

Application of the design of experiments in the epoxidation process of 1,5,9-cyclododecatriene

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An influence of the molar ratio of *cis,trans,trans*-1,5,9-cyclododecatriene to *tert*-butyl hydroperoxide, the concentration of the catalyst and the reaction time on the performance of the epoxidation process of *cis,trans,trans*-1,5,9-cyclododecatriene with *tert*-butyl hydroperoxide at the presence of molybdenum hexacarbonyl $\text{Mo}(\text{CO})_6$ was examined. Examinations were performed using statistical methods of the design of experiments. A mathematical model describing the influence of the parameters on conversion *cis,trans,trans*-1,5,9-cyclododecatriene was obtained. An analysis of the data and rests was performed and an optimal value of conversion of *cis,trans,trans*-1,5,9-cyclododecatriene was established.

Keywords: epoxidation, design of experiments, 1,5,9-cyclododecatriene, optimization.

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INTRODUCTION

The need for the knowledge, constant developing in scientific research and in industry but also the growing complexity of the examined objects needs a modern approach to the experimental studies. Because of this, there were worked out statistical methods of the design of experiments, which were based on the theory of probability and mathematical statistic, for example: fractional factorial designs, central composite designs, mixture designs, etc.¹⁻³. To the most important advantages of these designs can be recognized their efficiency; it means the possibility to examine a large number of variables at a small number of experiments as well as presenting the dependency between the input and output variables in the form of a mathematical function⁴.

In the literature there is not enough information about comparing the quality of different methods of the design of experiments in practice, which could bring more information about the usefulness of the theoretically weaker and better designs under real conditions. Thus, the aim of this work is to perform a comparison of two plans: orthogonal and rotatable in the epoxidation of *cis,trans,trans*-1,5,9-cyclododecatriene (CDT) using *tert*-butyl hydroperoxide (TBHP) over the molybdenum catalyst. As first, a rotatable design was realised for three input values: the molar ratio CDT/TBHP, the catalyst concentration and the reaction time.

MATERIALS AND METHODS

Chemicals

In the experiments there were used the 46% solution of TBHP in 1,2-dichloroethane (DCE), which was received in the extraction process of the 70% water solution of TBHP by DCE⁵, CDT of the concentration >98% from Sigma Aldrich, molybdenum hexacarbonyl, $\text{Mo}(\text{CO})_6$ of the concentration >95% from Merck, and DCE from POCH S.A., Poland.

Procedure

All the experiments were performed according to the same procedure. A precisely weighed amount of CDT and

the solution of TBHP in DCE was put into a three-necked flask of the capacity of 25 cm³, fitted with a thermometer, reflux and a mechanical stirrer. The flask was later immersed in an oil bath and the stirrer was started. When the temperature of the mixture reached 70°C, the molybdenum catalyst dissolved in DCE was added quickly. The whole amount of raw materials was constant in all experiments and equal 18 cm³. After finishing the reaction, the flask with the post-reaction mixture was cooled immediately to room temperature to stop the reaction. The content of the flask was weighed and chromatographic and iodometry analyses were performed in order to calculate the mass balance.

The experiments were performed according to the rotatable design^{1,6}. There were chosen three independent factors for the experiment: the molar ratio of CDT/TBHP (X_1), the concentration of $\text{Mo}(\text{CO})_6$ – catalyst (X_2), and the reaction time (X_3). The values of the factors in the normalized form (x_i) and the related to them values in a real form (X_i) are shown in Table 1. All the experiments were taken at the constant temperature of 70°C. 20 experiments altogether (8 in nucleus of the plan, 6 in star points and 6 in the centre of the plan) were performed for the three input values. The CDT ($K_{\text{CDT}} = \text{amount of reacted CDT} / \text{amount of introduced CDT} \times 100$) conversion was chosen as the answer function.

The design matrix of the experiments in the normalization form and the experimental results of the CDT conversion are shown in Table 2.

RESULTS AND DISCUSSION

Data analysis

First the experimental results were taken for a pre-analysis. The purpose of the pre-analysis was a proper identification of the structure and the quality of the received data.

