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NEURAL NETWORK BASED ADAPTIVE STATE FEEDBACK CONTROLLER FOR INVERTER WITH VOLTAGE MATCHING CIRCUIT

This paper describes a discrete adaptive state feedback controller used to load current control in terms of variable DC voltage of inverter. Controller was designed by using linear quadratic optimization method. Adaptive LQR was used because of non-stationarity of the control system caused by Voltage Matching Circuit - VMC. Gain values of the adaptive controller were approximated by using an artificial neural network. The VMC was realized as an additional buck converter integrated with the main inverter. As the load of the 2-level inverter a 3-phase symmetric RL circuit was used. Simulation tests show the behavior of the load current regulation during DC bus voltage level step changes. The dependence between current RMS value and inverter DC bus voltage level was also shown. Simulation test was made by using Matlab Simulink and PLECS software.

KEYWORDS: adaptive linear-quadratic controller, voltage matching circuit, artificial neural network, current ripple

1. INTRODUCTION

Rectangular shape of the of the converter output voltage produced by using PWM method deteriorates performance of the load operation due to current ripple as well as noise generation [1]. Current ripple generates undesirable noise. Reduction of the current ripple can be realized by using an additional passive LC filter between inverter and load [2] or by using multilevel inverters [3].

In this paper current ripple minimization is realized by using a 2-level voltage source inverter with an additional buck converter [4]. It was necessary to use an adaptive controller to realize current regulation process because Voltage Matching Circuit (VMC) introduces non-stationarity into the control system. A state feedback controller has been used because of ability of control non-stationary systems [5]. The adaptation was realized by an artificial neural network because of good approximation and control abilities [6]. The control behavior and quality is considered in a simulation study. The behavior of the current control loop is investigated during DC bus voltage value changes.

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2. MATHEMATICAL MODEL OF THE SYSTEM

Proposed system topology consist a three-phase RL symmetric circuit fed by a 2-level source voltage inverter. An additional buck converter was introduced to the inverter structure, which serves as a voltage matching circuit (Fig. 2). The block diagram of considered system was shown in Fig. 1

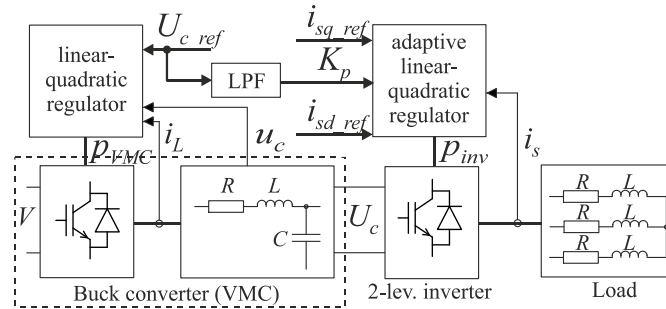


Fig. 1. Proposed control system block diagram

Mathematical model of the VMC is equal to a buck converter model with an LC filter on the output. The equation becomes a following form [4]:

$$\frac{dx_B}{dt} = A_B x_B + B_B u_B + E_B d_B \tag{1}$$

where:

$$x_B = \begin{bmatrix} i_L \\ u_c \end{bmatrix}, A_B = \begin{bmatrix} -\frac{R}{L} & -\frac{1}{L} \\ \frac{1}{C} & 0 \end{bmatrix}, B_B = \begin{bmatrix} \frac{K_{pp}}{L} \\ 0 \end{bmatrix}, E_B = \begin{bmatrix} 0 \\ -\frac{1}{C} \end{bmatrix}, u_B = u_{cc}, d_B = i_o$$

i_L – coil current, u_c – capacitor voltage, R – coil resistance, L –coil inductance, C – capacitor capacitance, K_{pp} – buck converter gain, u_{cc} – input voltage, i_o – load current. Dynamics of the VMC was approximated by using a proportional gain.

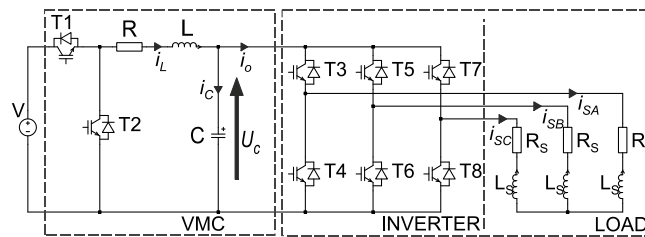


Fig. 2. Topology of the system

The mathematical model of the RL circuit was written in a orthogonal d, q coordinates system in state equation form:

$$\frac{d\mathbf{x}_L}{dt} = \mathbf{A}_L \mathbf{x}_L + \mathbf{B}_L \mathbf{u}_L \quad (2)$$

