



Ars Separatoria Acta 7 (2009/2010)
99-107

**ARS
SEPARATORIA
ACTA**

www.arsseparatoriaacta.com

KINETICS OF DRYING SELECTED VEGETABLES IN FOUNTAIN BED

Edward SOBCZAK, Krzysztof ŻYWOCIŃSKI¹⁾, Jerzy KASPRZAK²⁾

¹⁾University of Technology and Life Sciences, Faculty of Chemical
Technology and Engineering, Seminaryjna 3, 85-326 Bydgoszcz, Poland

²⁾Provincial Sanitary and Epidemiological Station in Bydgoszcz
e-mail: krzysztofzywocinski@utp.edu.pl

ABSTRACT

The results of drying kinetics are usually correlated with the linear flow of evaporated water depending on its content in the dried material. Investigation into the kinetics of drying vegetables such as: carrot, parsley, radish, celery and red beet, was the main aim of the present work in the bed fountain at temperatures close to ambient temperatures. Another aim of these investigations was to study the influence on the process of its three basic parameters: time, temperature, and moisture.

Keywords: vegetables, fountain bed, drying

INTRODUCTION

Drying by removing moisture from raw material by means of heat is a good way of food preservation. It is a very effective and economical method. Products obtained in the process are characterized by excellent stability. It is notable that not all materials can be dried by the same method. The development of various drying facilities allowed to develop many methods and ways of drying, which enables the application of the optimum conditions for a particular material and minimization of the loss of key ingredients from foods.

The drying process minimizes enzymatic and non-enzymatic conversion. Protection against microbial and mould growth is usually achieved by lowering the water content in the product to about 15%. However, to inhibit enzymatic and non-enzymatic conversion it was required to reduce water content in the product to quantities below 5%.

Drying should take place at temperatures from 60°C to 80°C. It must be remembered that excess temperatures cause denaturation of proteins of which the strength is lower in more humid environments.

A product dried at too high temperatures shows an ability to absorb water. Application of temperatures above 100°C leads to the decomposition and caramelization of sugar and, therefore, to the loss of dry matter and obtaining a dark brown colour of the dried product. The rate of evaporation of water is highly influenced by fragmentation of raw vegetables. If drying proceeds too rapidly, a very rapid evaporation of moisture follows from the surface layers of the product, with the result produced on the outside shell, which impedes the evaporation of water from deeper layers. Raw materials may be burned in certain places and not fully dried in other ones [1].

Application in the drying process of fluid fountain, which is the case of the fluidized bed [5, 6], enables the process to be conducted most efficiently.

The results of drying kinetics are usually correlated with the linear flow of evaporated water depending on its content in the dried material. The obtained values of the kinetic coefficient of the drying process depend on the particle size and hygroscopic properties, velocity, temperature and relative humidity [2, 7].

Investigation into the kinetics of drying vegetables such as: carrot, parsley, radish, celery and red beet, was the main aim of the present work in the bed fountain at temperatures close to ambient temperatures.

Another aim of these investigations was to study the influence on the process of its three basic parameters: time, temperature, and moisture.

METHODS

The vegetables used in the study were: carrot, parsley, radish, celery and beetroot. The vegetables were initially dehydrated in a juice extractor. After obtaining a vegetable press the corresponding five saponification-charges were prepared. Two samples, each weighing 50 g, were placed in a drying chamber for a period of seven days at 50°C to determine the weight of dry matter. However, three attempts at 200 g each were used for drying in a fluid fountain in three different times: 15, 30, 45 minutes. Before proceeding to drying at elevated temperatures a fan heater was started and then the drier fountain was filled with 200 g of the vegetable press. To prevent stripping away of the smallest dried particles of material a lid with a grid of mesh size 0.05 mm was used.

The successive trials in the drying fountain lasted 15, 30 or 45 minutes. The time and temperature of the process were strictly controlled. After the time had lapsed, the water mass loss was measured by weighing the sample by means of an electronic scale with an accuracy to 0.001 g. Immediately after the process, the sample was placed in a drying chamber for a period of seven days at 50°C.