The analysis of the basis statistics (Table 3) shows, that the smallest variability of the results has the subgroup, which contains 6 experiments (repetitions). The difference between the smallest and the largest value in the subgroup (range) is only 6.9%. The variance for the repetitions is 5.7

Table 1. The normalized and real values of the independent factors

Value of factor in normalized form x_i	Value of factor in real form X_i		
	X_1 [mol/mol]	X_2 [g/cm ³]	X_3 [min.]
-1	1	$5,280 \cdot 10^{-4}$	20
0	3	$2,904 \cdot 10^{-3}$	70
1	5	$5,280 \cdot 10^{-3}$	120

Table 2. The rotatable design experimental results

Number of exper.	x_1	x_2	x_3	K_{CDT} , %
1	-1	-1	-1	19,22
2	-1	-1	1	38,81
3	-1	1	-1	26,22
4	-1	1	1	45,97
5	1	-1	-1	9,94
6	1	-1	1	12,93
7	1	1	-1	9,71
8	1	1	1	23,22
9	-1,682	0	0	57,53
10	1,682	0	0	8,48
11	0	-1,682	0	8,39
12	0	1,682	0	25,84
13	0	0	-1,682	6,52
14	0	0	1,682	30,95
15(C)	0	0	0	21,99
16(C)	0	0	0	25,41
17(C)	0	0	0	26,16
18(C)	0	0	0	27,20
19(C)	0	0	0	28,89
20(C)	0	0	0	27,60

(C) – centre of plan, experiments 15 – 20

and is over 30 times less than the variance calculated for all the results. The average values in groups 14 and 20 of the experiments are similar, but in the group of 6 experiments (repetitions) some deviations to higher values are observed.

The correlation coefficients of the CDT conversion with independent variables were presented in Table 4. It follows from Table 4 that the molar ratio of the CDT/TBHP and conversion of CDT are highly negatively correlated (-0.74). Such good correlation partly results from the way of counting of the CDT conversion, where in the calculating formula the number of moles of CDT is inserted. The reaction time is also strongly connected with the CDT conversion (strong positive correlation). However, there is lack of significant correlation of the catalyst concentration with the conversion of CDT.

The analysis of variance^{7, 8}

In Table 5 parts of each input variable in the sum of squares (SS), were presented, it means their parts in the whole variability of the output values. Mean squares are distributed well among the variables. Pure error does not differ statistically from the error of fit, which means, that the regression equation containing all the variables from Table 5 will be statistically adequate. It is also seen that line effects have a significant influence on the K_{CDT} value, mainly the molar ratio (x_1) and the reaction time (x_3).

Table 3. Basic statistics calculated on the base of the results of the CDT conversion

	Average	Min.	Max.	Range	Variation	Dev.Std
K_{CDT} % (20 experiments)	24.0	6.5	57.5	51.0	172.6	13.1
K_{CDT} % (6 repetitions)	26.2	22.0	28.9	6.9	5.7	2.4
K_{CDT} % (14 experiments)	23.1	6.5	57.5	51.0	246.9	15.7

Table 4. The correlation coefficient (calculated from the real values)

	X_1	X_2	X_3
K_{CDT} %	-0,74	0,25	0,46

(bold coefficients are important with probability $\alpha=0.05$)

Mathematical model for the CDT conversion

Variables in Table 5, whose coefficients b_i are in bold were taken in the mathematical model describing an influence of the three input variables: the molar ratio of CDT/TBHP, the catalyst concentration and the reaction time on the CDT conversion. For the CDT conversion, the regression equation is in a square form:

$$Y_{K_{CDT}} = 26,18 - 11,49x_1 + 2,52x_1^2 + 3,92x_2 - 3,1x_2^2 + 7,1x_3 - 2,57x_3^2 - 2,85x_1x_3$$

The regression equation for the CDT conversion is adequate (Table 5) and has a high value of a coefficient of multiple correlation R^2 (>90%) for a confidence interval at the level of 95%.

