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# The influence of hydrogen addition for exhaust gas emission in SI gas engine

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One of the major problems in internal combustion engines is emission of pollutants with exhaust gases. Those pollutants are not only harmful for environment but also for humans. To decrease emission of pollutants many mechanical and chemical methods are used in internal combustion engines especially in exhaust system such as TWC, DPF, SCR. Alternative way for decrease in exhaust gas pollutants is use of alternative fuel as a primary energy carrier or as an additional fuel for base hydrocarbon one. In this studies the hydrogen was used as a additional fuel to methane. Both fuels were delivered to intake manifold. The share of the fuel was 100/0 methane/hydrogen and 70/30 methane/hydrogen. The addition of hydrogen to base fuel shown decrease of exhaust pollutants from engine and increase in engine operating parameters.

**Key words:** SI engine, hydrogen, methane, emissions.

## Introduction

One of the problems which is related with human activity is increase in emission of pollutants. Those pollutants are not only harmful for environment but also for humans. After industrial revolution the increase in CO<sub>2</sub> emission from fossil fuels increase almost from 0 to 35 billion of tones [10]. From that reason the governments of different countries as well as EU are very strict with limitation of emission of pollutants. One of the source of those pollutants are means of transport which are equipped with internal combustion engines. There are several methods to decrease emission of pollutants from IC engine. Nowadays for that purpose there are used three way catalytic converters (TWC), selective catalytic reactors (SCR) and diesel particulate filter (DPF). The aim of these methods is to decrease emission of such exhaust gas components as nitroxides (NO<sub>x</sub>), carbon dioxide (CO<sub>2</sub>), carbon monoxide (CO), unburned hydrocarbons (HC). Except these filtering methods for reduction of pollutants from exhaust gases, there are other options. One of another option is to use fuel with less carbon in it. That means that the hydrogen to carbon ratio (H/C) should be greater than for typical hydrocarbon fuel. Such alternative fuel which can be used is hydrogen.

It can be said that hydrogen is the cleanest fuel regarding CO, CO<sub>2</sub> and HC emissions, it should decrease the emissions [6]. The product of hydrogen combustion is only water. Besides those properties hydrogen has other which can bring other advantages to IC engine, among other are minimal ignition energy, laminar flame speed, explosion limits. The comparison of the hydrogen, methane and gasoline properties are presented in table 1.

**Tab. 1.** Fuel properties [1,7]

Physical properties	Hydrogen	Methane	Gasoline
Density (kg/m <sup>3</sup> )	0,081	0,657	720
Stoichiometric constant	34,79	17,17	14,7
Heat of combustion (MJ/kg)	141,7	55,6	46,4
Heat of combustion (MJ/dm <sup>3</sup> )	0,011	0,037	33,4
Heating value (MJ/kg)	119,7	37,71	42
Heating value (MJ/m <sup>3</sup> )	0,01	0,025	30,24
Minimal ignition energy (mJ)	0,02	0,28	0,25
Laminar flame speed (m/s)	1,9	0,38	0,37-0,42
Auto-ignition temperature (K)	858	813	550
Explosion limits (%)	4-75	5-15	1,1-6
Explosion limits (λ)	10-0,14	2-0,6	1,51-0,26

The hydrogen has four times higher laminar flame speed compared to methane or gasoline, because of that the ignition timing for such engine should be tuned. Wider combustion limits allow for combust very lean mixture what has influence on exhaust gas emission. Those properties allow to increase in engine indicated parameters such as efficiency. Kahraman et al. performed tests at spark ignited four cylinder engine fueled with hydrogen. The test results show that hydrogen caused decrease in all pollutant [5]. The same results achieved Changwei and Shuofeng during their research where the fuel which was combusted was a mixture of gasoline and hydrogen with proportion of 0%, 3% and 6% by volume. For stoichiometric mixture the emission of NO<sub>x</sub> was the highest for 6% share of hydrogen what is related with temperature of combustion for the mixture, but for lean mixtures the decrease of all pollutants was observed [2].

