

Shock safety modelling of indirect contact with low-voltage electric devices

WŁODZIMIERZ KORNILUK, DARIUSZ SAJEWICZ

*Białystok University of Technology
Wiejska 45D, 15-351 Białystok, Poland
e-mail: korniluk@pb.edu.pl, darsaj@op.pl*

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Abstract: The article presents a shock safety model of an indirect contact with a low-voltage electric device. This model was used for computations and analyses concerning the following: the probabilities of appearance of the particular shock protection unreliability states, electric shock states (ventricular fibrillation), contributions of the unreliability of different shock protection elements to the probability of occurrence of these states, as well as the risk of electric shock (and the shock safety), and contributions of the intensity of occurrence of damages to different shock protection elements to this risk. An example of a possibility to reduce the risk of an electric shock through changing the intensity of occurrence of damages to the selected protection elements was provided.

Key words: safety management process, expert system, Bayesian network, total probability, protection reliability states, appearance of touch and electric shock states, risk analysis and assessment

1. Introduction

In the process of shock safety management, the following tasks are performed, among others [1-3]: investigating electric shock incidents, analysing and assessing shock risks, as well as determining criteria of dimensioning shock protection means. The created expert system, supporting performance of these tasks [4], should have a knowledge base equipped with an appropriate shock safety model. Considering the characteristics of these tasks, a method of modelling the shock protection reliability and shock safety of low-voltage devices [5] was developed.

The suggested shock safety modelling method [5] consists in mapping – with the use of a Bayesian network – the total probability of appearance of different combinations of the considered damages and a lack of damages of the particular elements of shock protection means. The next stage comprises a computer identification of various touch scenarios (touch voltage appearing in the considered areas of contacting parts of electric devices). The probabilities of

appearance of touch effects on the basis of the touch voltage values and its duration as well as other pre-set circumstances and factors affecting the shock occurrence for the identified touch scenarios are subsequently determined. Such a method of modelling shock safety makes it possible to determine the probabilities and intensity of appearance of unreliability and shock states.

The article describes an example of applying the developed method to modelling shock safety in the case of an indirect contact with low-voltage electric devices.

The article includes the results of computations and analyses concerning:

- the probabilities of occurrence of different states of protection unreliability and of electric shock (ventricular fibrillation) as well as the contributions of the unreliability of different shock protection elements to the probability of occurrence of these states;
- the risk of an electric shock (and shock safety) as well as the contributions of the intensity of damages to the particular protection elements to this risk;
- the possibilities of reducing the risk of an electric shock.

2. Example of safety model

The developed shock safety model concerns shock protection against an indirect contact [6, 7] (auto power-off) for one of the devices installed in the wiring system of a single-family house connected to a single-phase TN-C-S system (Fig. 1).

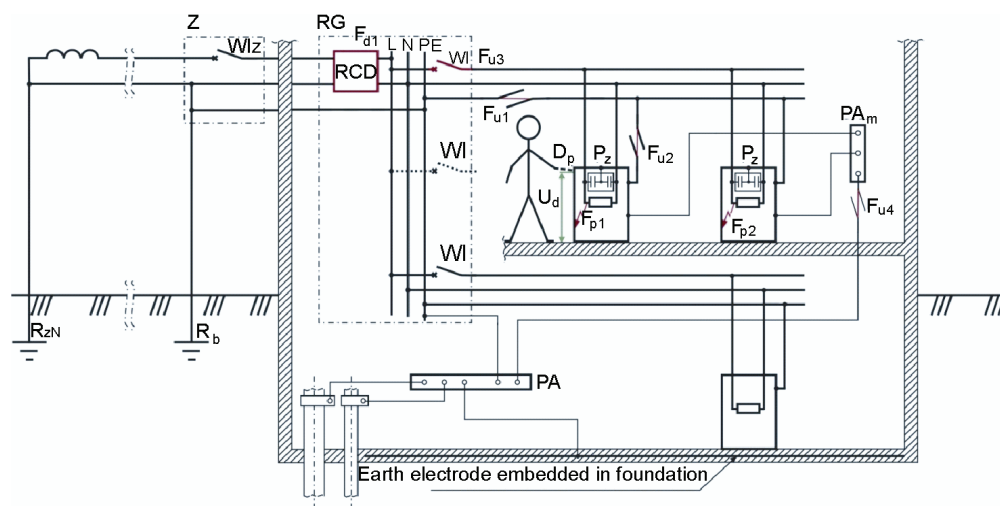


Fig. 1. Diagram of wiring system of single-family house connected to TN-C-S system. Symbols: Z – outdoor connector, PA – Main Equipotential Bonding, PA_m – Local Equipotential Bonding, RG – main switchgear, R_{zN} – earthing of system neutral point, R_b – earthing of PEN wire, W_{iz} , W_I – circuit breakers, RCD – high-sensitivity residual-current device, P_z – interference eliminator, F_{pi} , F_{ui} and F_{d1} – faults accounted for in reliability model of shock protection against indirect contact with one of devices

- The occurrence of the following types of protection was included in the model:
- basic protection: damage (a short circuit) to the basic insulation of the F_{p1} and F_{p2} devices;
 - fault protection: an (F_{u1}) discontinuity of a PE protective conductor, an (F_{u2}) discontinuity of a PE protective conductor, a state of (F_{u3}) fault condition of a protective device, and an (F_{u4}) discontinuity of the P_w protective bonding;
 - additional protection: a state of (F_{d1}) fault condition of the high-sensitivity residual-current device.