Research of the model: rests^{8, 9}

The diagnostics of a built approximation function relies mainly on testing the rests. The rests contain this part of the variation of the CDT conversion, which a received function does not explain.

Testing of the rests was performed graphically. A test of normality of rest distributions and rest distributions according to a sequence of time, was performed. In order to do this a histogram of rest normalities (Figure 1) was made and the Shapiro-Wilk test of normality was performed. It turned out that the distribution of rests exhibits normal character. The determined minimum, maximum, range and the variation values for the rests were shown in Table 6.

In Figure 2 there was shown a range of rests according to a sequence of time, which means, in the order of performing the experiments. The largest deviation from the centre can be observed in experiments 5 and 10. Apart from the pointed exceptions, the rests in the other experi-

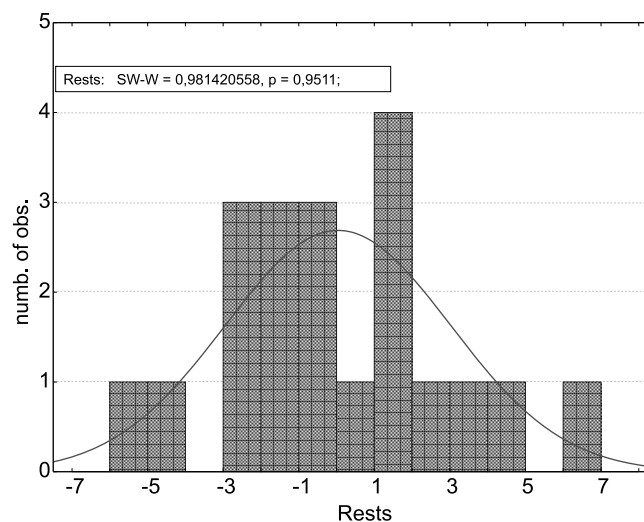
**Figure 1.** Range of normality of rests (in the box – results of Shapiro-Wilk test)

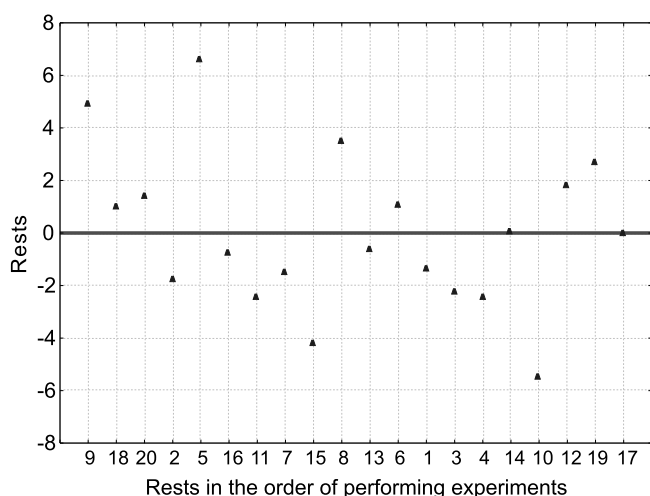
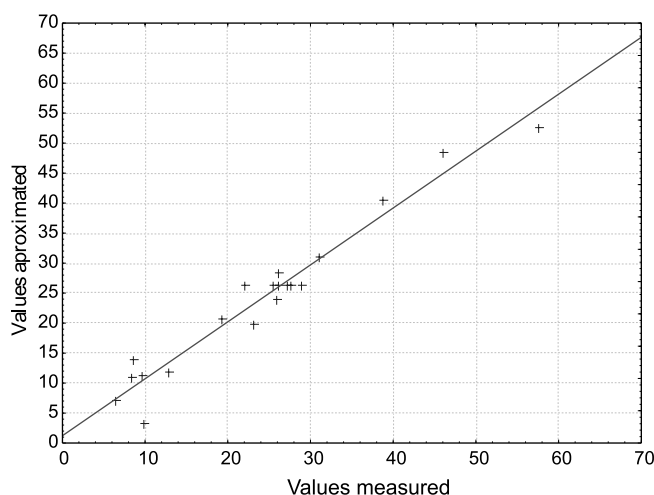
Table 5. The analysis of variance

