

APPLICATION OF STRAIN GAUGES IN MEASUREMENTS OF STRAIN DISTRIBUTION IN COMPLEX OBJECTS

Piotr Tutak

IT Institute, University of Social Sciences, Łódź, Poland

piotrtutak@wp.pl

Abstract

This article presents an application of strain gauges in measurements of strain which occurs in charge air cooler during the thermal cycle test. The work shows the main idea of measuring system based on strain gauges and important aspects that should be considered when performing measurement. In this article there has been also presented construction and principle operation of a strain gauge measurement system.

Key words: strain gauge, FEA, charge air cooler, thermal cycle.

1 Introduction

Strain gauges measurements play an important role in many industrial sectors. Appropriate measurements systems can define the strain level occurring in different construction from biomechanics to civil engineering. Based on strain, life time and threat of specific construction can be calculated. This article shows application of strain gauges in strain measurements for charge air cooler during thermal cycle test.

1.1 A Strain gauge

A Strain gauge (Figure 1) is a sensor used to measure strain. It has a conductive grid, which changes its electrical resistance when it is deformed. Grid deformation is caused by forces coming from the loaded object to which the strain gauge is mounted by bonding. The strain gauge produces an output change of resistance corresponding to a physical change of the investigated object.

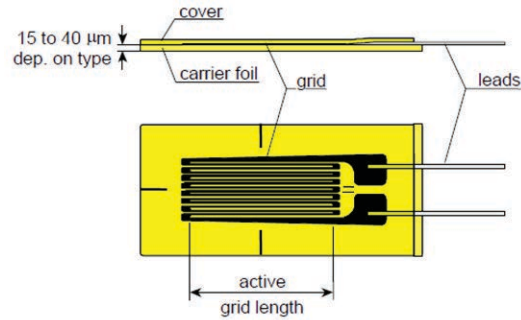


Figure 1. Strain gauge construction[www.hbm.com]

Functions of individual strain gauge's components presents Table 1.

Table 1. Strain gauge construction [own work]

Strain gauge component	Function
Grid	strain measurement as change of resistance
Carrier foil	base for grid on investigated object
Cover	protection against pollution
Leads	connection with measuring device

The strain gauge principle of operation is based on Equation (1). When the strain gauge is subjected to tensile or compressive forces, it changes its length and cross-section which affects change of the resistance.

$$R = \rho \frac{l}{S} \quad (1)$$

where:

R –electrical resistance [Ω]

ρ –electrical resistivity [$\Omega \cdot m$]

l – length [m]

s – cross section area [m^2]

The change of resistance is proportional to the change of the length, Equation (2).

$$\frac{\Delta R}{R} \sim \frac{\Delta L}{L_0} \quad (2)$$

where:

ΔL – difference between initial length L_0 and final L [m]

L_0 – initial length [m]

ΔR – change of resistance [Ω]

R – resistance [Ω]

The difference between absolute and relative change in length presents Fig. 2.

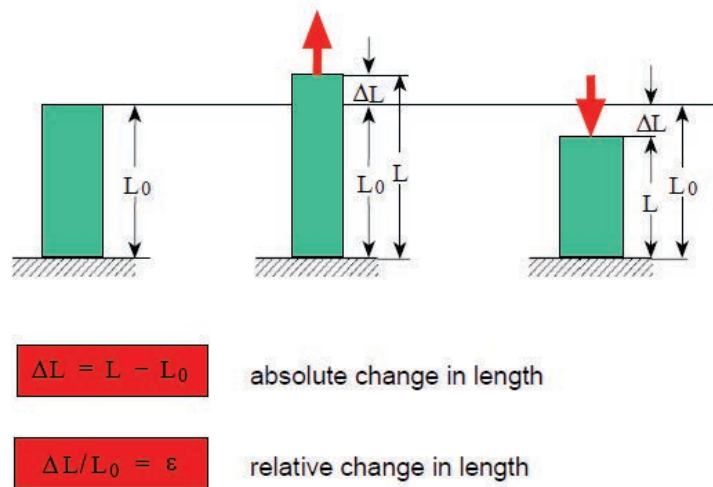


Figure 2. Absolute and relative length change[www.hbm.com]

Strain is the ratio of length change to the initial length of sample, Equation (3).