Hydrogen has unfortunately several disadvantages which can cause faster damage of the engine in some unfavorable conditions. Such condition is knock combustion [3,9]. Because of low value of minimum ignition energy hydrogen can easily achieved autoignition. But that disadvantage can be controlled with use of several methods. One of the methods is decrease of maximum temperature of combustion. That can be achieved by use of over-expanded cycle what describe Grab-Rogaliński and Szawaja [4] at their work. Another method for decrease the maximum temperature of combustion is use of EGR (Exhaust Gas Recirculation), such research was done by Nande et al. where he pointed the influence of EGR for reduction of knock combustion and NO<sub>x</sub> emission [8].

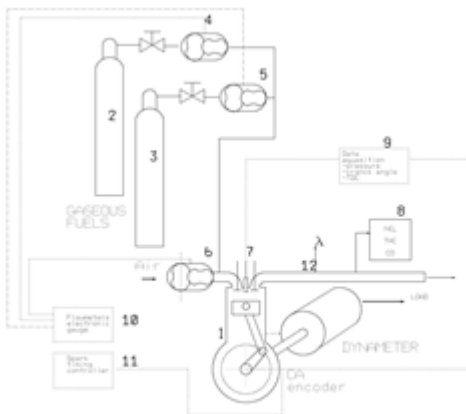
## 1 Test bed description

Test bed used during the research was equipped with single cylinder variable compression ratio spark ignited engine. The change in compression ratio is done by changing the position of cylinder head. The engine was modified to use gaseous fuel. The additional modification was made in ignition system instead of mechanical ignition system the engine use an electronic ignition system. The data of the engine are presented in table 2.

**Tab. 2.** Parameters of the research engine

Cylinder no (-)	1
Compression Ratio (-)	4:1 – 18:1
Bore (mm)	82,55
Stroke (mm)	115
Displacement volume(dm <sup>3</sup> )	0,615
rpm (min <sup>-1</sup> )	600 – 1000
Engine cooling system	Water cooled

The engine is coupled with asynchronous motor which is use as an starter for the combustion engine or as an generator to provide the load for the engine. The asynchronouse motor is controlled by frequency converter. The engine can be fuelled both liquid or gaseous fuels. Gaseous fuel are deliverd to the intake manifold close to the intake valve by gas mixer. Liquid fuel is provided by injector mounted in itake manifold. There is possibility to mix several gases in certaine proportion. The proportion of the gas can be set with use of the gas folwometers. The flow meters are set between gas tank and mixing device. The flow of gas fuel is regulated with use of precise needle valve which is placed before flowmeter. The scheme of test bed is presented in figure 1. The overview of the test bed is presented in figure 2.



**Fig. 1.** Test bed diagram; 1-engine with generator, 2-hydrogen flask, 3-methane flask, 4-hydrogen flowmeter, 5-methane flowmeter, 6-air flowmeter, 7-pressure sensor, 8- bosch gas analyzer, 9-data acquisition system, 10-flowmeters electronic gauge, 11-ignition control unit, 12-wide band oxygen sensor



**Fig. 2.** Test bed overview

The test bed is equipped with measurement system which allows to monitor such parameters as: incylinder pressure, temperature of the engine, temperature of the fresh air or charge and temperature of the exhaust gases. For measure of cranck angle and position of top dead center (TDC) encoder was use which was mounted on camshaft. Flowmeters are equipped with electronic counters which present the actual value of flow for use gases. For measuring of

excess air ratio wide band oxygen sensor was used. Additionally excess air ratio was measured on the exhaust gas analyzer. The pressure sensor and charge amplifier was manufacture by Kistler. Flowmeters CGR-1 were made by Common. Wide band oxygen sensor was made by Bosch. The encoder was made by Hohner. The parameters of the sensors used during the tests are presented in table 3.

