



COREDIV modelling of JET ILW discharges with different impurity seeding: nitrogen, neon, argon and krypton*

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Abstract. Numerical simulations with the COREDIV code of JET H-mode discharges with 25 MW of auxiliary heating in the ITER-like wall (ILW) configuration with different impurity seedings – nitrogen (N), neon (Ne), argon (Ar) and krypton (Kr) – are presented. All simulations have been performed with the same transport model and input discharge parameters like auxiliary heating, volume average plasma density, confinement factor. Only the seeded impurity puff rate was changed in the calculations. It appears that for the considered heating power of 25 MW and relatively low volume electron average density $\langle n_e \rangle = 6.2 \times 10^{19} \text{ m}^{-3}$, impurity seeding is necessary. It has been found that for every gas at the maximum level of the seeding rate, allowed by the code convergence, the power to the plate is reduced up to 2–4 MW, with electron temperature at the plate of about 2 eV, indicating semi-detached conditions in the divertor region. It should be noted, however, that in cases with low and medium Z impurity (N, Ne and Ar), tungsten radiation is a significant part of radiation losses and stays above 22–32% of the total energy losses, but for high Z impurity (Kr) it is reduced up to 10% of the total losses. The maximum of the Kr radiation is between the pedestal region and separatrix, showing that radiative mantle can be created, which might have a strong influence on the plasma parameters in the pedestal region.

Keywords: impurity seeding • integrated modelling • tokamak

Introduction

The scrape-off layer (SOL) radiation of intrinsic impurities in tokamaks with tungsten (W) as the target plate material is strongly limited. That might lead to high heat fluxes to divertor and corresponding high target plate temperatures, with the consequence of increased W sputtering. However, the reduction of divertor target power loads to an acceptable level is a critical issue for future tokamaks and fusion reactors. The radiative exhaust of energy by externally seeded impurities is considered presently as a promising method of spreading energy over a large wall area and therefore the effect of the impurity seeding on the plasma performance and heat load mitigation have to be understood. This is, in particular, true for JET experiments with the new ITER-like wall (ILW) configuration (ILW: beryllium (Be) wall + W divertor), which shows that the plasma performance is strongly affected by the presence of tungsten [1]. In particular, experiments have been performed to study the so-called radiative scenarios, where the influence of the seeding impurity on the main plasma parameters is studied [2]. It has been found that

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seeded impurities can affect the shape of density and temperature profiles, influence the L-H power threshold, the pedestal position and parameters as well as the pedestal stability with its direct consequence on plasma performance.

In this paper, numerical simulations with the COREDIV code of JET H-mode discharges in ITER-like wall configuration and with different impurity seedings such as nitrogen (N), neon (Ne), argon (Ar) and krypton (Kr) are presented.

Since the energy balance in tokamaks with metallic walls depends strongly on the coupling between bulk and the SOL plasma integrated modelling approach has to be applied. On the one side, the seeded impurities can reduce the power to the SOL/divertor regions, leading to a reduction of the W influx, but from the other side, they can increase the W production due to enhanced sputtering. Therefore, the joint treatment of both regions is necessary, as long as the edge plasma is not separated from the bulk plasma.

The physical model used in the COREDIV is based on a self-consistent coupling of the radial transport in the core to the 2D multi-fluid description of the scrape-off layer. The COREDIV code was successfully benchmarked against a number of JET discharges not only with carbon plates [3], but with tungsten divertor and beryllium wall (JET ILW) for nitrogen [4, 5] and neon [6] seeding, proving its capability of reproducing the main features of JET seeded discharges, as the electron density and temperature profiles, the total radiated power, the effective ion charge (Z_{EFF}) and tungsten concentration as well as profiles of radiation.

Model and results

Simulations are performed for JET discharges with different seeding gases (N, Ne, Ar and Kr) assuming different levels of impurity influx. As a reference scenario, high-power JET shot is chosen (#87194), which is characterized by the following main parameters: plasma current $I_p = 2.6$ MA, toroidal magnetic field $B_T = 2.5$ T, volume averaged $\langle n_e \rangle_{\text{VOL}} = 6.2 \times 10^{19} \text{ m}^{-3}$ and line averaged $\langle n_e \rangle_{\text{LINE}} = 6.7 \times 10^{19} \text{ m}^{-3}$ electron density, separatrix density $n_{es} = 3.0 \times 10^{19} \text{ m}^{-3}$, H-factor (IPB98(y,2) [7]) $H_{98} = 0.8$ and auxiliary heating $P_{\text{aux}} = 25$ MW. We observe that it is possible that changes in confinement due to the level of the different gases and to the different radiation patterns are not accounted for in this simulation.