	Effects	b_i	SS	df	MS	F	P
x_1	-22,98	-11,49	1803,2	1	1803,2	316,1	0,00001
x_2	7,85	3,92	210,1	1	210,1	36,8	0,00175
x_3	14,24	7,12	687,6	1	687,6	120,5	0,00011
x_1^2	5,03	2,52	91,3	1	91,3	16,0	0,01031
x_2^2	-6,20	-3,1	138,6	1	138,6	24,3	0,00436
x_3^2	-5,14	-2,57	92,6	1	92,6	16,2	0,01004
x_1x_2	-1,03	-0,51	2,1	1	2,1	0,4	0,56902
x_1x_3	-5,71	-2,85	65,2	1	65,2	11,4	0,01963
x_2x_3	2,67	1,33	14,3	1	14,3	2,5	0,17451
Lack of fit			122,6	5	24,5	4,3	0,06774
Pure error			28,5	5	5,7		
Total sum of Squares (SS)			3278,6	19			

SS – Sum of Squares, df – degrees of freedom, MS – Mean Square, F – distribution, p – values of probability calculated for F -statistics

Table 6. Basic statistics for the rests

	Av	Med.	Min.	Max.	Range	Variation
CDT conversion	0,0	-0,342	-5,5	6,58	12,09	8,82

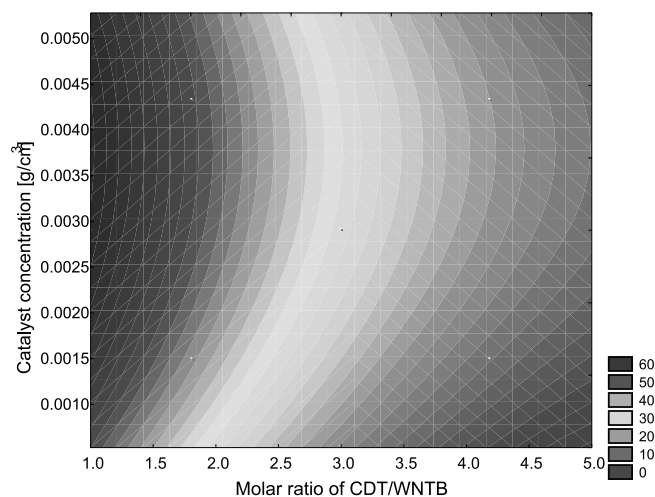
**Figure 2.** A range of rests according to the order of time**Figure 3.** The values measured in the experiments related to the approximate from a certain function for the CDT conversion

ments are spaced uniformly along the central line. It is confirmed by the constancy of the variance of the answer function.

The approximated values approach the real values (Figure 3) quite well. A matching line drawn through these points is at the 45° angle. Bigger deviations are seen at the smaller values of the functions.

The approximated function of the CDT ($Y_{K_{CDT}}$) conversion contains all the main variables which influence its value. Only two interactions (x_1x_2 and x_2x_3) turned out to be not important statistically, thus they were not put into the model. The maximum value of the function $Y_{K_{CDT}} = 66,47\%$, was received with the following values of the input factors: the molar ratio of CDT/TBHP = 1, the $\text{Mo}(\text{CO})_6$ catalyst concentration = 0,004092 and reaction time 120 min.

The influence of the studied process parameters on the CDT conversion was presented by the isoline diagram. For the molar ratio of CDT/TBHP = 1 and the reaction time = 120 min, the change of the catalyst concentration in the whole range from 0,000528 to 0,00528 g/cm³ influences on the CDT conversion, which can take high values under such conditions from 50.0 to 66.7% (Figure 4). An increase in the molar ratio of CDT/TBHP from 1 to 5, at the optimum catalyst concentration, causes a decrease in conversion to about 12%. The calculated values of the CDT conversion are partly correlated to the molar ratio of CDT/TBHP.

**Figure 4.** The influence of the molar ratio of CDT/TBHP and the catalyst concentration on the CDT conversion (reaction time = 120 min.)