where:

$$\mathbf{x}_L = \begin{bmatrix} i_{sd} \\ i_{sq} \end{bmatrix}, \mathbf{A}_L = \begin{bmatrix} -\frac{R}{L_s} & 0 \\ 0 & -\frac{R_s}{L_s} \end{bmatrix}, \mathbf{B}_L = \begin{bmatrix} \frac{K_p}{L_s} & 0 \\ 0 & \frac{K_p}{L_s} \end{bmatrix}, \mathbf{u}_L = \begin{bmatrix} u_{dc} \\ u_{qc} \end{bmatrix}$$

u_{dc}, u_{qc} – input voltage spade vector components, i_{dc}, i_{qc} – space vectors of current, R_s – load resistance, L_s – load inductance, K_p – variable inverter gain ($K_p = U_c/2$).

Note that the model of the load is non-stationary due variable inverter gain in matrix B_L due using VMC.

3. VMC CONTROLLER STRUCTURE

To realize the DC bus voltage control, there was used a discrete state feedback controller. In order to determine the controller gain values, a linear-quadratic optimization method has been used. It was necessary to introduce an internal model of the reference signal to eliminate DC voltage steady-state error. The extended state equation takes the following form [7]:

$$\frac{d\mathbf{x}_{BI}}{dt} = \mathbf{A}_{BI} \mathbf{x}_{BI} + \mathbf{B}_{BI} u_{BI} + \mathbf{F}_{BI} r_{BI} \quad (3)$$

where:

$$\mathbf{x}_{BI} = \begin{bmatrix} i_L \\ u_c \\ e_u \end{bmatrix}, \mathbf{A}_{BI} = \begin{bmatrix} -\frac{R}{L} & -\frac{1}{C} & 0 \\ \frac{1}{L} & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}, \mathbf{B}_{BI} = \begin{bmatrix} \frac{K_{pp}}{L} \\ 0 \\ 0 \end{bmatrix}, \mathbf{F}_{BI} = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix},$$

$$u_{BI} = u_B, r_{BI} = u_{cref}$$

u_{cref} – reference value of the DC voltage. The third state variable (DC voltage error) is described by the following equation:

$$e_u(t) = \int_0^t [u_c(\tau) - u_{cref}(\tau)] d\tau \quad (4)$$

To calculate the gains of the discrete linear-quadratic regulator the Matlab's *lqrd* function was used. Following penalty matrices were determined:

$$\mathbf{Q}_{BI} = \begin{bmatrix} 1 \cdot 10^{-3} & 0 & 0 \\ 0 & 4 \cdot 10^{-3} & 0 \\ 0 & 0 & 3 \cdot 10^3 \end{bmatrix}, \quad R_{BI} = I \quad (5)$$

Values of the matrices were selected empirically to achieve the maximum permissible dynamics in the linear area of modulation. It was very important to ensure zero steady-state voltage error for load current step changes as well as the reference voltage changes.

4. INVERTER CONTROLLER STRUCTURE

In order to realize the i_s current regulation a discrete state feedback controller has been used. In case of a regulated DC bus voltage the mathematical plant model would be non-stationary. The current regulation in each axis can be considered independently, because in a symmetric RL circuit doesn't exist any correlation between the current in d and q axis in a orthogonal coordinates system. The extended state equation of the receiver with inverter is as follow [7]:

$$\frac{d\mathbf{x}_{LI}}{dt} = \mathbf{A}_{LI}\mathbf{x}_{LI} + \mathbf{B}_{LI}u_{LI} + \mathbf{F}_{LI}r_{LI} \quad (6)$$

where:

$$\mathbf{x}_{LI} = \begin{bmatrix} i_{sd|sq} \\ e_{isd|sq} \end{bmatrix}, \quad \mathbf{A}_{LI} = \begin{bmatrix} -\frac{R_S}{L_S} & 0 \\ 1 & 0 \end{bmatrix}, \quad \mathbf{B}_{LI} = \begin{bmatrix} \frac{K_p}{L_S} \\ 0 \end{bmatrix}, \quad \mathbf{F}_{LI} = \begin{bmatrix} 0 \\ -1 \end{bmatrix}$$

$$u_{LI} = u_{sd|sq}, r_{LI} = i_{sd|sqref}$$

The variables e_{isd} and e_{isq} correspond to the integral of current error in d and q axis accordingly:

$$e_{isd|sq}(t) = \int_0^t [i_{sd|sq}(\tau) - i_{sdref|sqref}(\tau)] d\tau \quad (7)$$

where: i_{sdref} , i_{sqref} – reference value of the current in d and q axis. The input matrix \mathbf{B}_{LI} is non-stationary because of the presence of variable gain K_p . In such a case it was necessary to create an adaptive discrete state controller. Matlab's *lqrd* function has been used to calculate the gain coefficients of the controller (Fig. 3).

