid viscosity ν .

An assumption was also made in the proposed models, that increase $\Delta M_{Mm|M_M=0, n_M, b_M, \nu}$ of the torque of the mechanical losses is determined at the speed $n_M = n_{Mt}$ i.e. equal to the motor shaft theoretical speed, at the coefficient $b_M = 1$ (with $q_{Mgv} = q_{Mt}$) and at $\nu = \nu_n$ i.e. working fluid reference viscosity ν_n :

$$\begin{aligned} \Delta M_{Mm|M_M=0, n_M, b_M, \nu} &= f(M_M) = \\ &= \Delta M_{Mm|M_M=0, n_{Mt}, b_M=1, \nu_n} \sim M_M \end{aligned} \quad (3)$$

In constructing the theoretical and mathematical models describing the torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses in the „shaft – working chambers” assembly it was also assumed that:

- the impact of required shaft rotational speed n_M and value of the coefficient $b_M = q_{Mgv}/q_{Mt}$ on the load of the assembly elements with inertia forces,
- the impact of working fluid viscosity ν , n_M and b_M on the friction forces between elements and working fluid,

in consequence, the impact of n_M , b_M and ν on the torque M_{Mm} of mechanical losses in the motor can be determined with the shaft loading torque equal to zero ($M_M = 0$), because the inertia forces of the assembly elements and friction forces between the elements and working fluid are independent of the torque M_M loading the motor shaft:

$$M_{Mm|M_M=0, n_M, b_M, \nu} = f(n_M, b_M, \nu) \quad (4)$$

The above mentioned assumptions allow to describe the torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses in the „shaft – working chambers” assembly by a theoretical model in the form:

$$\begin{aligned} M_{Mm|M_M=0, n_M, b_M, \nu} &= M_{Mm|M_M=0, n_M, b_M, \nu} + \\ &+ \Delta M_{Mm|M_M=0, n_M, b_M=1, \nu_n} \end{aligned} \quad (5)$$

In a hydraulic motor with theoretical (constant) capacity q_{Mt} per one shaft revolution ($b_M = 1$), operating with theoretical (constant) shaft rotational speed n_{Mt} and the working fluid reference (constant) viscosity ν_n , the theoretical model describing the torque of mechanical losses in the assembly takes the form (Fig.1):

$$\begin{aligned} M_{Mm|M_M=0, n_M, b_M=1, \nu_n} &= M_{Mm|M_M=0, n_{Mt}, b_M=1, \nu_n} + \\ &+ \Delta M_{Mm|M_M=0, n_M, b_M=1, \nu_n} \end{aligned} \quad (6)$$

The impact of inertia forces of the „shaft – working chambers” assembly elements performing the rotational and reciprocating motion on the torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses in an unloaded motor may be presented as a function of the motor shaft rotational speed n_M and as a function of geometrical capacity q_{Mgv} (b_M coefficient) per one shaft revolution.

The impact of the friction forces between the „shaft – working chambers” assembly elements and the working fluid on the torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of the mechanical losses in an unloaded motor may be presented as a function of the working fluid viscosity ν and as a function of the motor shaft rotational speed n_M and of the capacity q_{Mgv} (coefficient b_M) per one shaft revolution.

The proposed theoretical models describing the torque $M_{Mm|M_M=0, n_M, b_M, \nu}$ of mechanical losses in the „shaft – working chambers” assembly of an unloaded hydraulic motor (with torque $M_M = 0$), with changing shaft speed n_M , with theoretical (constant) capacity q_{Mt} ($b_M = 1$) or geometrical (variable) capacity q_{Mgv} (b_M) of the motor per one shaft revolution and with changing working fluid viscosity ν , take the form:

- in a hydraulic motor with theoretical (constant) capacity q_{Mt} ($b_M = 1$) per one shaft revolution (Fig. 2):

$$\begin{aligned} M_{Mm|M_M=0, n_M, b_M=1, \nu} &= M_{Mm|M_M=0, n_M, b_M=1, \nu_n} \left(\frac{\nu}{\nu_n} \right)^{a_{vm}} = \\ &= (M_{Mm|M_M=0, n_M=0, b_M=1, \nu_n} + \Delta M_{Mm|M_M=0, n_M, b_M=1, \nu_n}) \left(\frac{\nu}{\nu_n} \right)^{a_{vm}} \end{aligned} \quad (7)$$

where:

$$\begin{aligned} \Delta M_{Mm|M_M=0, n_M=b_M=1, v_n} &= M_{Mm|M_M=0, n_M=b_M=1, v_n} + \\ &- M_{Mm|M_M=0, n_M=0, b_M=1, v_n} = \end{aligned} \quad (8)$$

$$= (M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n}) \frac{n_M}{n_{Mt}}$$