The limited number of damages to shock protection elements, analysed in the developed shock safety model, results from the necessity to simplify the model in order to illustrate the idea of the developed method well and to ensure clear demonstration of the obtained computation results.

Figure 2 shows a Bayesian network illustrating a shock safety model for an electric device in the case of a D_p indirect contact.

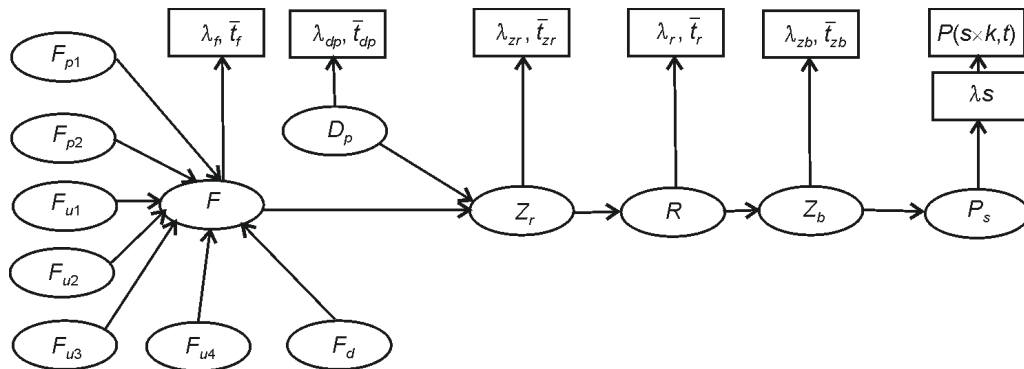


Fig. 2. Structure of Bayesian network illustrating shock safety model for indirect contact with one of devices installed in wiring system of single-family house (Fig.1). Symbols are explained in the text

The CPT of the F conditional node (Fig. 1) includes the values of probabilities representing 128 combinations of unreliability states for shock protection elements in an indirect contact.

The following reliability states were identified in the developed shock safety model: 128 – states of a lack of touch danger (a lack of damage or contact), 127 states of touch danger (a damage and contact occurred), 104 states (scenarios) of touch (8 states as a result of fault protection damage and 96 states resulting from basic protection damage), out of which 11 appeared in states of a lack of safety (protection) unreliability, and 93 in states of safety (protection) unreliability.

Eight scenarios of touch, which occur in the case of damage to fault protection elements (PE protective conductor and P_w protective bonding breaks) were considered; f_{u1} and f_{u4} occur as a result of using P_z interference eliminators in devices (Fig. 3). Electric network precipitators in electric devices are required in order to conform to the requirements of electromagnetic compatibility standards [8] concerning susceptibility and interference emissions. The structure of an asymmetric interference filter is shown in Figure 3a: condensers of the same

Table 1. List of values of reliability parameters of shock protection elements, adopted for computations before indirect contact with electric device (Fig. 1)

Type of damage to shock protection element	Parameter	Parameter values
(f_{u1}) discontinuity of PE protective conductor	$\lambda_{f_{u1}} [1/a]$	10^{-1} , 10^{-2} , or $5 \cdot 10^{-2}$
	$T_{ku1} [a]$	1, 2, or 5
(f_{p1}) damage (short circuit) to basic protection in device	$\lambda_{f_{p1}} [1/a]$	10^{-1} , 10^{-2} , or $5 \cdot 10^{-2}$
	$t_{wy1} [a]$	at auto power-off $1.27 \cdot 10^{-8}$
	$T_{kp1} [a]$	1, 2, or 5
(f_{p2}) damage (short circuit) to basic protection in device	$\lambda_{f_{p2}} [1/a]$	10^{-1} , 10^{-2} , or $5 \cdot 10^{-2}$
	$t_{wy2} [a]$	at auto power-off $1.27 \cdot 10^{-8}$
	$T_{kp2} [a]$	1, 2, or 5
(f_{u2}) discontinuity of PE protective conductor	$\lambda_{f_{u2}} [1/a]$	10^{-1} , 10^{-2} , or $5 \cdot 10^{-2}$
	$T_{ku2} [a]$	1, 2, or 5
(f_{u3}) state of fault condition of protective device	$\lambda_{f_{u3}} [1/a]$	$7.95 \cdot 10^{-2}$
	$T_{ku3} [a]$	1, 2, or 5
(f_{d1}) state of fault condition of high-sensitivity residual-current device	$\lambda_{f_{d1}} [1/a]$	$7 \cdot 10^{-3}$
	$T_{kd1} [a]$	1/12
$(f_{u4}) P_w$ protective bonding discontinuity	$\lambda_{f_{u4}} [1/a]$	10^{-1} , 10^{-2} , or $5 \cdot 10^{-2}$
	$T_{ku4} [a]$	1, 2, or 5