To calculate the variable controller gain values the following penalty matrices has been used:

$$Q_{LI} = \begin{bmatrix} 1 \cdot 10^{-1} & 0 \\ 0 & 5 \cdot 10^4 \end{bmatrix}, \quad R_{LI} = 1 \cdot 10^{-3} \quad (8)$$

The non-linear dependences presented in Fig. 3 were approximated by using artificial neural network. The controller coefficients can be successfully approximated with an artificial neural network with 4 neurons in the first layer and 2 neurons in the output layer. The mean square error was less than $1 \cdot 10^{-7}$ after 438 iterations. Structure of the designed controller was shown below (Fig. 4). The neural network is used to determine controller gain coefficients depending on the VMC voltage level (inverter gain value).

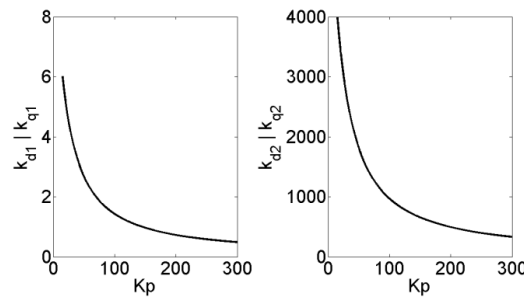


Fig. 3. Dependence between controller coefficients and inverter gain

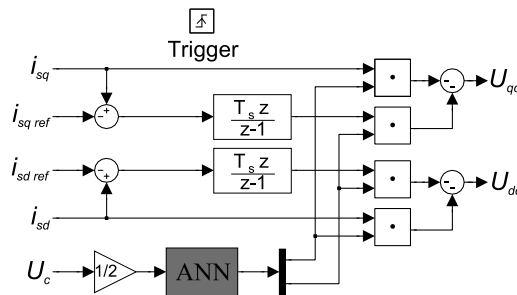


Fig. 4. Adaptive discrete state feedback controller structure

5. SIMULATION RESULTS

The proposed adaptive regulation system of the 2 level inverter with VMC has been simulated in a Matlab/Simulink/PLECS environment (Fig. 5). The designed controllers and measurement units were implemented as triggered discrete subsystems. It was necessary to ensure proper generation of the control systems. Measure blocks are triggered by a synchronization signal in the midpoint of the PWM length to provide measurement of the average signal value. The switching

frequency of the buck converter was set by $f_{s1} = 50$ kHz, while the voltage inverter switching frequency was set by $f_{s2} = 12$ kHz.

The simulations shows the behavior of the system in case of current step response during VMC voltage step changes (Fig. 6). The current error value in steady state is zero though DC voltage changes. The adaptation algorithm properly controls the load current.