- in a hydraulic motor with geometrical (variable) capacity q_{Mgv} ($q_{Mgv} = b_M q_{Mt}$) per one shaft revolution (Fig. 5):

$$\begin{aligned} M_{Mm|M_M=0, n_M, b_M, v} &= M_{Mm|M_M=0, n_M, b_M, v_n} \left(\frac{v}{v_n} \right)^{a_{vm}} \\ &= (M_{Mm|M_M=0, n_M=0, b_M=0, v_n} + \Delta M_{Mm|M_M=0, n_M, b_M, v_n}) \left(\frac{v}{v_n} \right)^{a_{vm}} \quad (9) \\ &= (M_{Mm|M_M=0, n_M=0, b_M=1, v_n} + \Delta M_{Mm|M_M=0, n_M, b_M, v_n}) \left(\frac{v}{v_n} \right)^{a_{vm}} \end{aligned}$$

where:

$$\begin{aligned} \Delta M_{Mm|M_M=0, n_M, b_M, v_n} &= M_{Mm|M_M=0, n_M, b_M, v_n} + \\ &- M_{Mm|M_M=0, n_M=0, b_M=0, v_n} = \end{aligned} \quad (10)$$

$$= M_{Mm|M_M=0, n_M, b_M, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n} =$$

$$= (M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n}) \frac{n_M}{n_{Mt}} b_M$$

It is assumed in expressions (9) and (10) that the torque $M_{Mm|M_M=0, n_M=0, b_M, v_n}$ of mechanical losses in the „shaft – working chambers” assembly of an unloaded hydraulic motor ($M_M = 0$) with geometrical (variable) capacity q_{Mgv} ($q_{Mgv} = b_M q_{Mt}$) per one shaft revolution and with zero shaft rotational speed ($n_M = 0$) is practically independent of the coefficient b_M of capacity per one shaft revolution and can be determined for $b_M = 1$. Therefore the following simplifying assumption is accepted:

$$\begin{aligned} M_{Mm|M_M=0, n_M=0, b_M=0, v_n} &= M_{Mm|M_M=0, n_M=0, b_M, v_n} = \\ &= M_{Mm|M_M=0, n_M=0, b_M=1, v_n} \end{aligned}$$

In effect, the proposed **theoretical models describing the torque M_{Mm} of mechanical losses in a hydraulic rotational motor** take the forms:

- in a hydraulic motor with theoretical (constant) capacity q_{Mt} ($b_M = 1$) per one shaft revolution (Fig. 3):

$$\begin{aligned} M_{Mm|M_M, n_M, b_M=1, v} &= \left[M_{Mm|M_M=0, n_M=0, b_M=1, v_n} + (M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n}) \frac{n_M}{n_{Mt}} \right] \left(\frac{v}{v_n} \right)^{a_{vm}} \\ &+ (M_{Mm|M_M=M_{Mt}, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n}) \frac{M_M}{M_{Mt}} \end{aligned} \quad (13)$$

- in a hydraulic motor with geometrical (variable) capacity q_{Mgv} ($q_{Mgv} = b_M q_{Mt}$) per one shaft revolution (Fig. 4 – with n_{Mt} , v_n , Fig. 6 – with v_{min} , v_n , v_{max}):

$$\begin{aligned} M_{Mm|M_M, n_M, b_M, v} &= \left[M_{Mm|M_M=0, n_M=0, b_M=1, v_n} + (M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n}) \frac{n_M}{n_{Mt}} b_M \right] \left(\frac{v}{v_n} \right)^{a_{vm}} \\ &+ (M_{Mm|M_M=M_{Mt}, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n}) \frac{M_M}{M_{Mt}} \end{aligned} \quad (14)$$

In models describing the torque of mechanical losses in a rotational hydraulic motor, used for description of losses and energy efficiency of the motor and of the hydrostatic transmission system in the ($0 \leq \overline{\omega}_M < \overline{\omega}_{Mmax}$, $0 \leq \overline{M}_M < \overline{M}_{Mmax}$) operating field, the increase of torque of mechanical losses occurring in fact at the motor speed n_M approaching the zero value ($n_M = 0$) is not taken into account. That increase occurs below the shaft critical speed n_{Mcr} . The motor rotational speed instability δn_M increases below the critical speed n_{Mcr} and in effect the torque M_{Mm} of mechanical losses in the „shaft – working chambers” assembly increases. Assessment of the value of torque $M_{Mm|M_M=0, n_M=0, b_M, v_n}$ of mechanical losses in a motor with zero rotational speed n_M ($n_M = 0$) is done by approximation of the function $M_{Mm|M_M=0, n_M, b_M, v_n} = f(n_M)$ at $n_M = 0$.

Exponent a_{vm} in expressions (7) and (9) determines the impact of the ratio v/v_n of viscosity v to the reference viscosity $v_n = 35 \text{ mm}^2 \text{ s}^{-1}$ of the working fluid on the value of torque of mechanical losses. The impact occurs mainly in a piston displacement machines with fluid filling the casing (in pumps and hydraulic motors).