**Tab. 3.** The parameters of the sensors

Sensor	Measurement range
Pressure sensor KISTLER 6041B	0-250 bar
Flow meter (Air) Common CGR-01	0,6-65 m <sup>3</sup> /h
Flow meter (CH <sub>4</sub> ) Common CGR-01	0,25-25 m <sup>3</sup> /h
Flow meter (H <sub>2</sub> ) Common CGR-01	0,5-25 m <sup>3</sup> /h
Encoder Hohner PR90-23C1C-C	1-65536
Wide band oxygen sensor BOSCH LSU 4.2	9,56 AFR (0,65 λ)-∞
Bosch BA250 exhaust gas analyzer	CO 0,00-10,00% vol. HC 0-9999 ppm vol. CO <sub>2</sub> 0,00-20,00% vol. NO 0,00-22,00% vul. O <sub>2</sub> 0,00-5000 ppm vol. λ 0,500-9,999

Complete measurement system was connected to data acquisition system made by Measurements Computing The sampling rate of data card was 250kS/s. The card has 8 analog inputs, which allow to recorde signals provided by sensors. In this researche the signals which were connected to data aqisition system were: incylinder pres-sure, cranck angle and position of TDC. From data aqisition system the data were transferred to the PC where special program "SAWIR" calculated such parameters as: IMEP, rev, cumulative heat reales, ROHR, incylinder temperature, maximum incylinder pressure, cranck angle for maximum incylinder pressure, maximum pressure increase and cranck angle for maximum pressure increas, indicated power.

## 2 Test procedures

The tests of the engine were done in two phases. Before the test starts the volume share of gaseous fuels flow was determined. In case of this researche the two type of gaseouse fuels were use. First fuel was pure methane and the second one was methane and hy-droge in a share of around 70% by vol. of methane and 30% by vol. of hydrogen. The calculation of the flows for gas fuels was done on a basis of the measurement of actual use of the air for the engine and declaration of the value of excess air ratio. Such approach for actual ambient pressure and temperature allowed to calculate flows which were close to the assumed values. After this calculations the precise setting of the gas flows were done on a basis of measurement of excess air ratio and flows for the fuels and air where engine was running. The measured value were use to calculate the percentage share by volume for the gases which were actually used. The excess air ration under which the test were done was  $\lambda \approx 1$  (CH<sub>4</sub> and CH<sub>4</sub>/H<sub>2</sub>) and  $\lambda \approx 1,3$ .

The first phase after settings for the fuel flows was to detrmine optimal ignition timing for the fuels with different excess air ratio. The determination was done by changing ignition timing in certaine range different for pure methane and for methane/hydrogen mixture. After determinatin the optimal ignition timing the measurement of exhaust gas emmission were done. The length of the test for each setting was 100 combustion cycle. The engine rpm was 850 rev/min. Operating temperature for the engine was 90°C. The complete test matrix is presented in table 4.

Tab. 4. Test matrix/Rodzaje pomiarów

Fuel	First phase		Second phase	
	CH <sub>4</sub>	CH <sub>4</sub> /H <sub>2</sub>	CH <sub>4</sub>	CH <sub>4</sub> /H <sub>2</sub>
$\lambda$	1	1,3	1	1,3
Ignition timing range (CA)	320-360	320-360	320	320
Number of cycles	100	100	100	100
Exhaust gas emissions	No	No	Yes	Yes

The ignition timing was not differ for different combinations of gasoues fuels and for differen excess air ratio. This may be related with the fakt that the methane was main fuel. The results for determination of optimal ignition timing are presented in figure 3.