$$\varepsilon = \frac{\Delta L}{L_0} \quad (3)$$

Based on Equation (2) and Equation (3) we obtain Equation (4).

$$\frac{\Delta R}{R} \sim \varepsilon \quad (4)$$

where:

ε – strain [$\mu m/m$]

The proportional sign in Equation (4) can be replaced by a constant k , which is characteristic for the individual strain gauge and gives connection between resistance change and strain, Equation (5).

$$\frac{\Delta R}{R} = k \cdot \varepsilon \quad (5)$$

Because ΔL is very small, the magnitude $10^{-6} m$ for strain ε commonly used unit is $\mu m/m$. When selecting strain gauge following criteria should be taken in consideration:

- Material to which the strain gauge temperature response is matched
- Measuring grid resistance
- Maximum permissible effective bridge excitation voltage
- Number of measuring grid, their dimensions and positions to each other's

When the strain gauge has been selected, another important aspect is to use suitable adhesive and covering material adapted to working conditions, mainly in terms of the operating temperature. Figure 3 presents fully installed strain gauge on the object.

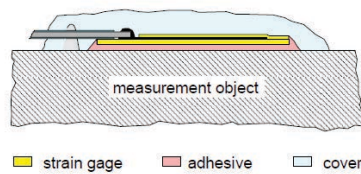


Figure 3. Properly installed strain gauge on object[www.hbm.com]

1.2 A Wheatstone bridge

A Wheatstone bridge (Fig.4) is an electrical circuit that consists of four resistive elements R_1 , R_2 , R_3 and R_4 . On each of four legs of the Wheatstone bridge depending on bridge configuration can be placed a resistor or a strain gauge which changes its electrical resistance when it is deformed by forces from the investigated object.

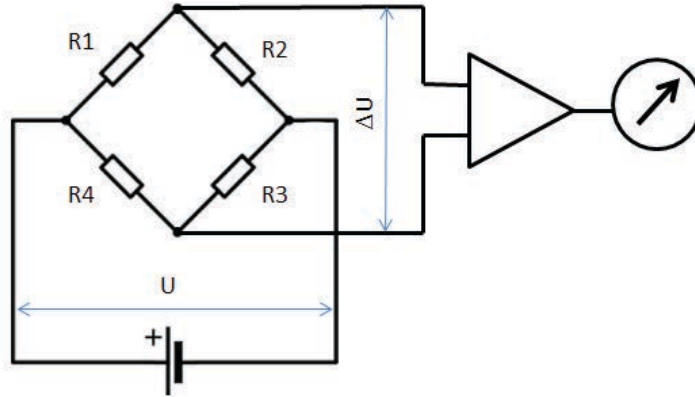


Figure 4. Wheatstone bridge circuit [own work]

The Wheatstone bridge works based on voltage division rule. Namely, in bridge there are two parallel voltage divider circuits between nodes D and B: the first one is R_1 and R_2 and the second one is R_3 and R_4 . The output signal of Wheatstone bridge is measured between nodes A and C. Then the signal is amplified and recorded. By means of the Wheatstone bridge very small variations in resistance can be measured on the level $10^{-4}\Omega$. The change in the resistance of Wheatstone bridge is calculated by measuring device as the strain. Strain can be positive (tensile) or negative (compressive). The magnitude of strain is very small that is why strain is often expressed as micro strain which means 10^{-6} , instead of using common expression for this type of measurements for example mm/mm.

The number of the active element in the Wheatstone bridge determines the kind of bridge configuration. There are three types of bridge configurations:

- quarter-bridge,
- half-bridge
- full-bridge.

Table 1 presents number of active strain gauge in each bridge configuration.

Table 2. Wheatstone bridge type definition [own work]

Bridge configuration	Number of active Stain gauge
Quarter-bridge	1
Half-bridge	2
Full-bridge	4

Full and half bridge are used when the temperature compensation is needed. In case of half bridge there are 2 strain gauges. One is located in strain area and the second one is placed where there is no strain. For both strain gauges the temperature must be the same in order that the second strain gauge could compensate the impact of the temperature on the strain measured by the loaded strain gauge. Similar, for full bridge configuration but there are 4 strain gauges. Two elements perpendicular to each other's in strain area and the other two in area where there is no strain. It is possible also to compensate the impact of temperature on strain in case of quarter bridge but a thermocouple is needed to record the temperature.