The proposed **theoretical model of the increase of torque $\Delta M_{Mm|M_M, n_M, b_M, v}$ of mechanical losses in a rotational hydraulic motor, the increase resulting from loading the motor shaft with torque M_M , takes the same form in the case of a motor with theoretical (constant) capacity q_{Mt} per one shaft revolution ($b_M = 1$) and in the case of a motor with geometrical (variable) capacity q_{Mgv} per one shaft revolution ($q_{Mgv} = b_M q_{Mt}$):**

- in a hydraulic motor with theoretical (constant) capacity q_{Mt} ($b_M = 1$) per one shaft revolution (Fig. 1 and 3):

$$\begin{aligned} \Delta M_{Mm|M_M, n_M, b_M=1, v} &= \end{aligned} \quad (11)$$

$$= (M_{Mm|M_M=M_{Mt}, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n}) \frac{M_M}{M_{Mt}}$$

- in a hydraulic motor with geometrical (variable) capacity q_{Mgv} ($q_{Mgv} = b_M q_{Mt}$) per one shaft revolution (Fig. 4 and 5):

$$\begin{aligned} \Delta M_{Mm|M_M, n_M, b_M, v} &= \end{aligned} \quad (12)$$

$$= (M_{Mm|M_M=M_{Mt}, n_M=n_{Mt}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=n_{Mt}, b_M=1, v_n}) \frac{M_M}{M_{Mt}}$$

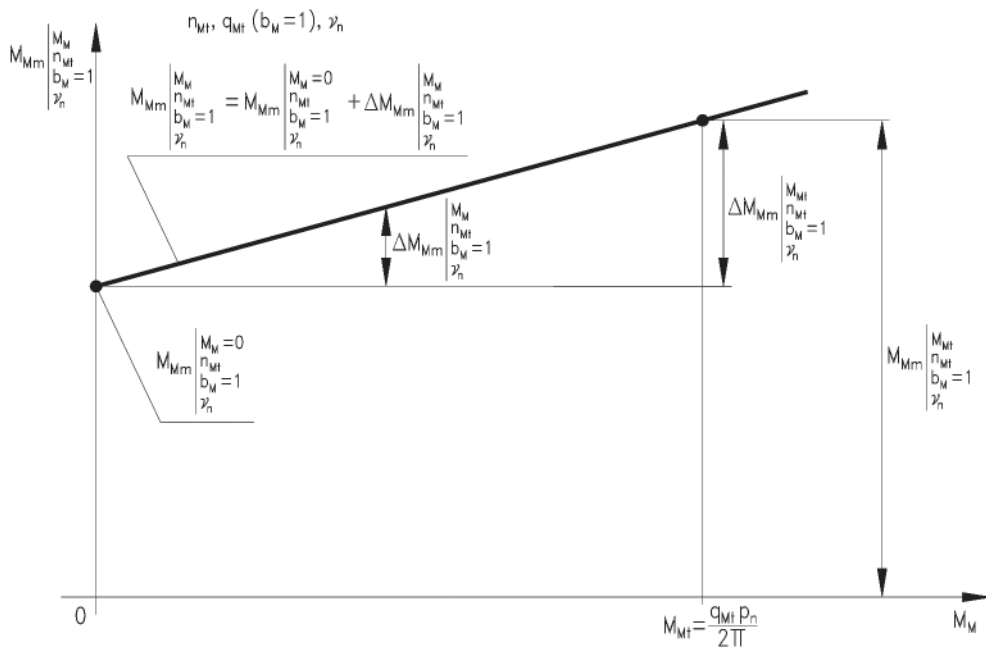


Fig. 1. Torque $M_{Mm|M_M=n_M, n_{Mt}=1, v_n}$ of mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with constant capacity q_{Mt} per one shaft revolution ($b_M = 1$), at the shaft theoretical rotational speed n_{Mt} and at the working fluid reference viscosity v_n , as a function of the motor shaft torque M_M – graphical interpretation of the theoretical model (6)