Table 2. List of touch voltage values and touch duration times, adopted for computations, and calculated conditional probabilities of occurrence of result in the form of ventricular fibrillation

No.	Protection damage	$U_d [V]$	$t_r [s]$	$P(s/F_{p1}, \dots, F_{d1})$	Number of scenarios
1	f_{p1} or f_{p2} basic protection	40	0.4	$1.22 \cdot 10^{-15}$	37
		50	5	$9.26 \cdot 10^{-7}$	8
2	f_{p1} or f_{p2} basic protection f_{u4} fault protection	80	0.4	$3.24 \cdot 10^{-10}$	14
			5	$2.64 \cdot 10^{-4}$	9
3	f_{u1} and f_{u4} fault protection	16	10	$2.48 \cdot 10^{-14}$	8
4	f_{p1} or f_{p2} basic protection $f_{u1} \vee f_{u2}$ and f_{u4} fault protection f_{d1} additional protection	230	10	0.59	28

The adopted touch voltage values ranged from several volts (when only the basic protection was damaged) to 230 V (damaged basic protection, and broken PE and P_w). The adopted

touch duration times resulted from the allowed operating times for particular protection means [12] or, in the cases when the power is not switched off quickly, the time of 10 s was adopted. The results of calculating $P(s/F_{p1}, \dots, F_{d1})$ conditional probabilities of occurrence of a result in the form of ventricular fibrillation in the particular shock scenarios for the adopted U_d touch voltage values and the t_r touch duration times are listed in Table 2.

The selected results pertaining to the probabilities and intensity of occurrence of unreliability states of protection elements at an indirect contact as well as the reliability states of shock protection at indirect contacts with electric devices (Fig. 1) are listed in Tables 3 and 4. The results indicate that the probability of occurrence of the touch state decreases with the increase of the ensured reliability of protection elements (through reducing λ_r and/or T_k).

Table 3. Probability of occurrence of shock protection unreliability states at indirect contact with electric devices (Fig. 1)

$\lambda_{fx}[1/a]$	$T_k[a]$	$P(f)$	$P(z_r)$	$P(r)$	$P(\bar{z}_b)$	$P(z_b)$
0.1	5	0.606	0.545	$6 \cdot 10^{-2}$	$3.8 \cdot 10^{-2}$	$2.2 \cdot 10^{-2}$
	2	0.312	0.281	$9.8 \cdot 10^{-3}$	$7.8 \cdot 10^{-3}$	$2 \cdot 10^{-3}$
	1	0.172	0.154	$2.4 \cdot 10^{-3}$	$2.1 \cdot 10^{-3}$	$3 \cdot 10^{-4}$
0.05	5	0.430	0.387	$1.5 \cdot 10^{-2}$	$1.1 \cdot 10^{-2}$	$4 \cdot 10^{-3}$
	2	0.203	0.183	$2.4 \cdot 10^{-3}$	$2.1 \cdot 10^{-3}$	$3 \cdot 10^{-4}$
	1	0.108	0.097	$5.8 \cdot 10^{-4}$	$5.4 \cdot 10^{-4}$	$4 \cdot 10^{-5}$
0.01	5	0.234	0.211	$5.8 \cdot 10^{-4}$	$5.4 \cdot 10^{-4}$	$4 \cdot 10^{-5}$
	2	0.103	0.092	$9.18 \cdot 10^{-5}$	$8.88 \cdot 10^{-5}$	$3 \cdot 10^{-6}$
	1	0.053	0.048	$2.27 \cdot 10^{-5}$	$2.235 \cdot 10^{-5}$	$3.5 \cdot 10^{-7}$

Determined for: $\lambda_{fx} = \lambda_{fp1} = \lambda_{fp2} = \lambda_{fu1} = \lambda_{fu2} = \lambda_{fu4}$,
 $\lambda_{fu3} = 0.0795$ 1/a and $\lambda_{fd1} = 0.007$ 1/a

Table 4. Results of calculating intensity of occurrence of protection elements unreliability states at indirect contact with electric devices and shock protection reliability states (Fig. 1)

$\lambda_{fx}[1/a]$	$T_k[a]$	$\lambda_x[1/a]$	$\lambda_{z_r}[1/a]$	$\lambda_r[1/a]$	$\lambda_{z_b}[1/a]$	$\lambda_{z_b}[1/a]$
0.1	5	0.587	0.528	0.245	0.128	0.117
	2			0.206	0.167	0.039
	1			0.190	0.164	0.026
0.05	5	0.337	0.304	0.105	0.074	0.031
	2			0.095	0.082	0.013
	1			0.092	0.085	0.007
0.01	5	0.136	0.123	0.018	0.0171	$9 \cdot 10^{-4}$
	2			0.018	0.0176	$4 \cdot 10^{-4}$
	1			0.018	0.0178	$2 \cdot 10^{-4}$