The test was conducted in the air stream collected from the surroundings heated to temperatures in the range 30÷40°C, and not heated at temperatures in

the range 8÷16°C. The same vegetables were used in both cases, which enabled determination of the effect of temperature on the drying kinetics.

The study of the drying kinetics in the air stream in a fluid fountain was conducted in the camera; the pattern shown is in Figure 1.

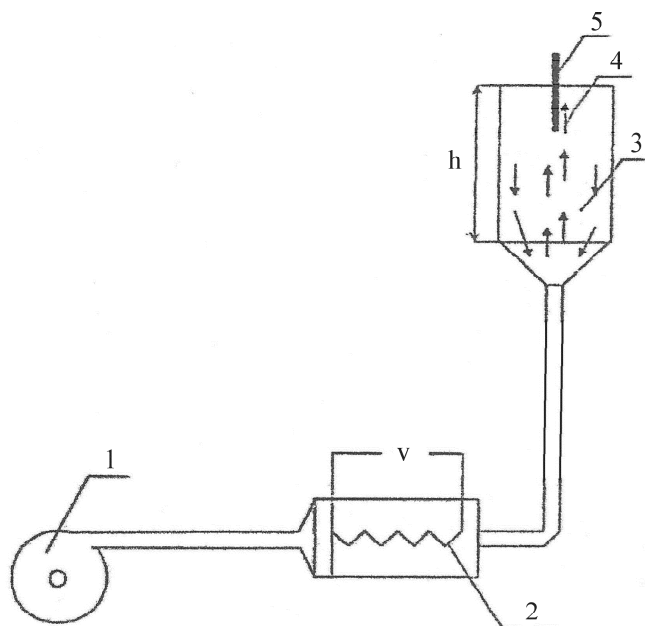


Fig. 1. Diagram of drying apparatus: 1 – blowing fan, 2 – air heater, 3 – chamber, 4 – dried material in fountain bed, 5 – thermometer.

Drying was held in a conical chamber of which the height was about 320 mm, inlet diameter 50 mm and outlet diameter 180 mm. The flow rate of the stream of air carried out by the deposit was $20 \text{ dm}^3 \cdot \text{s}^{-1}$. Temperature was measured in the interior deposit of the fountain bed at 5 min time intervals. The results of the measurements: temperature t , sample mass before drying M_0 , sample mass after drying in the fountain deposit M_1 , mass after drying in the chamber dryer M_{S1} , content of dry matter after drying in the chamber dryer m_s in a sample of the mass m_0 were given in Table 1.

RESULTS AND DISCUSSION

Due to the possibility of material loss during the sample on drying, dry mass M_S was calculated on the basis of the dry matter content in a 1 g sample (m_s/m_0):

$$M_S = \frac{m_s}{m_0} M_0 \quad (1)$$

where:

- M_S – dry matter contained in sample M_0 , [g],
- m_S – dry matter received from sample of mass m_0 , [g],
- M_0 – the mass used to drying in fountain bed, [g].

From the above, the content of water $M_{w0} = M_0 - M_S$ in the sample M_0 .

Based on the moisture content in the sample after drying ($M_1 - M_{S1}$) in a fluid fountain M_{w1} the mass of water in the sample to dry M_S was calculated:

$$M_{w1} = \frac{M_1 - M_{S1}}{M_{S1}} M_S \quad (2)$$

where:

- M_{w1} – the mass of water contained in the sample after drying in fountain bed, [g].

Equation of the speed of drying:

$$-\frac{dM_w}{d\tau} = kP_w M_w \quad (3)$$

where:

- P_w – saturated vapour pressure [kPa].

After transformation of Equation (3) the mass of water M_w was determined in a dried analytical sample in drying time:

$$M_w = M_{w0} \exp(-kP_w \tau) \quad (4)$$

or

$$y = \frac{M_w}{M_{w0}} = a_0 \exp(-kx) \quad (5)$$

where:

- τ – time of drying in fountain bed, [h],
- P_w – saturated vapour pressure at drying temperature, [kPa],
- x = $(P_w \cdot \tau)$ [kPa · h],
- a_0 = 1.