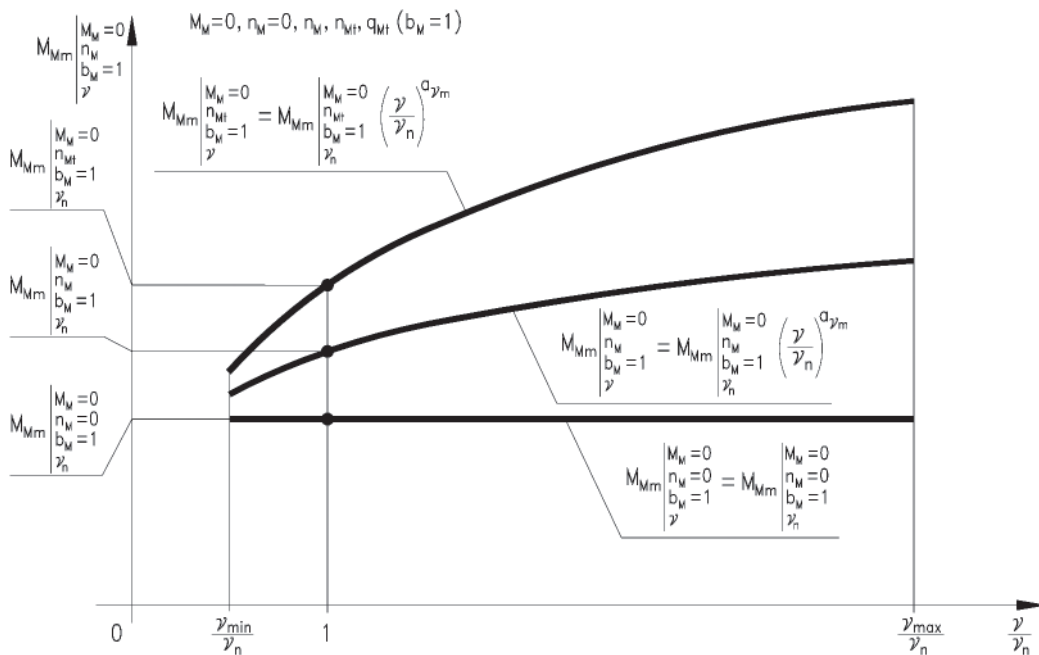


Fig. 2. Torque $M_{Mm|M_M=0, n_M=0, n_{Mt}=1, v_n}$ of mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with constant capacity q_{Mt} per one shaft revolution ($b_M = 1$), at shaft torque $M_M = 0$, as a function of the ratio v/v_n of viscosity v to the working fluid reference viscosity v_n – graphical interpretation of the theoretical models (7) and (8); motor shaft speeds: $n_M = 0, n_M, n_{Mt}$. The impact of working fluid viscosity v on friction forces between the „shaft – working chambers” assembly elements and the working fluid occurs mainly in the piston hydraulic motors with casing filled with the working fluid.

MATHEMATICAL MODELS OF THE TORQUE OF MECHANICAL LOSSES

In mathematical models describing the torque M_{Mm} of mechanical losses in a hydraulic rotational motor coefficients k_i of losses are used relating (comparing) the components describing the torque M_{Mm} of losses in theoretical models to the following reference values:

- theoretical torque $M_{Mt} = \frac{q_{Mt} p_n}{2 \Pi}$ of a hydraulic motor with theoretical (constant) capacity q_{Mt} per one shaft resolution, determined at the decrease of Δp_M of pressure in the motor

equal to the system nominal pressure p_n ($\Delta p_M = p_n$) and with assumption that there are no pressure and mechanical losses in the motor,

- theoretical rotational speed n_{Mt} of a hydraulic motor with constant capacity q_{Mt} per one shaft revolution resulting from the motor capacity Q_M equal to the theoretical pump Q_{Pt} ($n_{Mt} = \frac{Q_{Pt}}{q_{Mt}}$),
- theoretical capacity Q_{Pt} of the hydraulic motor driving pump – a product of the theoretical capacity q_{Pt} per one shaft revolution of the constant capacity pump and the shaft speed n_{p0} of an unloaded pump ($Q_{Pt} = q_{Pt} n_{p0}$).