1.3 Wheatstone bridge for thermal cycle

In case of measurements connected with thermal cycle test the bridge configuration is set as quarter with four wires strain gauge connection. Major strain in a charge air cooler is caused by tube extension when the charge air temperature changes from lower to upper limit. Due to the time limitation, compensation of temperature was not included in the strain results presented in this article (Table 3) but the calculated error on the level 5% is acceptable. However, the temperature was recorded and can be used to compensate the test results. Four wires strain gauges connection is used to compensate heat of the cables which ensures better signal quality than two wires connection and eliminates potential noise.

2 Measuring system

Measuring system was based on HBM Device MGCplusAB22A (Fig.5). The bridge was configured as quarter with four wires strain gauge connection. Four strain gauges Vishay SG 350 Ohm WK-13-125BT-350 were used in the measurement.

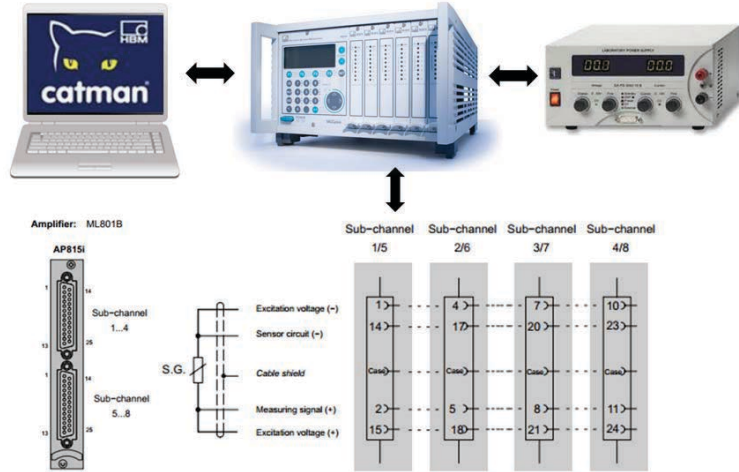


Figure 5. Measuring system[www.hbm.com]

All strain measurements were managed by CATMAN Easy software (Fig.6).

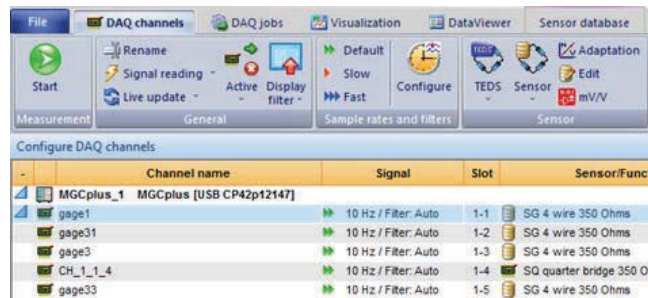


Figure 6. CATMAN Easy software[www.hbm.com]

The sampling frequency was set for 10 samples per second and the data was recorded for five minutes for each of stand configuration.

3 Measurement

The object of the strain measurements is a Charge Air Cooler (Fig.7). It has an aluminum core that consists of set of tubes, cooling types called air centers, two reinforcements and headers. On the both ends of the exchanger

there are plastic tanks. Tightness of the system is ensured by gaskets placed between core and tanks.

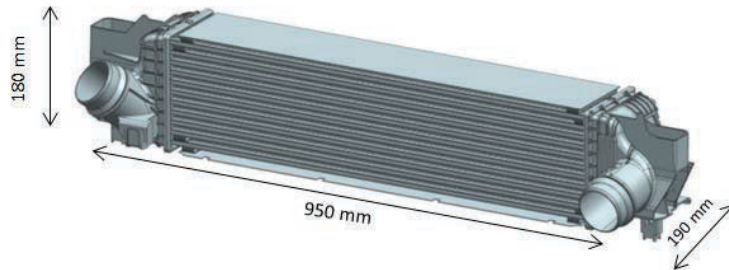


Figure 7. Charge air cooler [own work]

The aim of the measurement was to measure strain which occurs in the charge air cooler's tubes with different parameters and configurations of the thermal cycle test stand (Fig.8).