The comparison between experimental and simulated profiles of electron density and electron and ion temperatures is shown in Figs. 1 and 2, respectively.

In order to reproduce the experimental density profile, relatively strong plasma peaking has been assumed ($C_p = 0.3$), where C_p is the density peaking coefficient [8, 9].

All the simulations are done for the same input parameters, except seeded impurity type and its puffing rate. In case of N seeding, the recycling coefficient of $R_1 = 0.25$ is used whereas for Ne, Ar and Kr the coefficient is $R_1 = 0.925$, taking into account that nitrogen is not recycling impurity. For radial diffusion in the

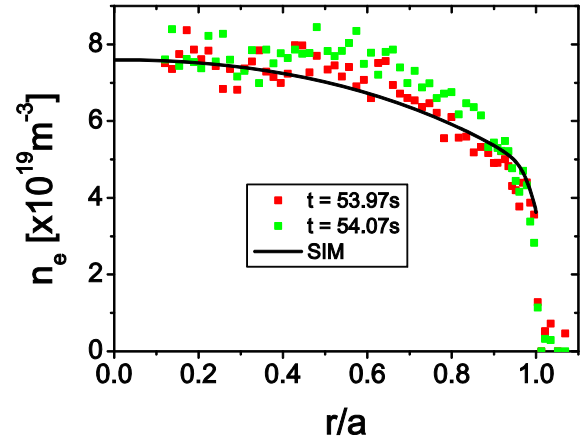


Fig. 1. Density profile by simulation and experiment for shot #87194 at the time $t \sim 54$ s.

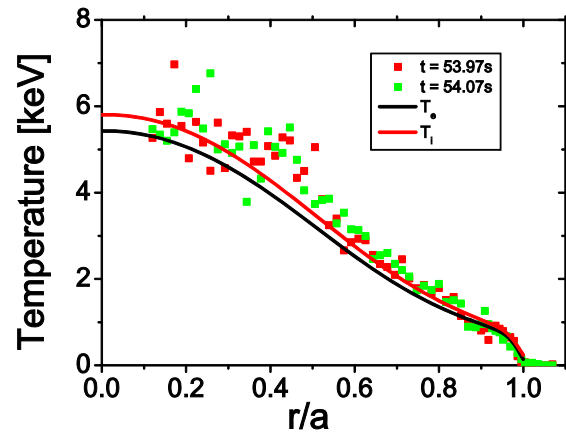


Fig. 2. Ion and electron temperature profile by simulation and experiment for shot #87194 at the time $t \sim 54$ s.

SOL, we use $D_{\perp}^{\text{SOL}} = 0.5 \text{ m}^2/\text{s}$ whereas for the core transport, only anomalous transport is considered, neglecting contributions from the neoclassical transport.

The main plasma parameters versus impurity influx for different gases (N, Ne, Ar and Kr) are presented in Fig. 3. In particular, we show radiation fraction (f_{RAD}), power to the SOL (P^{SOL}) and to the plate (P^{PLATE}), electron temperature at the plate (T_e^{PLATE}), SOL radiation (R^{SOL}) and effective charge (Z_{EFF}). It should be noted that the nitrogen puff level is reduced by a factor of 7 in the figures in order to have better comparison between all impurities. Simulations are performed from a negligible level of the seeding until the maximum value allowed by the numerical code stability and consequently, full detachment is not considered in the simulations.

The threshold power ($P_{\text{H-L}}$), calculated according to the Martin's law [10] is found to be 9.5 MW for the considered JET shot and it can be seen that there is no problem to stay in H-mode for all impurities and seeding levels. However, the power to the plate without impurity seeding (13.5 MW) (see Fig. 3) would be relatively high (exceeding technological heat flux limits $10 \text{ MW}/\text{m}^2$ and we use that divertor plate surface is 1 m^2) and impurity seeding is necessary to reduce the power to the target plates for the simulated discharge.