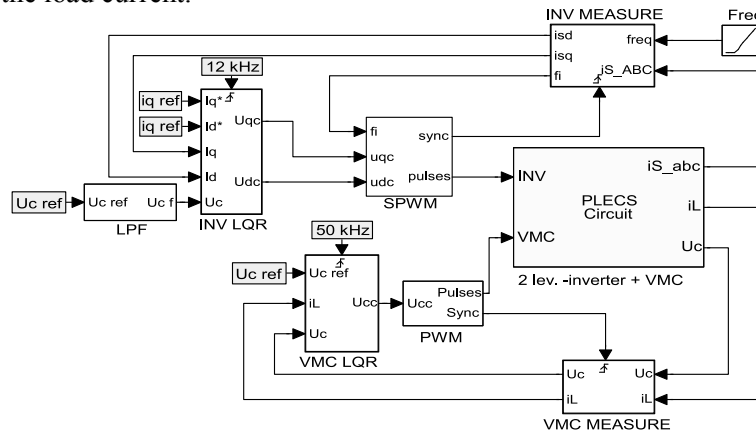


Fig. 5. Schematic diagram of the designed control system

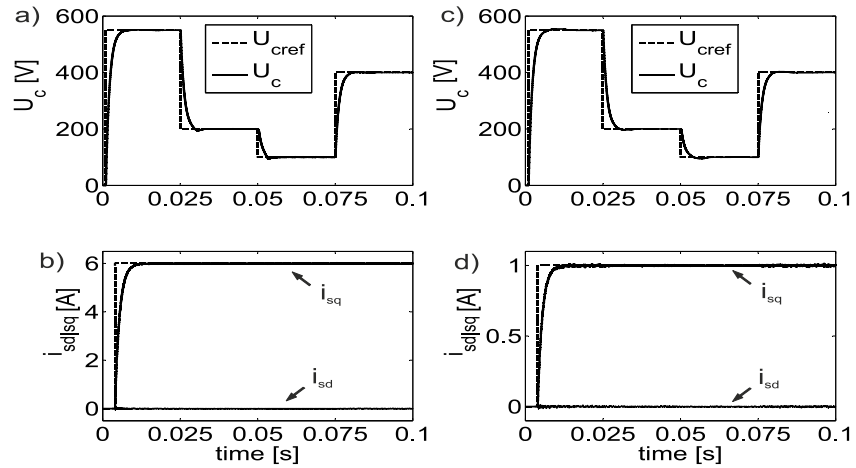


Fig. 6. Receiver current step response during VMC voltage changes

The root mean square value of the load current error in steady-state was analyzed depending of the DC voltage. The considered RMS is given by equation below:

$$RMS_{eisd|sq} = \sqrt{\frac{1}{t_2 - t_1} \int_{t_1}^{t_2} [i_{sdref|sqref}(t) - i_{sd|sq}(t)]^2 dt} \quad (9)$$

The dependence between inverter gain value and calculated RMS (10) value was shown in Fig. 7 and Fig. 8, where can see that dc voltage reduction reduces the average current ripple in both axes. Positive impact of the designed system is visible in different working conditions (i.e. reference current value and frequency).

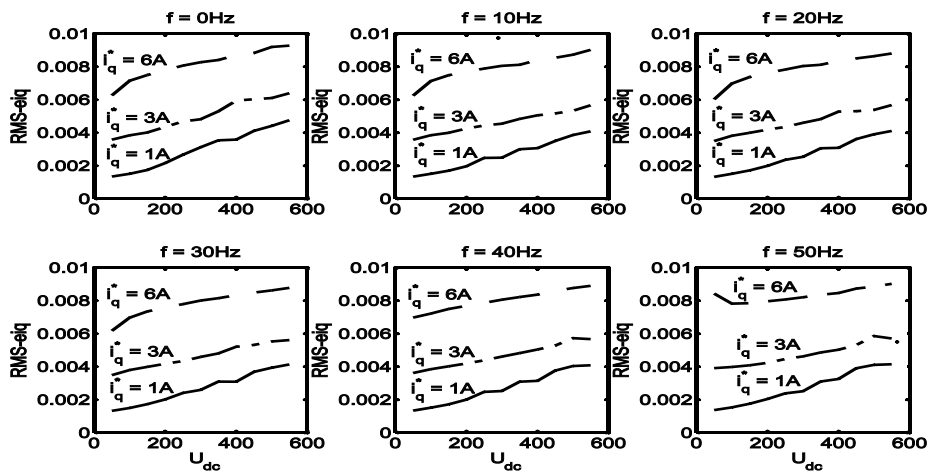


Fig. 7. RMS current error values in q axis

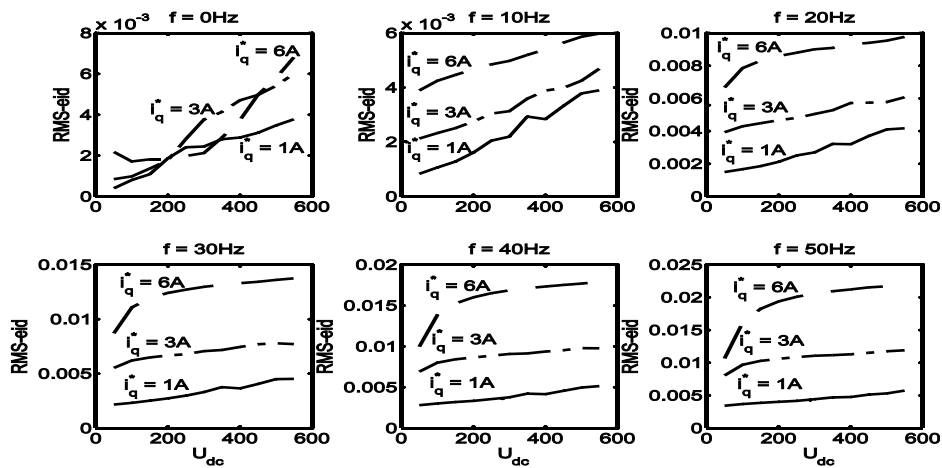


Fig. 8. RMS current error values in d axis

6. CONCLUSION

It was found that the neural network based adaptive state feedback controller can be successfully used to control load current during DC voltage value changes. The artificial neural network approximate the non-linear dependences between controller coefficient and inverter gain. The adaptation algorithm properly controls the load current and the steady-state current error is equal zero. DC bus voltage changes don't affect the system response through proposed adaptation algorithm.

Based on buck converter structure VMC was successfully introduced in order to precise control of the DC voltage value.

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