Determined for: $\lambda_{fx} = \lambda_{fp1} = \lambda_{fp2} = \lambda_{fu1} = \lambda_{fu2} = \lambda_{fu4}$,
 $\lambda_{fu3} = 0.0795$ 1/a and $\lambda_{fd1} = 0.007$ 1/a

The total probability of 104 touch scenarios amounts to $P(r) = 5.8 \cdot 10^{-4}$ (calculated for the case where $\lambda_{fx} = 0.01$ 1/a, $\lambda_{fu3} = 0.0795$ 1/a, $\lambda_{fd1} = 0.007$ 1/a, and $T_k = 5a$). Out of these touch scenarios, the following have the highest probability of occurrence:

– the first scenario

$$P(r_1) = P(\bar{f}_{p1wyt}) \cdot P(\bar{f}_{p2wyt}) \cdot P(f_{u1}) \cdot P(\bar{f}_{u2}) \cdot P(\bar{f}_{u3}) \cdot P(f_{u4}) \cdot P(\bar{f}_{d1}) = 4.35 \cdot 10^{-4},$$

$$P(r_1) / P(r) \cdot 100\% = 75\%,$$

– the second scenario

$$P(r_2) = P(f_{p1}) \cdot P(\bar{f}_{p2wyt}) \cdot P(\bar{f}_{u1}) \cdot P(\bar{f}_{u2}) \cdot P(\bar{f}_{u3}) \cdot P(f_{u4}) \cdot P(\bar{f}_{d1}) = 1.07 \cdot 10^{-5},$$

$$P(r_2) / P(r) \cdot 100\% = 1.86\%,$$

– the third scenario

$$P(r_3) = P(\bar{f}_{p1wyt}) \cdot P(f_{p2}) \cdot P(\bar{f}_{u1}) \cdot P(f_{u2}) \cdot P(\bar{f}_{u3}) \cdot P(f_{u4}) \cdot P(\bar{f}_{d1}) = 1.07 \cdot 10^{-5},$$

$$P(r_3) / P(r) \cdot 100\% = 1.86\%.$$

The total intensity of the 104 touch scenarios equals $\lambda_r = 1.86 \cdot 10^{-2}$ 1/a (calculated for the case where $\lambda_{fx} = 0.01$ 1/a, $\lambda_{fu3} = 0.0795$ 1/a, $\lambda_{fd1} = 0.007$ 1/a, and $T_k = 5a$). Out of these touch scenarios, the following are characterised by the greatest intensity of occurrence:

– the first scenario

$$\lambda_{r1} = P(f_{p1wyt}) \cdot P(\bar{f}_{p2wyt}) \cdot P(\bar{f}_{u1}) \cdot P(\bar{f}_{u2}) \cdot P(\bar{f}_{u3wyt}) \cdot P(\bar{f}_{u4}) \cdot P(\bar{f}_{d1}) = 8.35 \cdot 10^{-3} \text{ 1/a},$$

$$\lambda_{r1} / \lambda_r \cdot 100\% = 44.9\%,$$

– the second scenario

$$\lambda_{r2} = P(\bar{f}_{p1wyt}) \cdot P(\bar{f}_{p2wyt}) \cdot P(\bar{f}_{u1}) \cdot P(f_{u2}) \cdot P(\bar{f}_{u3}) \cdot P(f_{u4}) \cdot P(f_{d1}) = 3.56 \cdot 10^{-4} \text{ 1/a},$$

$$\lambda_{r2} / \lambda_r \cdot 100\% = 1.91\%,$$

– the third scenario

$$\lambda_{r3} = P(f_{p1wyt}) \cdot P(\bar{f}_{p2wyt}) \cdot P(\bar{f}_{u1}) \cdot P(\bar{f}_{u2}) \cdot P(\bar{f}_{u3wyt}) \cdot P(f_{u4}) \cdot P(\bar{f}_{d1}) = 2.10 \cdot 10^{-4} \text{ 1/a},$$

$$\lambda_{r3} / \lambda_r \cdot 100\% = 1.13\%.$$

The relative contributions of (f_{p1}, f_{p2}) unreliability of the particular basic, $(f_{u1}, f_{u2}, f_{u3}, f_{u4})$ fault, and (f_{d1}) additional protection elements to the $P(r)$ probability as well as the relative contributions of the damage intensity of these elements to the λ_r intensity of touch states at an indirect contact with electric devices (Fig. 1) are shown in Figure 4.

Relative contributions of unreliability of the particular basic, fault, and additional protection elements to the $P(r)$ probability of occurrence of touch can be successfully applied to determine the most probable touch scenario occurring in the event of an electrical accident.