The achieved total radiation fractions are between 70 and 80%: 71% for N, 80% for Ne, 76.5%

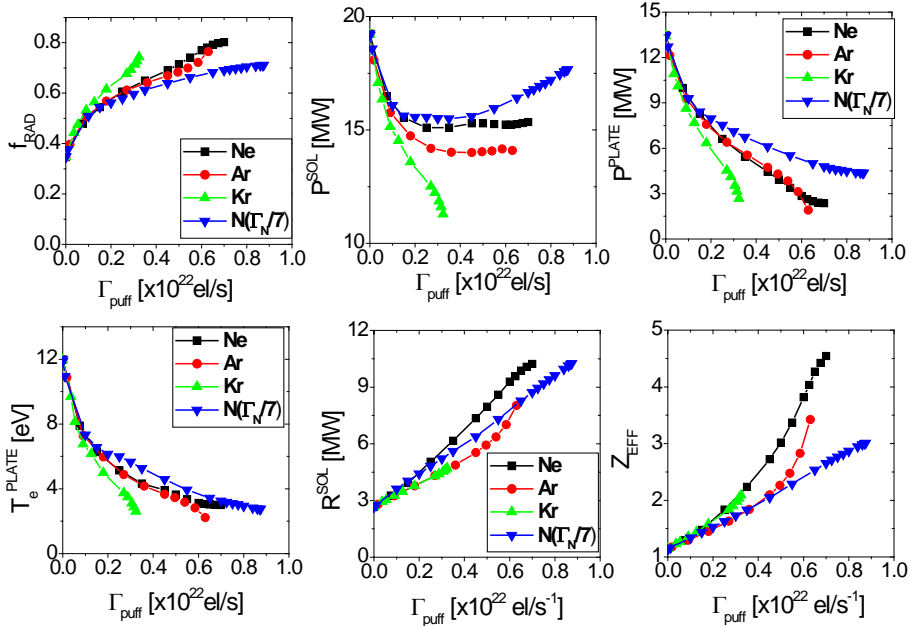


Fig. 3. Main plasma parameters versus impurity influx for different gases (N, Ne, Ar and Kr): radiation fraction (f_{RAD}), power to the SOL (P^{SOL}) and to plate (P^{PLATE}), electron temperature at the plate (T_e^{PLATE}), SOL radiation (R^{SOL}) and effective charge.

for Ar and 74.5% for Kr seeding, respectively. The radiation fraction for low Z impurities (N, Ne) goes to saturation with the increasing of the seeding rate. It has been found that for every gas at the maximum level of the seeding power to the plate is reduced by 2–5 MW and the electron temperature at the plate is about 2–3 eV, indicating semi-detached conditions in the divertor region. In case of Kr seeding, the reduction of the power to the plate is very sensitive to the seeding level. For puffing levels smaller than 0.3×10^{22} el/s, we observe similar values of $Z_{\text{EFF}} \approx 1.8$ –2, but for higher puffing rates, there are significant differences in the Z_{EFF} values. The maximum Z_{EFF} is obtained for the Ne seeding, which is about two times higher in case of Kr seeding.

SOL radiation (R^{SOL}) increases almost linearly with the seeding level, and the largest radiation is achieved for N and the smallest for Kr seeding, depending on the cooling rates of the impurity type. The behaviour of the power to the SOL as a function of the impurity puff rate depends on the impurity type. For Kr, it always decreases with the increase of the seeding level, for Ne and Ar, saturation is achieved, whereas for N seeding, increase of P^{SOL} is seen after initial reduction. Therefore, for nitrogen, large seeding levels are possible in the H-mode.

In Fig. 4, we present total core radiation, W radiation in the core (R_W^{CORE}), radiation by seeding impurity ($R_{\text{IMP}}^{\text{CORE}}$), average ion temperature ($\langle T_i \rangle$), tungsten concentration (C_W) and seeded impurity