The CDT conversion increases with the rise in the reaction time (Figure 5). The largest values of K_{CDT} (>57%) were obtained for the reactions time in the range from 80 to 120 minutes and for the molar ratio of CDT/TBHP = 1. It follows from Figures 5 and 6 that higher values of conversion can be received by extending the reaction time to 120 min.

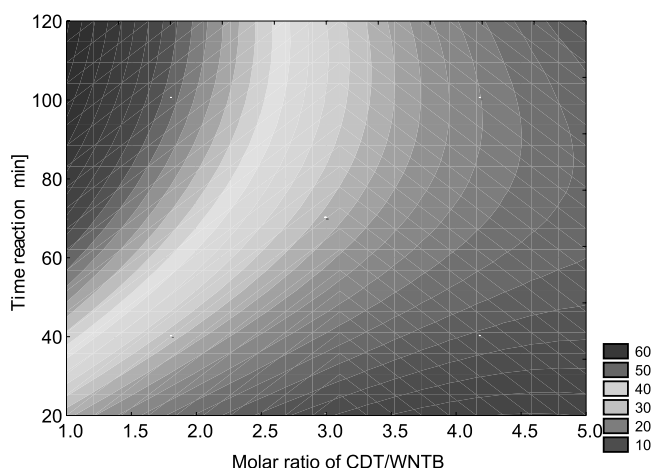


Figure 5. The influence of the molar ratio of CDT/TBHP and the reaction time on the CDT conversion (catalyst concentration – 0,004092 g/cm³)

For the smallest Mo(CO)₆ catalyst concentration (0,000528 g/cm³) and the maximum value of the reaction time (120 min) and the equimolar ratio of CDT/TBHP, the values of the CDT conversion are higher than 40% (Figure 6). Shortening of the reaction time to 20 minutes, at the same catalyst concentration, reduces the CDT conversion to about 10%. An increase in the catalyst concentration to the optimum value at the reaction time – 120 min increases a degree of the reacted CDT to 66,5%, then a slight decrease of conversion happens.

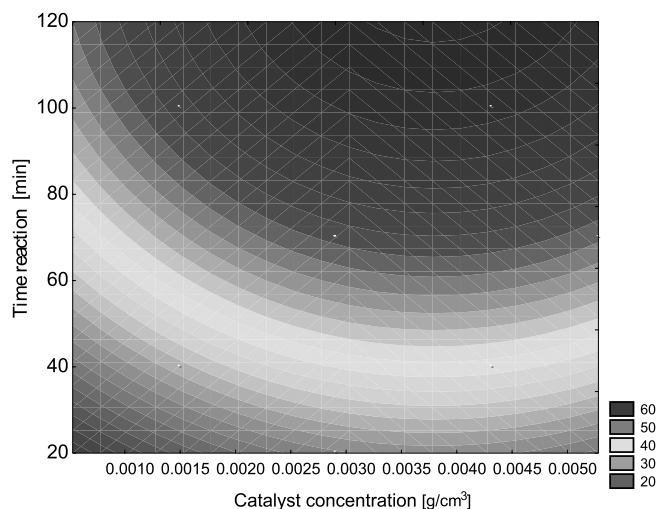


Figure 6. The influence of the catalyst concentration and the reaction time on the CDT conversion (molar ratio of CDT/TBHP = 1)

The biggest positive influence on the value of the CDT conversion has the low molar ratio of CDT/TBHP, the long reaction time and the high catalyst concentration.

CONCLUSIONS

The influence of the molar ratio of CDT/TBHP, the catalyst concentration and the reaction time on the CDT conversion was described by a statistic method of the design of experiments. The received predicative model is well fitted to the real data, which was proved by testing the rests, where no serious deviation was seen. The maximum value of the $Y_{K_{CDT}} = 66,47\%$ function was received at the following values of the input variables: the molar ratio of

CDT/TBHP = 1, the Mo(CO)₆ catalyst concentration = 0,004092 and the reaction time 120 min. It was shown that the low molar ratio of CDT/TBHP, the high catalyst concentration and the long reaction time have positive influence on the CDT conversion.

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