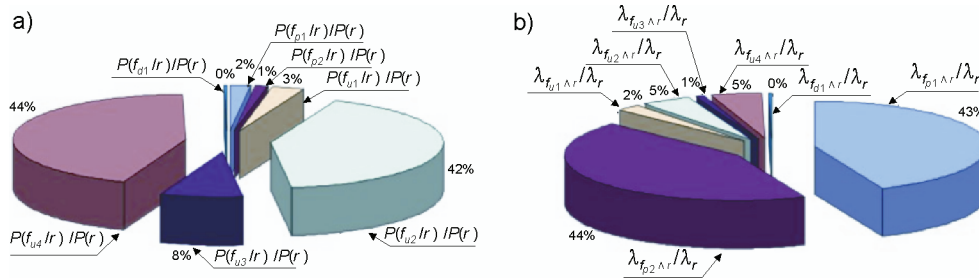


Fig. 4. Relative contributions of (a) unreliability of particular elements of basic (f_{p1}, f_{p2}), fault ($f_{u1}, f_{u2}, f_{u3}, f_{u4}$) and additional (f_{id1}) protection to $P(r)$ probability of occurrence of touch states and (b) intensity of damage to protection elements to λ_r intensity of occurrence of touch states at indirect contacts with electric devices. Calculations were performed for $\lambda_{fx} = 0.01$ 1/a, $\lambda_{fu3} = 0.0795$ 1/a, $\lambda_{fid1} = 0.007$ 1/a, intensities and $T_k = 5a$ inspection time. Symbols for damages and states of fault condition as in Figure 1

The relative distribution of contributions of unreliability of the particular protection elements to the probability of occurrence of touch (Fig. 4a) during an indirect contact with a device indicates that in 89% of touch scenarios, fault condition of the fault protection elements ($f_{u1} \vee f_{u2} \vee f_{u4}$) takes place. On the other hand, the relative distribution of contributions of the intensity of damages to the protection to the intensity of touch states occurrence (Fig. 4b) indicates that 87% of touch incidents are caused by the state of fault condition of the basic protection ($f_{u1} \vee f_{u2}$).

The selected results concerning the probabilities of occurrence of an electric shock with a result in the form of ventricular fibrillation with a reliable $P(s \wedge \bar{z}_b)$ and unreliable protection $P(s \wedge z_b)$ as well as the total $P(s)$ at indirect contacts with electric devices (Fig. 1) are given in Table 5.

Table 5. Probability of occurrence of electric shock with a result in the form of ventricular fibrillation with reliable $P(s \wedge \bar{z}_b)$ and unreliable protection $P(s \wedge z_b)$ as well as the total $P(s)$ at indirect contacts with electric devices (Fig. 1)

$\lambda_{fx}[1/a]$	$T_k[a]$	$P(s \wedge \bar{z}_b)$	$P(s \wedge z_b)$	$P(s)$
0.1	5	$9.34 \cdot 10^{-16}$	$1.33 \cdot 10^{-2}$	$1.33 \cdot 10^{-2}$
	2	$1.93 \cdot 10^{-16}$	$1.23 \cdot 10^{-3}$	$1.23 \cdot 10^{-3}$
	1	$5.21 \cdot 10^{-17}$	$1.75 \cdot 10^{-4}$	$1.75 \cdot 10^{-4}$
0.05	5	$2.89 \cdot 10^{-16}$	$2.26 \cdot 10^{-3}$	$2.26 \cdot 10^{-3}$
	2	$5.21 \cdot 10^{-17}$	$1.75 \cdot 10^{-4}$	$1.75 \cdot 10^{-4}$
	1	$1.35 \cdot 10^{-17}$	$2.34 \cdot 10^{-5}$	$2.34 \cdot 10^{-5}$
0.01	5	$1.35 \cdot 10^{-17}$	$2.34 \cdot 10^{-5}$	$2.34 \cdot 10^{-5}$
	2	$2.20 \cdot 10^{-18}$	$1.56 \cdot 10^{-6}$	$1.56 \cdot 10^{-6}$
	1	$5.55 \cdot 10^{-19}$	$1.98 \cdot 10^{-7}$	$1.98 \cdot 10^{-7}$

Determined for: $\lambda_{fx} = \lambda_{fp1} = \lambda_{fp2} = \lambda_{fu1} = \lambda_{fu2} = \lambda_{fu4}$, $\lambda_{fu3} = 0.0795$ 1/a and $\lambda_{fid1} = 0.007$ 1/a

Table 6. λ_s intensity of occurrence of electric shock with a result in the form of ventricular fibrillation (divided into states with a reliable $\lambda_{s \wedge \bar{z}_b}$ and unreliable $\lambda_{s \wedge z_b}$ protection) and $P(s \times k = 0, t = 1a)$ probabilities of non-occurrence of electric shock within one year at indirect contact with electric devices (Fig. 1)