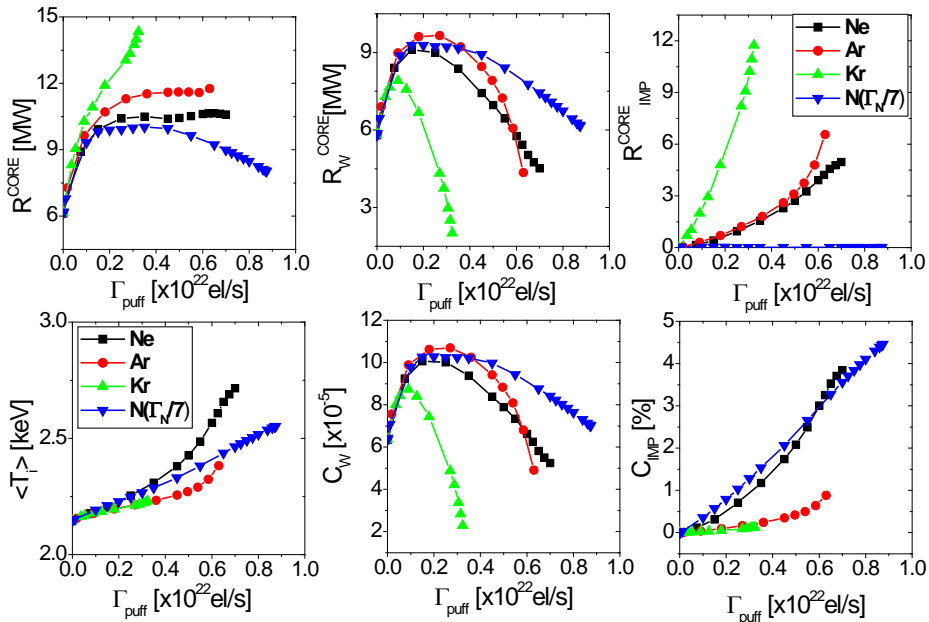


Fig. 4. Main plasma parameters for different impurity puff: N, Ne, Ar and Kr level: total (R^{CORE}), W (R_W^{CORE}) and by seeding impurity ($R_{\text{IMP}}^{\text{CORE}}$) radiation in the core, average ion temperature ($\langle T_i \rangle$), W (C_W) and impurity (C_{IMP}) concentration.

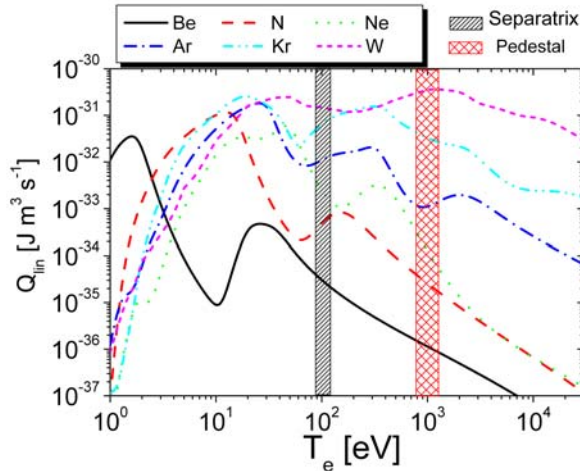


Fig. 5. Cooling rate for Be, N, Ne, Ar, Kr, W in coronal equilibrium.

concentration (C_{IMP}) versus impurity puffing level. The maximum seeded impurity radiation in the core is observed for Kr seeding, with the smallest for nitrogen, which is consistent with our expectations coming from coronal equilibrium (see Fig. 5). For typical core temperatures ($T_e \gg 150$ eV), the radiation efficiency of Kr is about 1000 higher than for N.

Only for Kr seeding, the W radiation in the core might be fully replaced by Kr radiation whereas for other impurities the W radiation in the core remains a significant part of the total radiation losses. For low and medium Z impurities (N, Ne and Ar), tungsten radiation is a significant part of radiation losses and stays above 22–32% of the total energy losses, but for high Z impurity (Kr), it is reduced down to 10% of the total losses. Correspondingly, W concentration for N, Ne, Ar goes down to $5\text{--}6 \times 10^{-5}$ level whereas only for Kr, it is reduced to

2×10^{-5} . For all impurities, similar temperatures at the plate of about 2–3 eV are achieved, as can be seen in Fig. 3, which corresponds to similar sputtering yield values. However, the total tungsten influx due to sputtering processes is higher for low Z impurities, which is the effect of higher impurity flux to the target plates. At maximum seeding rate, the impurity concentrations range from 4% for Ne and N to 0.1% for Kr. It can be seen from Fig. 4 that with the increase of the impurity puff level, the average ion temperature increases due to the effect of plasma dilution by impurity ions.