Table 1. Drying in heater air (round 1).

| Raw material | Sample no. | Mass before drying in chamber drier m_0 [g] | Mass after drying in chamber drier m_s [g] | Mass before drying in fountain bed M_0 [g] | Mass after drying in fountain bed M_1 [g] | Mass after drying in chamber drier (period 7 days) M_{s1} [g] | Process temperature t [°C] | Drying time τ [h] |
|--------------|------------|--|---|---|--|--|---------------------------------|---------------------------|
| Carrot | I | 50 | 7.1 | 200 | 111.2 | 26.3 | 35.5 | 0.25 |
| | II | | | 200 | 59.9 | 25.5 | 38 | 0.5 |
| | III | | | 200 | 27.9 | 23.7 | 39.5 | 0.75 |
| Parsley | I | 50 | 10.6 | 200 | 70 | 39 | 34 | 0.25 |
| | II | | | 200 | 45.4 | 39.6 | 34 | 0.5 |
| | III | | | 200 | 30.3 | 26.5 | 37 | 0.75 |
| Radish | I | 50 | 4.95 | 200 | 68.9 | 20 | 34.5 | 0.25 |
| | II | | | 200 | 37.3 | 19.9 | 36 | 0.5 |
| | III | | | 200 | 24.6 | 18.8 | 38.5 | 0.75 |
| Celery | I | 50 | 6.8 | 200 | 88.7 | 25.1 | 30 | 0.25 |
| | II | | | 200 | 37.6 | 27.1 | 30 | 0.5 |
| | III | | | 200 | 26.9 | 22.6 | 31.5 | 0.75 |
| Red beet | I | 50 | 8.65 | 200 | 130.6 | 33.8 | 31 | 0.25 |
| | II | | | 200 | 64.3 | 32.4 | 32.5 | 0.5 |
| | III | | | 200 | 31.8 | 27.7 | 37.5 | 0.75 |

Table 2. Drying in cool air (round 2).

| Raw material | Sample no. | Mass before drying in chamber drier m_0 [g] | Mass after drying in chamber drier m_s [g] | Mass before drying in fountain bed M_0 [g] | Mass after drying in fountain bed M_1 [g] | Mass after drying in chamber drier (period 7 days) M_{s1} [g] | Process temperature t [°C] | Drying time τ [h] |
|--------------|------------|--|---|---|--|--|---------------------------------|---------------------------|
| Carrot | I | 50 | 8.2 | 200 | 131.5 | 32.3 | 15 | 0.25 |
| | II | | | 200 | 121.5 | 30.8 | 16 | 0.5 |
| | III | | | 200 | 105.9 | 28.8 | 15.5 | 0.75 |
| Parsley | I | 50 | 13.7 | 200 | 175.4 | 58.1 | 8.5 | 0.25 |
| | II | | | 200 | 144.9 | 56.9 | 9 | 0.5 |
| | III | | | 200 | 117.5 | 51.3 | 9 | 0.75 |
| Radish | I | 50 | 4.7 | 200 | 164.4 | 19.8 | 9 | 0.25 |
| | II | | | 200 | 148.2 | 20 | 8.5 | 0.5 |
| | III | | | 200 | 108.3 | 18.6 | 9 | 0.75 |
| Celery | I | 50 | 7.75 | 200 | 159.1 | 31.1 | 15 | 0.25 |
| | II | | | 200 | 119.4 | 30.6 | 14.5 | 0.5 |
| | III | | | 200 | 83.0 | 29.9 | 14 | 0.75 |
| Red beet | I | 50 | 8.5 | 200 | 149.3 | 35.9 | 9.5 | 0.25 |
| | II | | | 200 | 118.7 | 37.1 | 8 | 0.5 |
| | III | | | 200 | 87.7 | 33.8 | 9.5 | 0.75 |

Table 3. Drying in heater air (round 1).