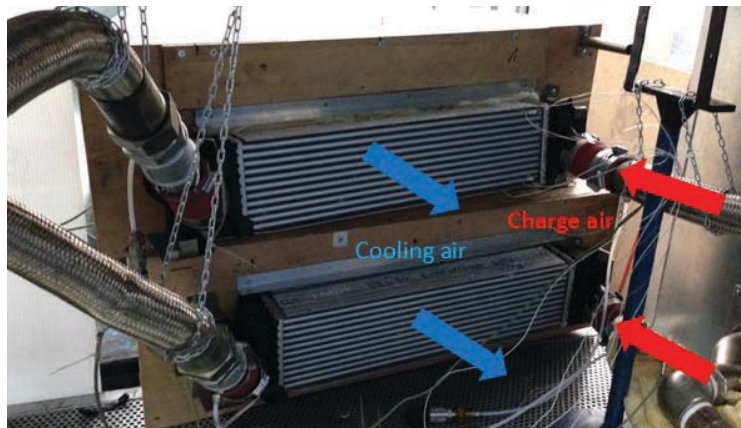


Figure 8. Thermal cycle test [own work]

The thermal cycle test relies on applying on the inlet side of the exchanger the charge air with specific flow, pressure and temperature changing in time. The another point of the test is cooling the core by external air.

Four strain gauges and thermocouples were glued on places where occurs the biggest stress level (Fig. 9).

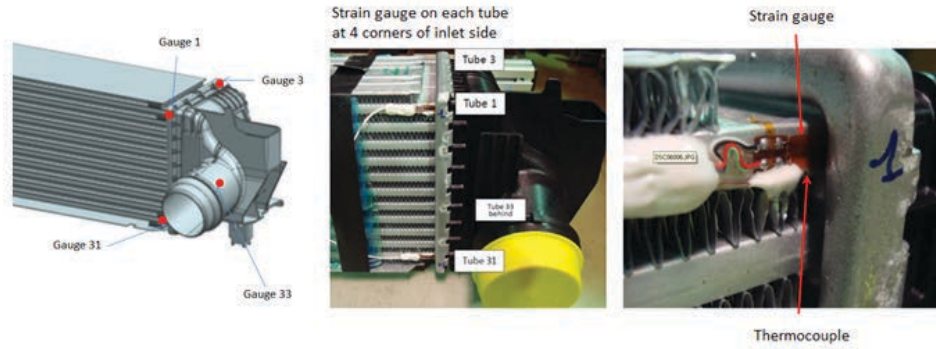


Figure 9. Strain gauge and thermocouples location [own work]

The exact position of sensors were defined by Finished Element Analysis. The most stressed places of the charge air cooler are the four external tubes on the inlet side close to the header (Fig. 10).

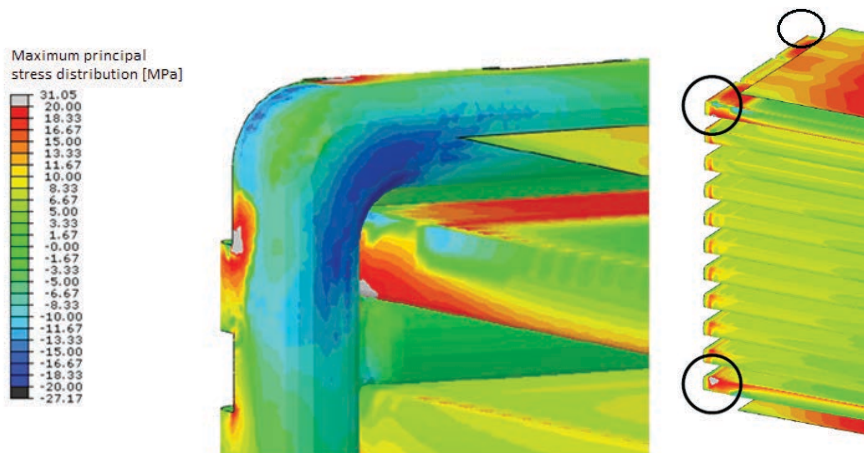


Figure 10. Maximum stressed places by FEA [own work]

Strain gauges measurements were done with different test parameters and test stand configuration (Table 3). During the measurements there was changed the maximum temperature of the charge air and ramp time which means the speed of the change of temperature from lower to upper limit. There were also changes of flow, external air speed and temperature. From stand configuration the size of the duct which provides external air has been also changed to supply cooling air on different area of the charge air cooler.