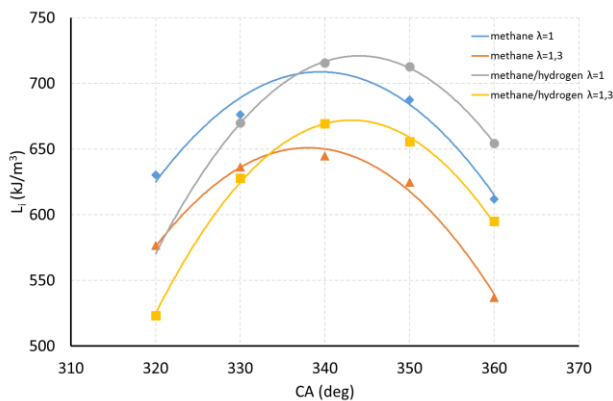


Fig. 3. Optimal ignition timing for tested fuels

As can be seen on the figure 3 the optimal timing for all fuels is around 340 degrees of CA, which means that the ignition advance is 20 degrees of CA bTDC. In case of fuels with hydrogen addition the ignition timing in both case of excess air ratio is closer than without hydrogen by 5 degrees of CA. The smaller value of ignition timing in that case is related with hydrogen laminar flame speed which is around four times higher than for mthane and othe hydro-carbon fuels.

### 3 Results and discussion

#### 3.1 Indicated parameters

The measurements during the test were done for constant ignition timing in all cases. The chosen ignition timing was 340 degrees of CA (20 degrees of CA before TDC). Figure 4 present pressure vs. CA.

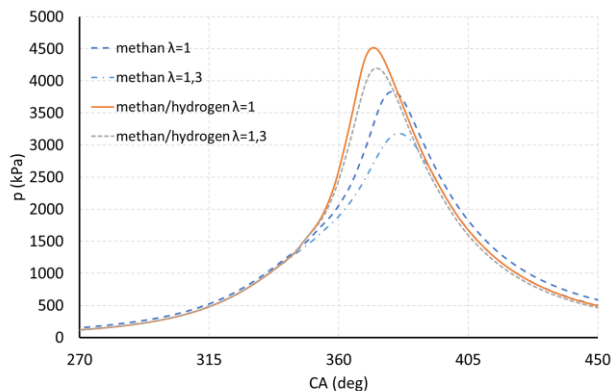


Fig. 4. Pressure vs. CA for tested fuels with different excess air ratio

As can be seen addition of hydrogen to base fuels in both cases of excess air ratio cause increase in pressure. That increas is caused by laminar flame speed for hydrogen. This property allow to reach hihger value of pressure because the combustion last shorter than for hydrocarbon fuels and for first phase of combustion pressure increase is much higher. That can be seen in figure 5, which presents the increase in pressure as a function of CA.

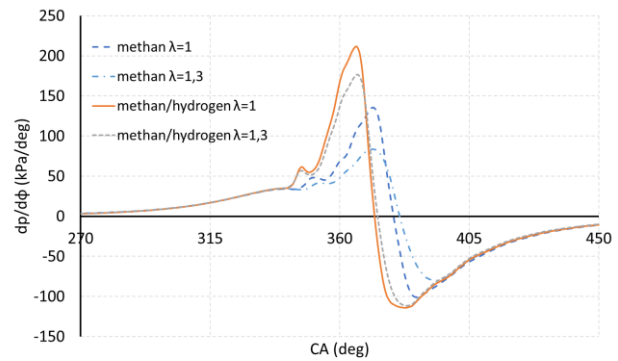


Fig. 5. Pressure increase vs. CA

The figure 5 shows that the trend with shortening the combustion is related with two factors first is excess air ratio in that case for pure methane the combustin duration for lean mixture is longer than for stoichiometric mixture. In mixture with the hydrogen the difference for the end of combustion is small. That can be observed in figure 6.