$\lambda_{f\bar{a}} [1/a]$	$T_k [a]$	$\lambda_{s \wedge \bar{z}_b}$	$\lambda_{s \wedge z_b}$	λ_s	$P(s \times k = 0, t = 1a)$
0.1	5	$1.82 \cdot 10^{-17}$	$6.86 \cdot 10^{-5}$	$6.86 \cdot 10^{-5}$	0.999931
	2	$2.37 \cdot 10^{-18}$	$1.97 \cdot 10^{-6}$	$1.97 \cdot 10^{-6}$	0.999998
	1	$3.83 \cdot 10^{-19}$	$9.04 \cdot 10^{-8}$	$9.04 \cdot 10^{-8}$	~1
0.05	5	$1.78 \cdot 10^{-18}$	$2.17 \cdot 10^{-6}$	$2.17 \cdot 10^{-6}$	0.999998
	2	$1.79 \cdot 10^{-19}$	$4.21 \cdot 10^{-8}$	$4.21 \cdot 10^{-8}$	~1
	1	$2.64 \cdot 10^{-20}$	$1.66 \cdot 10^{-9}$	$1.66 \cdot 10^{-9}$	~1
0.01	5	$4.15 \cdot 10^{-21}$	$2.59 \cdot 10^{-10}$	$2.59 \cdot 10^{-10}$	~1
	2	$3.34 \cdot 10^{-22}$	$3.49 \cdot 10^{-12}$	$3.49 \cdot 10^{-12}$	~1
	1	$4.57 \cdot 10^{-23}$	$1.21 \cdot 10^{-13}$	$1.21 \cdot 10^{-13}$	~1

Determined for: $\lambda_{fx} = \lambda_{fp1} = \lambda_{fp2} = \lambda_{fu1} = \lambda_{fu2} = \lambda_{fu4}, \lambda_{fu3} = 0.0795 \text{ 1/a}$ and $\lambda_{fd1} = 0.007 \text{ 1/a}$

The selected results concerning the λ_s intensity of occurrence of an electric shock with a result in the form of ventricular fibrillation (divided into states with a reliable $\lambda_{s \wedge \bar{z}_b}$ and unreliable $\lambda_{s \wedge z_b}$ protection) as well as the $P(s \times k = 0, t = 1a)$ probabilities of non-occurrence of an electric shock within one year at an indirect contact with electric devices (Fig. 1) are presented in Table 6. It needs to be emphasised that $\lambda_{s \wedge z_b} \gg \lambda_{s \wedge \bar{z}_b}$ in all the cases, thus the intensity of occurrence of an electric shock with a result in the form of ventricular fibrillation λ_s is determined by the unreliability of the shock protection elements [5].

The relative contributions of unreliability of the particular basic (f_{p1}, f_{p2}), fault ($f_{u1}, f_{u2}, f_{u3}, f_{u4}$), and additional (f_{d1}) protection elements to the $P(s)$ probability as well as the relative contributions of the damage intensity of these elements to the λ_s intensities of occurrence of states of an electric shock at indirect contacts with electric devices (Fig. 3) are illustrated in Figure 5.

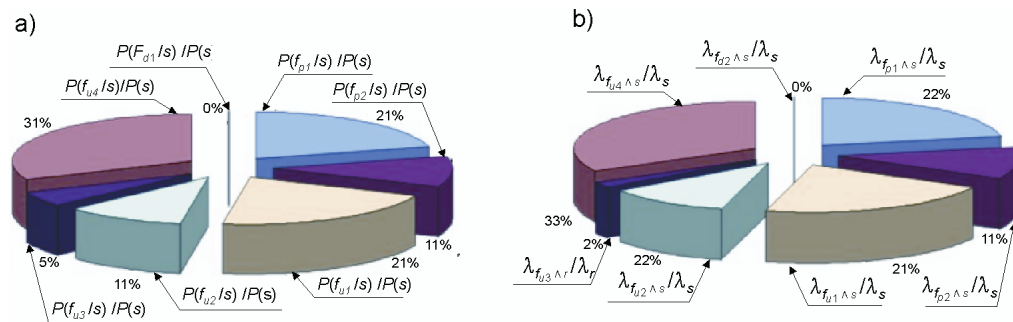


Fig. 5. Relative contributions of (a) unreliability of particular elements of basic (f_{p1}, f_{p2}), fault ($f_{u1}, f_{u2}, f_{u3}, f_{u4}$), and additional (f_{d1}) protection to $P(s)$ probability of occurrence of a state with ventricular fibrillation and (b) intensity of damage to these elements to λ_s intensity of occurrence of such states at indirect contacts with electric devices. Calculations were performed for $\lambda_{fx} = 0.01 \text{ 1/a}$, $\lambda_{fu3} = 0.0795 \text{ 1/a}$, $\lambda_{fd1} = 0.007 \text{ 1/a}$ intensities and $T_k = 5a$ inspection time. Symbols for damages and states of fault condition as in Figure 1.

Relative contributions of unreliability of the particular basic, fault, and additional protection elements to the $P(s)$ probability of occurrence of an electric shock (ventricular fibrillation) can be effectively used for determining the most probable shock scenario occurring during an electrical accident.