Table 3. Strain and temperature measurements [own work]

Id	Internal Air				External Air		Measured magnitude strain [µm/m] temp. [°C]	Gage3	Gage33	Gage31	Gage1	Comments
	Low temp. [°C]	High temp. [°C]	Ramp Time [s]	Flow [kg/h]	Temp. [°C]	Speed [m/s]						
1	30	220	30	600	20	8,1	Strain	563	635	922	475	
							Temp.	130	145	175	170	
2	30	220	30	600	-	-	Strain	908	1459	1054	569	No external flow
							Temp.	200	200	200	200	
3	30	220	30	600	20	8,1	Strain	715	649	794	507	Shutdown flow during cold phase
							Temp.	130	145	170	170	
4	30	220	30	600	24	10	Strain	584	529	685	454	
							Temp.	125	140	170	165	
5	30	190	30	600	20	8,1	Strain	540	560	755	410	
							Temp.	115	125	150	147	
6	30	160	30	600	20	8,1	Strain	452	438	570	374	
							Temp.	100	108	128	125	
7	30	220	30	440	20	8,1	Strain	533	458	716	407	
							Temp.	125	140	170	165	
8	30	220	6	440	20	8,1	Strain	529	376	763	476	
							Temp.	125	125	165	175	
9	30	190	6	440	20	8,1	Strain	472	344	678	438	Passed real test
							Temp.	110	110	140	150	
10	30	190	6	600	20	8,1	Strain	513	390	719	457	
							Temp.	115	115	150	160	
11	30	220	6	600	20	8,1	Strain	569	447	813	507	Failed real test
							Temp.	130	135	175	185	
12	30	220	6	600	20	10	Strain	549	433	746	485	
							Temp.	125	130	170	180	
13	30	220	6	600	20	5	Strain	631	589	895	543	
							Temp.	140	145	185	195	
14	30	220	6	600	35	8,1	Strain	548	447	763	497	
							Temp.	135	140	175	185	
15	30	220	6	600	35	10	Strain	518	444	716	474	
							Temp.	130	135	170	175	
16	30	220	6	600	35	12	Strain	788	839	838	576	
							Temp.	150	175	195	205	
17	30	220	6	600	35	10	Strain	758	840	828	582	Small duct
							Temp.	155	175	195	210	
18	30	220	6	600	20	10	Strain	744	812	809	551	
							Temp.	150	175	195	205	

From the Table 3 we can see that the main impact on the strain result is coming from external air and ramp time. Based on data from real test Table 3 we are able to identify what parameters have the biggest impact on the test result of the thermal cycle test for charge air cooler.

4 Conclusion

Correlation strain and stress from FEA with real measurements it is not easy task because the performed simulation is simplified versus the real test. However, the most stressed places pointed by FEA are in line with failure mode which occurs during the thermal cycle test. Therefore, this approach is correct to indicate where strain gauges should be glued and measurement should take place. The measurements show the strain level of the tubes and the influences of different test parameters to their strain level. Based on this information and real test data we can define what test parameters have the biggest impact on the charge air cooler construction.

References

1. Hoffman K., 1989, An Introduction to Measurements using Strain Gauges, HBM GmbH, Darmstadt.
2. Bathe K. J., 1996, *Finite Element Procedures*, Prentice Hall, New Jersey.
3. Cook R.D., 2002, *Concepts and applications of Finite Element Analysis*, J. Wiley & Sons, New Jersey.
4. Crisfield M.A., 1991, *Non-linear Finite Element Analysis of Solid and Structures*, J. Wiley & Sons, Chichester.
5. Stöcker H., 2010, *Nowoczesne kompendium fizyki*, PWN, Warszawa,
6. Zienkiwicz O.C., 2000, *The Finite Element Method Volume 2: Solid Mechanics*, Oxford.
7. www.pecm.co.uk, access 27.11.2014
8. www.uk.farnell.com, access 27.11.2014
9. www.computerbuddies.co.uk, access 27.11.2014
10. www.vishaypg.com, access 27.11.2014
11. www.hbm.com, access 27.11.2014