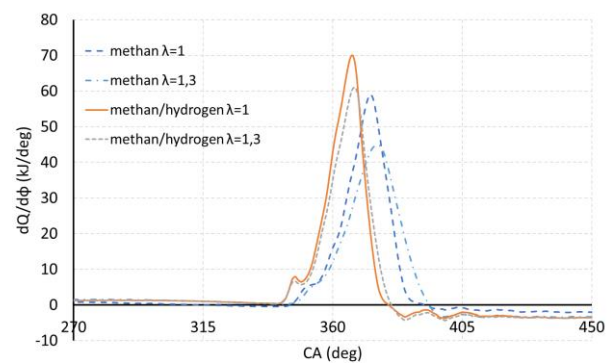
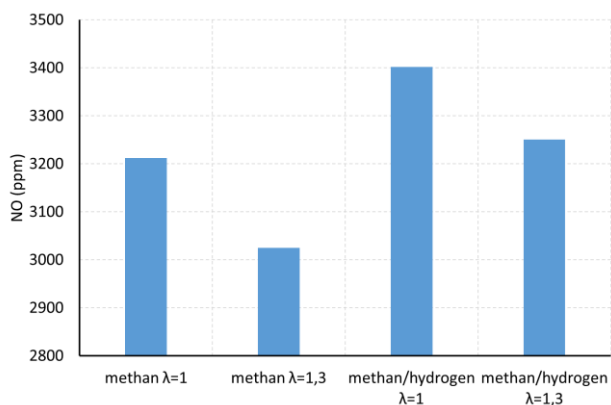


Fig. 6. Heat release rate vs. CA

As can be seen for mixtures which conatins hydrogen the heat release rate are higher than for pure methane. The heat release rate for methane with stoichiometric mixture is almost as high as for methane/hydrogen with lean mixture but the duration of combustion is longer for methane compared to methane/hydrogen mixture at different excess air ratio.

#### Emissions

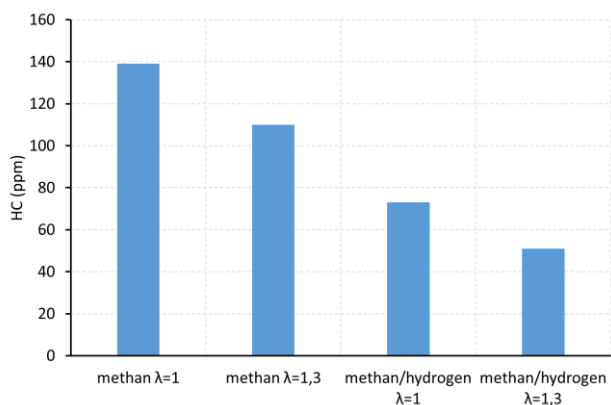
During the test the exhaust gas emission was measured. The measured compounds of exhaust gas were NO, HC, CO<sub>2</sub> and CO<sub>2</sub>. Figure 7 present emission of NO component.



**Fig. 7.** NO emission as a function of excess air ratio (methane and methane/hydrogen)

As can be seen in figure 7 with increase in hydrogen and decrease in excess air ratio the emission of NO is increasing. This behavior is related with excess air ratio and hydrogen addition and caused by higher maximum temperature during combustion.

Figure 8 present emission of HC. In case of HC emission with increase of excess air ratio and addition of hydrogen, the emission is decreasing.