The radiation profiles in the core for different impurities at the maximum impurity seeding level are shown in Fig. 6. As can be seen, radiation in the core by seeded impurities increases with the impurity atomic number, and simultaneously tungsten radiation is reduced. Only for nitrogen, the extrinsic impurity radiation is located close to the separatrix, whereas for other impurities, strong radiation in the pedestal region is observed, which might affect the confinement properties. In addition, for Ar and Kr, significant part of the radiation is localized in the core. The maximum of the radiation for N, Ne and Ar is at the separatrix, but for Kr, the maximum is between separatrix and pedestal. In the case of Ar and Kr seeding, the formation of the radiating belt might be possible.

Conclusion

The COREDIV code has been used to simulate JET discharges in the new ITER-like wall configuration. The focus has been put on auxiliary heated 25 MW H-mode discharge with different impurity seeding: N, Ne, Ar and Kr. For the considered auxiliary heat-

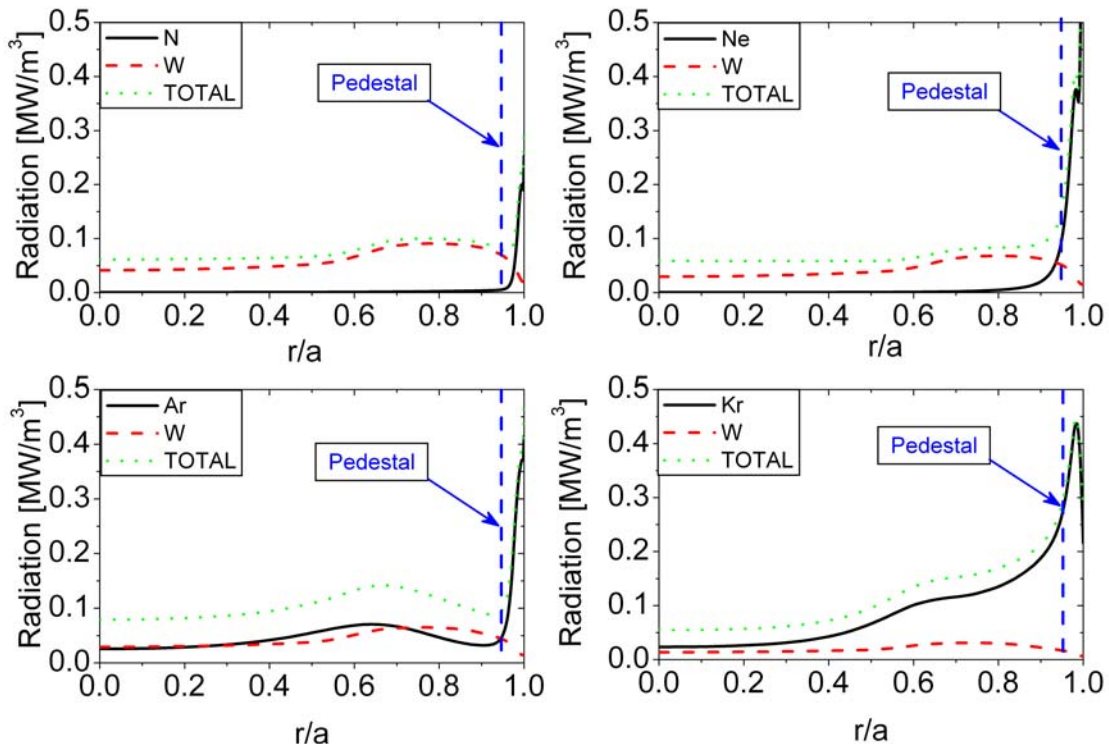


Fig. 6. Radiation profiles: total, W and seeded impurity in the core. The dotted line shows the pedestal position.

ing and density levels, impurity seeding to reduce the power to the target is required. Sensitivity studies have been done to give insight on the influence of different impurities on main plasma parameters:

- Z_{EFF} is defined by low-Z impurity level, smaller dilution for the case with Kr, $Z_{\text{EFF}} \sim 2.2$.
- Only for nitrogen, radiation is localized close to the separatrix.
- Maximum radiation fraction is observed for Ne (80%).
- W radiation decreases with increasing the impurity atomic number.
- For Ar and Kr, significant part of the radiation is localized in the core.
- Only for Kr, $C_w \sim 2 \times 10^{-5}$, the W production practically stops.
- Possible pedestal degradation is observed for Ne, Ar and Kr seeding.
- Possible formation of radiation belt for Ar and Kr seeding can be seen.

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