| Raw material | Sample no. | Dry matter content M_s [g] | Water content in sample before drying in fountain bed M_{w0} [g] | Water content in sample after drying in fountain bed M_{w1} [g] | Saturate vapour pressure at fountain bed temperature P_{wv} [kPa] | Coefficient k |
|--------------|------------|---------------------------------|---|--|--|-----------------|
| | | | | | | |
| Carrot | I | 28.4 | 171.6 | 91.67 | 5.6227 | 0.4460 |
| | II | | | 38.31 | 6.6229 | 0.4526 |
| | III | | | 5.03 | 6.9915 | 0.6731 |
| Parsley | I | 42.4 | 157.6 | 33.7 | 5.3192 | 1.16 |
| | II | | | 6.21 | 5.3192 | 1.2159 |
| | III | | | 6.08 | 6.2749 | 0.6916 |
| Radish | I | 19.8 | 180.2 | 48.4 | 5.3192 | 0.9885 |
| | II | | | 17.3 | 5.9411 | 0.7888 |
| | III | | | 6.1 | 6.6249 | 0.6814 |
| Celery | I | 27.2 | 172.8 | 68.9 | 4.2427 | 0.8669 |
| | II | | | 10.5 | 4.2427 | 1.3202 |
| | III | | | 5.2 | 4.4922 | 1.0399 |
| Red beet | I | 34.6 | 165.4 | 99.0 | 4.4922 | 0.4570 |
| | II | | | 34.0 | 4.7545 | 0.6655 |
| | III | | | 5.12 | 6.2749 | 0.7384 |

Table 4. Drying in cool air (round 2).

| Raw material | Sample no. | Dry matter content | Water content in sample before drying in fountain bed | Water content in sample after drying in fountain bed | Saturate vapour pressure at fountain bed temperature | Coefficient k |
|--------------|------------|--------------------|---|--|--|-----------------|
| | | M_s [g] | M_{w0} [g] | M_{w1} [g] | P_{wv} [kPa] | |
| Carrot | I | 32.8 | 167.2 | 100.8 | 1.7048 | 1.1874 |
| | II | | | 96.5 | 1.8176 | 0.6048 |
| | III | | | 87.8 | 1.7048 | 0.5038 |
| Parsley | I | 54.8 | 145.2 | 110.6 | 1.116 | 0.9756 |
| | II | | | 84.7 | 1.1847 | 0.9099 |
| | III | | | 70.7 | 1.1847 | 0.8099 |
| Radish | I | 18.8 | 181.2 | 137.2 | 1.1847 | 0.9391 |
| | II | | | 120.5 | 1.116 | 0.7311 |
| | III | | | 90.7 | 1.1847 | 0.7789 |
| Celery | I | 31.2 | 168.8 | 128.4 | 1.7048 | 0.6419 |
| | II | | | 90.5 | 1.5981 | 0.7801 |
| | III | | | 55.4 | 1.5981 | 0.9295 |
| Red beet | I | 34 | 166 | 107.4 | 1.1847 | 1.4702 |
| | II | | | 73.9 | 1.116 | 1.4503 |
| | III | | | 54.21 | 1.1847 | 1.2595 |

CONCLUSIONS

- The kinetic coefficient, k , of drying in fountain bed for five vegetables and three drying periods was determined:
 - during drying in a stream of ambient air the kinetic coefficient ranges from 0.5 – 1.5 [h · kPa]. The lowest value was obtained for the carrot, and the highest for the beet root,
 - when drying in a stream of air heated to about 25°C, the kinetic coefficient ranges from 0.4 to 1.3 [h · kPa]. The lowest value was obtained for the coefficient of carrots, and the highest for celery.

REFERENCES

- [1] Kłossowski T., 1997. Zarys technologii przemysłu spożywczego. WNT Warszawa.
- [2] Pijanowski E., Dłużewski M., Dłużewska A., Jarczyk A., 1997. Ogólna technologia żywności. WNT Warszawa.
- [3] Marrae R., Robinson E.K., Sadler H.J., 1993. Encyclopaedia of Food Science, Food Technology and Nutrition. Academic Press London.
- [4] Pabis S., 1982. Teoria konwekcyjnego suszenia produktów rolniczych. PWRiL Warszawa.
- [5] Kneule F., 1970. Suszenie. Arkady Warszawa.
- [6] Serwiński M., 1971. Zasady inżynierii chemicznej operacje jednostkowe. WNT Warszawa.
- [7] Strumiłło Cz., 1983. Podstawy teorii i techniki suszenia. WNT Warszawa.