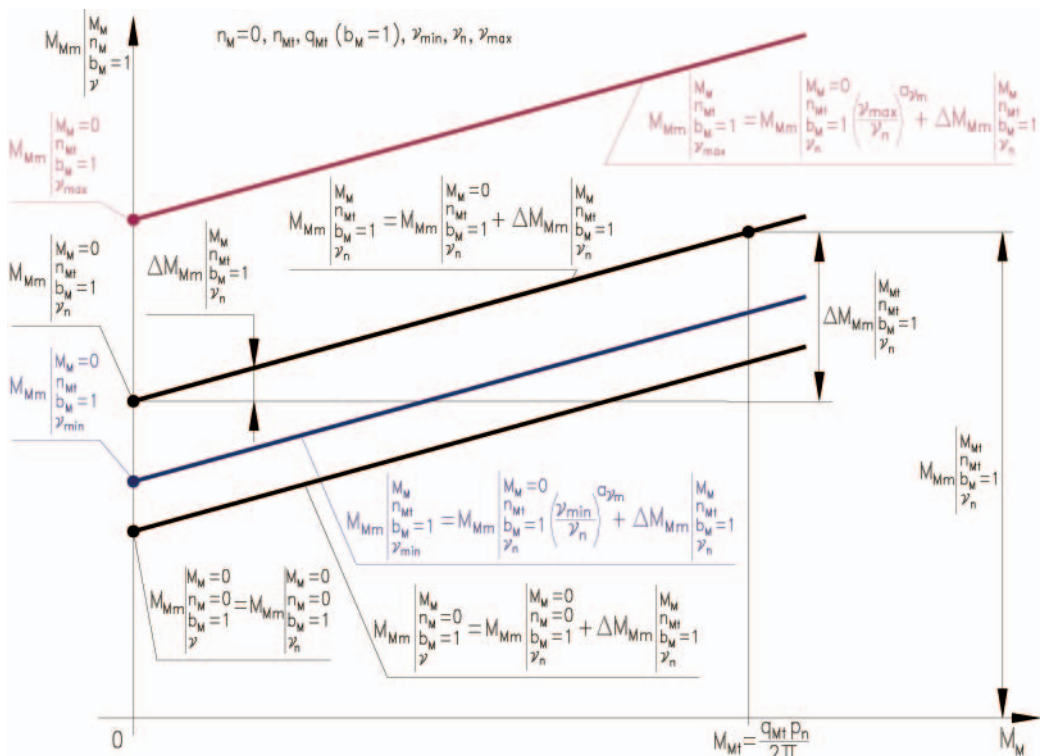


Fig. 3. Torque $M_{Mm|n_Mt, n_M, b_M=1, \gamma}$ of m mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with constant capacity q_{Mt} per one shaft revolution ($b_M=1$), as a function of the motor shaft torque M_M – graphical interpretation of the theoretical model (13); motor shaft speeds: theoretical speed n_{Mt} , $n_M=0$; working fluid viscosity ν_{min} , ν_n and ν_{max} . The impact of working fluid viscosity ν on friction forces between the „shaft – working chambers” assembly elements and the working fluid occurs mainly in the piston hydraulic motors with casing filled with the working fluid.

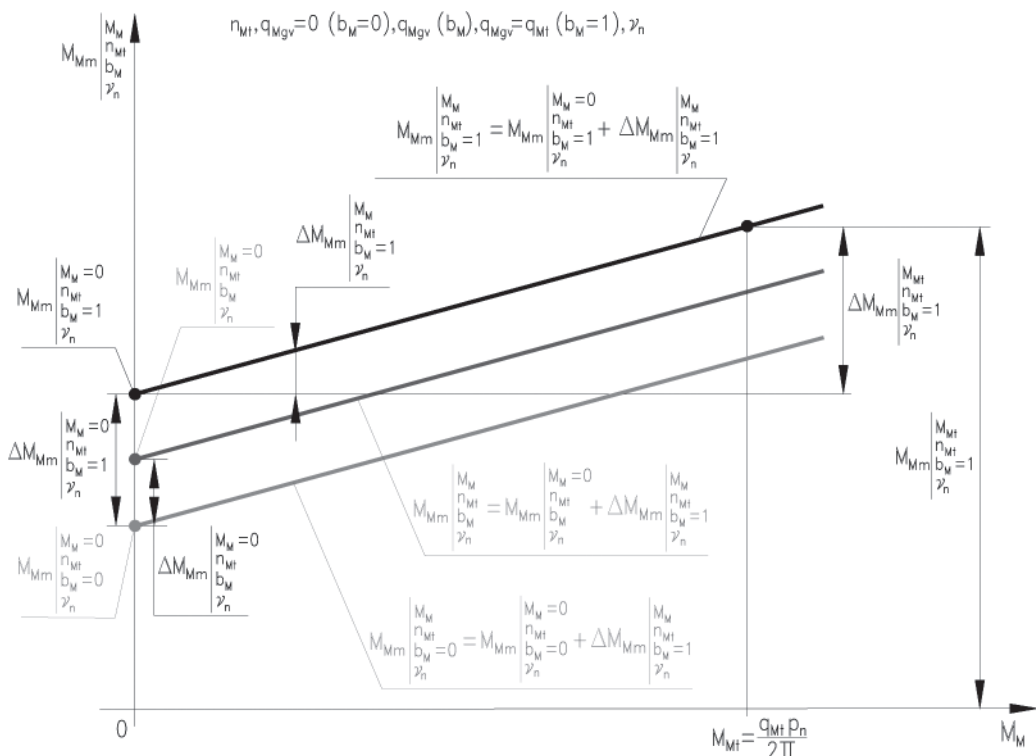


Fig. 4. Torque $M_{Mm|n_Mt, n_M, b_M, \nu}$ of mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with variable capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution, at theoretical shaft rotational speed n_{Mt} and at working fluid reference viscosity ν_n , as a function of the motor shaft torque M_M – graphical interpretation of the theoretical model (14); capacity q_{Mgv} per one shaft revolution (coefficient b_M of the change of capacity per one shaft revolution): $q_{Mgv}=0$ ($b_M=0$), $q_{Mgv}(b_M)$, $q_{Mgv}=q_{Mt}$ ($b_M=1$)

Theoretical and mathematical models describe the torque M_{Mm} of mechanical losses in a rotational hydraulic motor with theoretical (constant) capacity q_{Mt} per one shaft revolution or with geometrical (variable) capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution:

– $q_{Mt} = q_{M|\Delta p_{Mfi}=0, p_{M2i}=0, \nu_n}$ is a theoretical capacity per one shaft resolution of a constant capacity motor, determined at $\Delta p_{Mfi} = 0$, $p_{M2i} = 0$ and ν_n , which is equal to the theoretical active volume of the working chambers during one shaft revolution,