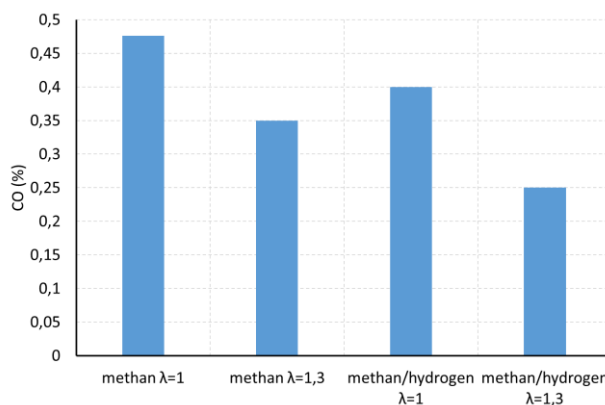


**Fig. 8.** HC emission as a function of excess air ratio (methane and methane/hydrogen)

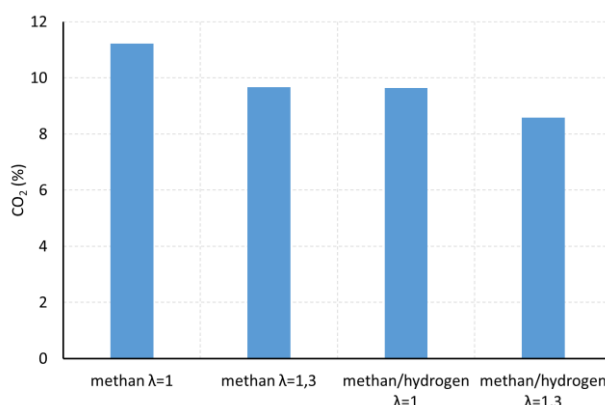
This trend is caused by lowering the amount of carbon in fuel, first by leaner mixture, second by hydrogen addition.

In figure 9 CO emission can be observed. In case of CO emission the most impact for it emission has amount of carbon in fuel and excess air ratio. In case of CO emission with increase in excess air ratio the decrease of this component is observed. Additional decrease of CO is achieved by adding the hydrogen. As a result for excess air ratio of 1,3 with hydrogen the lowest emission of CO was observed.

Figure 10 presents emission of CO<sub>2</sub>. Emission for this component show similar trend as for CO. Both factors as increase in excess air ratio and increase in hydrogen content in fuel mixture cause decrease in emission of CO<sub>2</sub>. That fact is related with decreasing in carbon content in base fuel which was methane by adding 30% of hydrogen and also decrease in amount of methane which fueled engine by increase in excess air ratio.



**Fig. 9.** CO emission as a function of excess air ratio (methane and methane/hydrogen)



**Fig. 9.** CO<sub>2</sub> emission as a function of excess air ratio (methane and methane/hydrogen)

## Conclusions

The obtained results of the research allowed to present some conclusions as follows:

1. Addition of hydrogen to the base fuel require modification of ignition timing, it should be retarded, to obtain optimal engine performance.
2. Addition of hydrogen to the methane cause increase in maximum pressure, what has influence for maximum temperature of combustion.
3. Increase in excess air ratio cause extended combustion for methane but for mixture of methane and hydrogen the combustion phase for both excess air ratio was nearly the same.
4. Methane/hydrogen mixture cause increase in NO emission what is a result of higher temperature of combustion than for pure methane.
5. CO emission in all cases decreased what is caused by increase in excess air ratio and change in H/C ratio.
6. CO<sub>2</sub> emission is decreasing with increase in excess air ratio and H/C ratio.
7. Addition of hydrogen lead to decrease in HC emission.

To summarize the results it can be said that addition of hydrogen to hydrocarbon fuel can be a promising method for limitation an exhaust gas emission from internal combustion engine.

## Acknowledgements

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**Wpływ dodatku wodoru na emisję toksycznych składników spalin w gazowym silniku spalinowym o zapłonie iskrowym**

Jednym z głównych problemów silników spalinowych jest emisja toksycznych składników spalin. Zanieczyszczenia te są nie tylko szkodliwe dla środowiska ale również dla człowieka. Do obniżenia emisji toksycznych składników spalin wykorzystuje się w silnikach spalinowych wiele mechanicznych i chemicznych metod między innymi katalizatory trójdrożne, filtry cząstek stałych oraz katalizatory selekcyjne. Alternatywną metodą obniżenia emisji toksycznych składników spalin jest wykorzystanie paliwa alternatywnego jako nośnika energii lub jako dodatku do paliwa węglowodorowego. Prezentowany artykuł przedstawia wykorzystanie wodoru jako dodatku do paliwa podstawowego jakim był metan. Paliwa podawane były do kolektora dolotowego. Procentowy stosunek objętościowy dla badanych paliw był następujący 100/0 metan/wodór i 70/30 metan/wodór. Prowadzone pomiary wykazały, że dodatek wodoru do paliwa podstawowego wykazał spadek w emisji toksycznych składników spalin oraz wzrost parametrów użytkowych silnika.

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**Słowa kluczowe:** Silnik Zi, wodór, metan, emisje.

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