The relative distribution of contributions of unreliability of the particular protection elements of a device to the probability of occurrence of ventricular fibrillation (Fig. 5a) in the case of an indirect contact with this device indicates that in 32% of incidents of an electric shock, damage to the elements of basic protection ($f_{p1} \vee f_{p2}$), and in 63% of cases damage to fault protection ($f_{u1} \vee f_{u2} \vee f_{u4}$) elements is observed, whereas the relative distribution of contributions of the intensity of damages to the protection to the intensity of an electric shock occurrence (Fig. 5b) indicates that 33% of cases of an electric shock result from ($f_{p1} \vee f_{p2}$) damages to the basic protection, and 65% from ($f_{u1} \vee f_{u2} \vee f_{u4}$) fault condition of the fault protection.

The $P(s)$ probability of occurrence of the state of an electric shock with ventricular fibrillation (a), as well as (b) the λ_s intensity of occurrence of such states at contacts with electric devices (Fig. 1), determined for the $\lambda_{fx} = 0.01$ 1/a, $\lambda_{fu3} = 0.0795$ 1/a, $\lambda_{fu1} = 0.007$ 1/a intensities and the $T_k = 1, 2,$ and $5a$ inspection times, are listed respectively in Fig. 6.

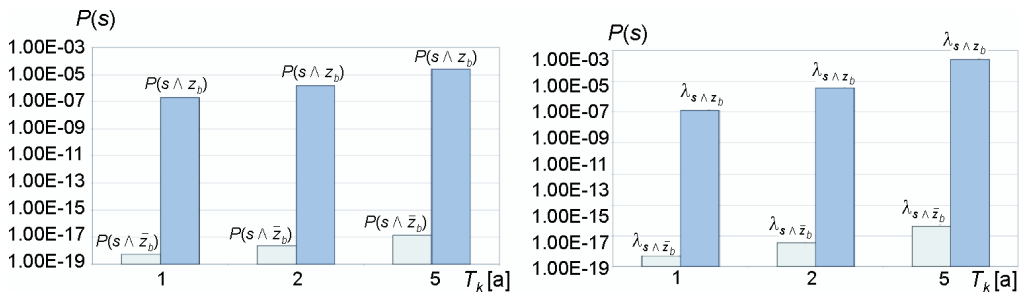


Fig. 6. $P(s)$ probability of occurrence of electric shock state with ventricular fibrillation (a) and λ_s intensity of occurrence of such states (b) at contacts with electric devices for different T_k inspection times. Calculations were carried out for $\lambda_{fx} = 0.01$ 1/a, $\lambda_{fu3} = 0.0795$ 1/a, $\lambda_{fu1} = 0.007$ 1/a intensities. Symbols for damages and states of fault condition as in Figure 1

Calculations of the intensity of occurrence of an electric shock with a result in the form of ventricular fibrillation were also performed for three other variants of solving the shock protection against an indirect contact in the system under concern (Fig. 1). In the 1st variant, a high-sensitivity residual-current device and an equipotential bonding were used; in the 2nd variant there is no high-sensitivity residual-current device ($P(f_{d1})=1$ and $P(\bar{f}_{d1})=0$); the 3rd variant does not have an equipotential bonding ($P(f_{u4})=1$ and $P(\bar{f}_{u4})=1$); in the 4th variant, here is no high-sensitivity residual-current device or equipotential bonding ($P(f_{d1})=1$, $P(\bar{f}_{d1})=0$ and $P(f_{u4})=1$, $P(\bar{f}_{u4})=1$). The calculation results are presented in Table 7.

Table 7. List of calculated intensities of occurrence of electric shock with a result in the form of ventricular fibrillation λ_s (divided into states with a reliable $\lambda_{s \wedge \bar{z}_b}$ and unreliable $\lambda_{s \wedge z_b}$ protection) at indirect contact with electric devices (Fig. 1) for four variants of solving the shock protection