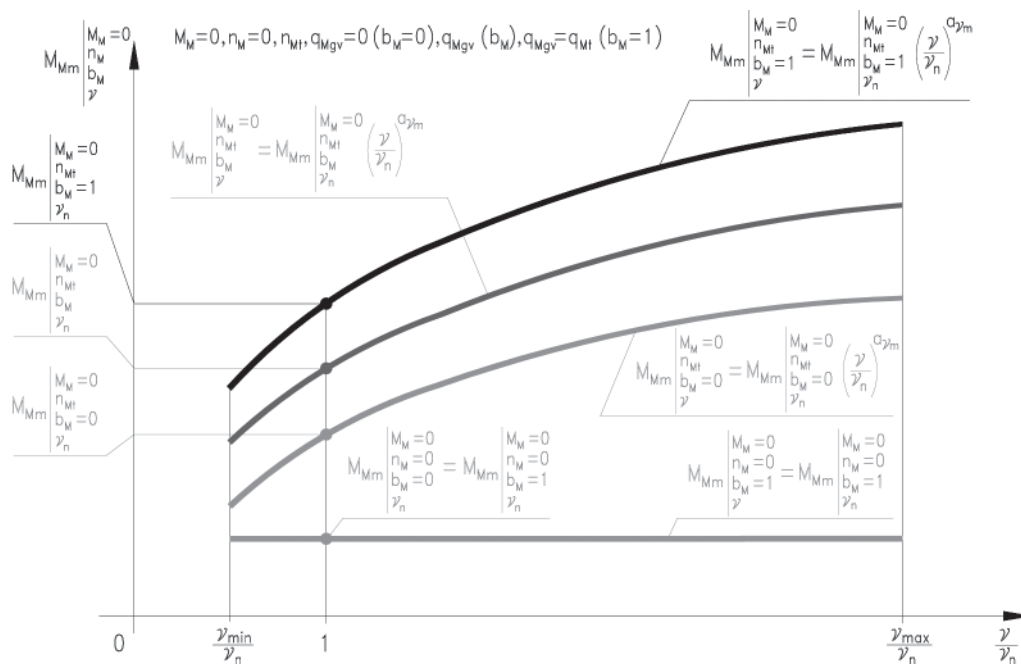


Fig. 5. Torque $M_{Mm|M_M=0, n_M=0, \gamma_n=0, q_{Mgv}=0 (b_M=0), q_{Mgv}=q_{Mt} (b_M=1)}$ of mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with variable capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution, at the shaft torque $M_M = 0$ as a function of the ratio v/v_n of viscosity v to the working fluid reference viscosity v_n – graphical interpretation of the theoretical models (9) and (10); motor shaft speeds: theoretical speed $n_M, n_M = 0$; capacity q_{Mgv} per one shaft revolution (coefficient b_M of the change of capacity per one shaft revolution): $q_{Mgv} = 0 (b_M = 0), q_{Mgv} = (b_M) q_{Mt}, q_{Mgv} = q_{Mt} (b_M = 1)$. The impact of working fluid viscosity v on friction forces between the „shaft – working chambers” assembly elements and the working fluid occurs mainly in the piston hydraulic motors with casing filled with the working fluid.

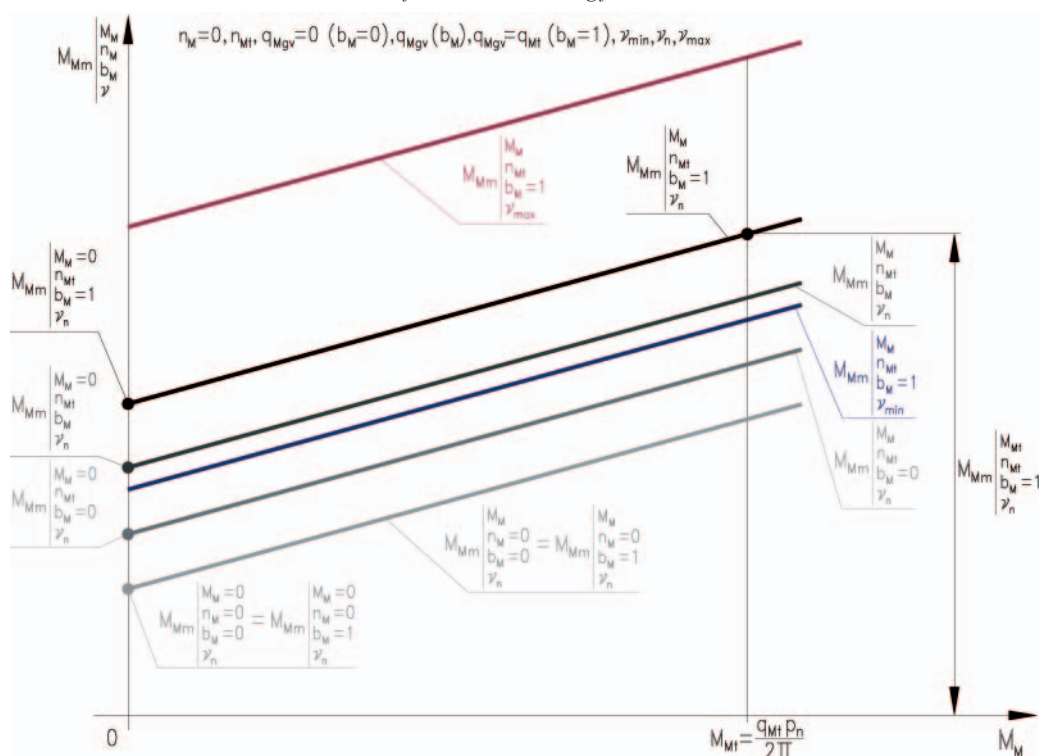


Fig. 6. Torque $M_{Mm|M_M=0, n_M=0, \gamma_n=0, q_{Mgv}=0 (b_M=0), q_{Mgv}=q_{Mt} (b_M=1)}$ of mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with variable capacity $q_{Mgv} = b_M q_{Mt}$ per one shaft revolution as a function of the motor shaft torque M_M – graphical interpretation of the theoretical model (14); motor shaft speeds: theoretical speed $n_M, n_M = 0$; capacity q_{Mgv} per one shaft revolution (coefficient b_M of the change of capacity per one shaft revolution): $q_{Mgv} = 0 (b_M = 0), q_{Mgv} = (b_M) q_{Mt}, q_{Mgv} = q_{Mt} (b_M = 1)$. The impact of working fluid viscosity v on friction forces between the „shaft – working chambers” assembly elements and the working fluid occurs mainly in the piston hydraulic motors with casing filled with the working fluid

– $q_{Mgv} = b_M q_{Mt}$ is a geometrical capacity per one shaft revolution of a variable capacity motor, determined at $\Delta p_{Mi} = 0, p_{M2i} = 0$ and v_n , which is equal to the geometrical active volume of the working chambers during one shaft revolution. In developing the models it is assumed that capacity q_{Mgv} per one hydraulic motor shaft revolution changes in the $0 \leq q_{Mgv} \leq q_{Mt}$ range and coefficient $b_M = q_{Mgv}/q_{Mt}$

of the variation of capacity per one motor shaft revolution changes in the $0 \leq b_M \leq 1$ range.

The proposed mathematical models describing the torque M_{Mm} of mechanical losses in the „shaft – working chambers” assembly, related to the theoretical models of the torque of mechanical losses, take the form:

- in a hydraulic motor with theoretical (constant) capacity q_{M_t} ($b_M = 1$) per one shaft revolution [referring to theoretical model (13)]:

$$M_{Mm|M_M, n_M, b_M=1, v} = \left(k_{7.1.1} + k_{7.1.2} \frac{n_M}{n_{M_t}} \right) M_{M_t} \left(\frac{v}{v_n} \right)^{a_{vm}} + k_{7.2} M_M = \left(k_{7.1.1} + k_{7.1.2} \frac{n_M}{n_{M_t}} \right) \frac{q_{M_t} p_n}{2\Pi} \left(\frac{v}{v_n} \right)^{a_{vm}} + k_{7.2} M_M \quad (15)$$

where:

$$k_{7.1.1} = \frac{M_{Mm|M_M=0, n_M=0, b_M=1, v_n}}{M_{M_t}} = \frac{M_{Mm|M_M=0, n_M=0, b_M=1, v_n}}{\frac{q_{M_t} p_n}{2\Pi}} \quad (16)$$

$$k_{7.1.2} = \frac{M_{Mm|M_M=0, n_M=n_{M_t}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n}}{M_{M_t}} \quad (17)$$

$$= \frac{M_{Mm|M_M=0, n_M=n_{M_t}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=0, b_M=1, v_n}}{\frac{q_{M_t} p_n}{2\Pi}}$$

$$k_{7.2} = \frac{M_{Mm|M_M=M_{M_t}, n_M=n_{M_t}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=n_{M_t}, b_M=1, v_n}}{M_{M_t}} \quad (18)$$

$$= \frac{M_{Mm|M_M=M_{M_t}, n_M=n_{M_t}, b_M=1, v_n} - M_{Mm|M_M=0, n_M=n_{M_t}, b_M=1, v_n}}{\frac{q_{M_t} p_n}{2\Pi}}$$

- in a hydraulic motor with geometrical (variable) capacity $q_{M_{gv}}$ ($q_{M_{gv}} = b_M q_{M_t}$) per one shaft revolution [referring to theoretical model (14)]:

$$M_{Mm|M_M, n_M, b_M, v} = \left(k_{7.1.1} + k_{7.1.2} \frac{n_M}{n_{M_t}} b_M \right) M_{M_t} \left(\frac{v}{v_n} \right)^{a_{vm}} + k_{7.2} M_M = \left(k_{7.1.1} + k_{7.1.2} \frac{n_M}{n_{M_t}} b_M \right) \frac{q_{M_t} p_n}{2\Pi} \left(\frac{v}{v_n} \right)^{a_{vm}} + k_{7.2} M_M \quad (19)$$

where: coefficient $k_{7.1.1}$ is described by expression (16), coefficient $k_{7.1.2}$ – by expression (17), coefficient $k_{7.2}$ – by expression (18).