Variant of protection solution	Intensity of occurrence of state	For $\lambda_{fx} = 0.01$ 1/a	For $\lambda_{fx} = 0.05$ 1/a	For $\lambda_{fx} = 0.1$ 1/a
1st variant of protection solution with RCD and P_W	λ_s [1/a] shock	$2.59 \cdot 10^{-10}$	$2.17 \cdot 10^{-6}$	$6.86 \cdot 10^{-5}$
	$\lambda_{s \wedge \bar{z}_b}$ [1/a] shock with reliable protection	$4.15 \cdot 10^{-21}$	$1.18 \cdot 10^{-18}$	$1.82 \cdot 10^{-17}$
	$\lambda_{s \wedge z_b}$ [1/a] shock with unreliable protection	$2.59 \cdot 10^{-10}$	$2.17 \cdot 10^{-6}$	$6.86 \cdot 10^{-5}$
2nd variant of protection solution with P_W and without RCD	λ_s [1/a] shock	$2.88 \cdot 10^{-10}$	$2.16 \cdot 10^{-6}$	$6.84 \cdot 10^{-5}$
	$\lambda_{s \wedge \bar{z}_b}$ [1/a] shock with reliable protection	$4.16 \cdot 10^{-21}$	$1.77 \cdot 10^{-18}$	$1.77 \cdot 10^{-17}$
	$\lambda_{s \wedge z_b}$ [1/a] shock with unreliable protection	$2.88 \cdot 10^{-10}$	$2.16 \cdot 10^{-6}$	$6.84 \cdot 10^{-5}$
3rd variant of protection solution protection with RCD and without P_W	λ_s [1/a] shock	$2.91 \cdot 10^{-7}$	$1.161 \cdot 10^{-4}$	$1.128 \cdot 10^{-3}$
	$\lambda_{s \wedge \bar{z}_b}$ [1/a] shock with reliable protection	$3.59 \cdot 10^{-18}$	$1.74 \cdot 10^{-18}$	$2.49 \cdot 10^{-16}$
	$\lambda_{s \wedge z_b}$ [1/a] shock with unreliable protection	$2.91 \cdot 10^{-7}$	$1.161 \cdot 10^{-4}$	$1.128 \cdot 10^{-3}$
4th variant of protection solution protection without RCD or P_W	λ_s [1/a] shock	$3 \cdot 10^{-7}$	$1.165 \cdot 10^{-4}$	$1.125 \cdot 10^{-3}$
	$\lambda_{s \wedge \bar{z}_b}$ [1/a] shock with reliable protection	$3.62 \cdot 10^{-18}$	$7.47 \cdot 10^{-17}$	$2.41 \cdot 10^{-16}$
	$\lambda_{s \wedge z_b}$ [1/a] shock with unreliable protection	$3 \cdot 10^{-7}$	$1.165 \cdot 10^{-4}$	$1.125 \cdot 10^{-3}$

Determined for: $\lambda_{fx} = 0.01$ 1/a or $\lambda_{fx} = 0.05$ 1/a or $\lambda_{fx} = 0.1$ 1/a, $\lambda_{fz3} = 0.0795$ 1/a, $\lambda_{fid1} = 0.007$ 1/a and $T_k = 5a$

Shock protection is 'efficient' if the residual risk of an electric shock, represented by λ_s , is smaller than the tolerated $\lambda_s \leq \lambda_{s dop} = 10^{-6}$ 1/a. Such an approach is applied to criticality analysis [13, 14] in order to differentiate between allowed and unallowable risks. The condition of $\lambda_s \leq \lambda_{s dop} = 10^{-6}$ 1/a for $\lambda_{fx} = 0.05$ 1/a is not met by the 3rd variant of a protection solution with an RCD and without a P_W or the 4th variant of a protection solution without an RCD or a P_W . The possibilities of reducing the risk of an electric shock for these variants of protection are listed in Table 8.

Reducing the risk of an electric shock at contacts with electric devices in the considered case is possible for the 3rd and 4th variants of the protection (Tab. 8) through improving the basic and fault protection reliability.

Table 8. Possibilities of reducing risk of an electric shock for two variants of shock protection

Variant of protection solution	Intensity of occurrence of state	Residual risk			
		Without reduction	After reduction		
			Reduction through improving basic protection reliability from $\lambda_{fp1} = \lambda_{fp2} = 0.05$ 1/a to $\lambda_{fp1} = \lambda_{fp2} = 0.01$ 1/a	Reduction through improving fault protection reliability from $\lambda_{fu1} = \lambda_{fu2} = 0.05$ 1/a to $\lambda_{fu1} = \lambda_{fu2} = 0.01$ 1/a	Reduction through improving basic and fault protection reliability from $\lambda_{fp1} = \lambda_{fp2} = \lambda_{fu1}$ $\lambda_{fu2} = 0.05$ 1/a to $\lambda_{fp1} = \lambda_{fp2} = \lambda_{fu1}$ $\lambda_{fu2} = 0.01$ 1/a
3rd variant of protection solution with RCD and without PW	λ_s [1/a] shock	$1.161 \cdot 10^{-4}$	$5.77 \cdot 10^{-6}$	$6.15 \cdot 10^{-6}$	$3.05 \cdot 10^{-7}$
4th variant of protection solution without RCD or PW	λ_s [1/a] shock	$1.165 \cdot 10^{-4}$	$5.82 \cdot 10^{-6}$	$6.28 \cdot 10^{-6}$	$3.14 \cdot 10^{-7}$

Determined for: $\lambda_{fx} = 0.05$ 1/a, $\lambda_{fu3} = 0.0795$ 1/a, $\lambda_{fu1} = 0.007$ 1/a and $T_k = 5a$

3. Conclusions

The method of modelling shock safety for low-voltage devices, based on using a Bayesian network, makes it possible to perform a comprehensive analysis and assessment of the risk of an electric shock, and also to investigate electric shock incidents and determine criteria of dimensioning shock protection means (including their reliability), which was confirmed by the calculations and analyses carried out with the use of the developed model of the protection reliability and shock safety for indirect contacts with electric devices installed in the wiring system of a single-family house.

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