CONCLUSIONS

1. Theoretical and mathematical models have been developed of the torque M_{Mm} of mechanical losses in the „shaft – working chambers” assembly of a rotational hydraulic motor with constant q_{M_t} (V_{M_t}) and with variable $q_{M_{gv}}$ ($V_{M_{gv}}$) capacity per one motor shaft revolution. The models present dependence of the torque M_{Mm} of mechanical losses in the assembly on the torque M_M loading the shaft and on the shaft speed n_M [changing in the ($0 \leq \overline{M}_M < \overline{M}_{Mmax}$, $0 \leq \overline{\omega}_M < \overline{\omega}_{Mmax}$) motor (and the hydrostatic transmission system) operating range] and also on the working fluid viscosity v changing in the $v_{min} \leq v \leq v_{max}$ range. Torque M_M , shaft speed n_M and working fluid viscosity v are independent of the motor and of the losses in it. The models present also the dependence of torque M_{Mm} on the capacity $q_{M_{gv}}$ per one shaft revolution (coefficient

$b_M = q_{M_{gv}}/q_{M_t}$ of the capacity per one shaft revolution) in a variable capacity motor. In the models, the change of $q_{M_{gv}}$ (b_M) is assumed in the $0 \leq q_{M_{gv}} \leq q_{M_t}$ ($0 \leq b_M \leq 1$) range, although during the motor operation b_{Mmin} is of the order of $0.2 \div 0.3$.

2. Mathematical models of the torque M_{Mm} of mechanical losses are based on the defined coefficients k_i of energy losses, relating the torque of mechanical losses to the reference values:
 - theoretical torque M_{M_t} of the motor with theoretical (constant) capacity q_{M_t} per one shaft revolution determined at the system nominal pressure p_n ,
 - theoretical rotational speed n_{M_t} of the motor with theoretical (constant) capacity q_{M_t} per one shaft revolution resulting from the pump theoretical capacity Q_{Pr} .
3. Mathematical models of the torque M_{Mm} of mechanical losses in the „shaft – working chambers” assembly should correspond with models of volumetric losses in the motor working chambers and with models of pressure losses in the motor channels.

BIBLIOGRAPHY

1. Paszota Z.: *Graphical presentation of the power of energy losses and power developed in the elements of hydrostatic drive and control system. Part I – Rotational hydraulic motor speed series throttling control systems*. Chapter in the monograph: „Research, design, production and operation of hydraulic systems” (in Polish), Adam Klich, Edward Palczak and Andrzej Meder editors. „Cylinder” Library. Komag Mining Mechanisation Centre, Gliwice 2008
2. Paszota Z.: *Graphical presentation of the power of energy losses and power developed in the elements of hydrostatic drive and control system. Part II – Rotational hydraulic motor speed parallel throttling control and volumetric control systems*. Chapter in the monograph: „Research, design, production and operation of hydraulic systems” (in Polish), Adam Klich, Edward Palczak and Andrzej Meder editors. „Cylinder” Library. Komag Mining Mechanisation Centre, Gliwice 2008
3. Paszota Z.: *Direction of increase of power stream in the hydrostatic drive and control system. Graphical presentation of the power of energy losses and power developed in the elements of hydrostatic drive and control system. Part I – Rotational hydraulic motor speed series throttling control systems*. (in Polish), Napędy i sterowanie, scientific monthly, No 10 (114), October 2008
4. Paszota Z.: *Direction of increase of power stream in the hydrostatic drive and control system. Graphical presentation of the power of energy losses and power developed in the elements of hydrostatic drive and control system. Part II – Rotational hydraulic motor speed parallel throttling control and volumetric control systems*. (in Polish), Napędy i sterowanie, scientific monthly, No 11 (115), November 2008
5. Paszota Z.: *Graphical presentation of the power of energy losses and power developed in the elements of hydrostatic drive and control system. Part I – Rotational hydraulic motor speed series throttling control systems*. Polish Maritime Research 03/2008
6. Paszota Z.: *Graphical presentation of the power of energy losses and power developed in the elements of hydrostatic drive and control system. Part II – Rotational hydraulic motor speed parallel throttling control and volumetric control systems*. Polish Maritime Research 04/2008
7. Paszota Z.: *The operating field of a hydrostatic drive system*. Chapter in the monograph: „Research, design, production and operation of hydraulic systems” (in Polish), Adam Klich, Antoni Kozieł and Edward Palczak editors. „Cylinder” Library. Komag Mining Mechanisation Centre, Gliwice 2009

8. Paszota Z.: *Parameters of the energy efficiency investigations of pumps and hydraulic motors. The operating field of a hydrostatic drive system.* (in Polish), *Napędy i sterowanie*, scientific monthly, No 11 (127), November 2009
9. Paszota Z.: *The operating field of a hydrostatic drive system parameters of the energy efficiency investigations of pumps and hydraulic motors.* *Polish Maritime Research* 04 / 2009
10. Paszota Z.: *Energy losses in the hydraulic rotational motor – definitions and relations for evaluation of the efficiency of motor and hydrostatic drive.* *Polish Maritime Research* 02/2010.

CONTACT WITH THE AUTHOR

Prof. Zygmunt Paszota
Faculty of Ocean Engineering
and Ship Technology
Gdansk University of Technology
Narutowicza 11/12
80-233 Gdansk, POLAND
e-mail: zpaszota@pg.gda.pl