

Response surface methodology approach for optimization of biosorption process for removal of Hg(II) ions by immobilized Algal biomass *Coelastrella* sp.

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Currently, adsorption stands as a viable technique for the effective removal of pollutants such as heavy metals from water. Within this research endeavor, adapted green algae (*Coelastrella* sp.) have been harnessed as a sustainable and environmentally conscious adsorbent, employed in the removal of Hg(II) ions from a simulated aqueous solution via employment of an Airlift bioreactor. The analysis of the attributes of adsorbent was conducted through the utilization of Fourier transform infrared (FTIR) spectroscopy. The examination of residual concentrations of Hg(II) ions in the treated solution was accomplished through the utilization of atomic absorption spectroscopy (AAS). The impact of various experimental factors, including the duration of contact (ranging from 10 to 90 minutes), initial concentrations of Hg(II) ions (ranging from 500 to 2000 $\mu\text{g/l}$), quantity of adsorbent introduced (ranging from 0.1 to 0.7 g per 250 ml), temperature variations (ranging from 20 to 40 $^{\circ}\text{C}$), and airflow velocity (ranging from 200 to 300 ml/min), was systematically examined. For the optimization of adsorption efficiency, MINITAB 18 software was employed. The equilibrium data was subjected to analysis using the Langmuir, Freundlich, and Temkin isotherm models. Employing the framework recommended by MINITAB 18, the optimal parameters for adsorption were identified as 2000 $\mu\text{g/l}$ for initial concentration, 90 minutes for contact time, 40 $^{\circ}\text{C}$ for temperature, and 300 ml/min for airflow rate. The Langmuir equation yielded the highest adsorption capacity, measuring 750 $\mu\text{g/g}$ at a temperature of 40 $^{\circ}\text{C}$.

Keywords: Adsorption; green algae; equilibrium; airlift bioreactor; kinetics.

INTRODUCTION

The removal of hazardous heavy metals from wastewater has grown to be a significant global issue. Effluents resulting from many industries, including pulp and wood industries, paper board mills, metal cleaning and plating, and municipal wastewater, are the primary causes of heavy metal contamination¹⁻⁵. Mercury, Hg (II), and its derivatives are cumulative poisons detrimental to human health, even at a very low concentration⁶⁻⁸. The discharge of effluents containing mercury into the ecosystem has the potential to pose threats to aquatic organisms and exert significant ramifications on the ecological food web. The pronounced toxicity associated with this element, its propensity to accumulate within soil and sediment matrices, and a series of notable ecological events, particularly exemplified by the Minamata Bay incident in Japan between 1953 and 1956, collectively catalyzed the advancement of methodologies aimed at the mitigation of mercury-laden effluents⁹. Currently, coal-fired power stations represent the most substantial contributor to atmospheric emissions. Nevertheless, the widespread utilization of mercury in dental amalgam implies that crematoria could potentially surpass them as the most significant source in the future. Additionally, hospitals equipped with medical waste incinerators play a significant role in contributing to the mercury issue. Although the number of medical waste incinerators is decreasing, resulting in reduced emissions, concerns persist within the healthcare community regarding the exposure of patients and other vulnerable groups to mercury through

the use of healthcare products. Furthermore, the chlor-alkali industry, being the largest consumer of mercury in Europe, has discharged numerous tons of mercury into the aquatic environment over the years, thereby contributing to fish contamination¹⁰. Mercury contamination may occur from a variety of sources, including effluents from chlorine manufacture, switchgear/batteries, fluorescent lights, dental wastes, paints, fertilizers, and medicines. Several of conventional technologies such as chemical precipitation, traditional coagulation, activated carbon adsorption, lime softening, ion exchange, and reverse osmosis have been used to remove mercury from contaminated water¹¹. Because of the high cost of commercial activated carbon, there has been a quest for acceptable low-cost adsorbents. Due to its low cost, great effectiveness, minimal secondary waste, and environmental friendliness, biosorption has been widely used method in treating polluted water to reduce hazardous contaminants like mercury present in industrial effluents. *Coelastrella* is a genus of green algae in the family Scenedesmeaceae. *Coelastrella* species may be found in a variety of terrestrial settings, including soil, tree bark, rock surfaces, concrete floors, and brick walls. Tolerance to a very broad temperature range allows for an overall distribution that spans the tropical and polar zones¹². Green algae has been used as a renewable adsorbent to minimize chemical consumption in the waste treatment process, lowering the cost of the treatment plant indirectly¹³. The primary objective of the present study is to examine the effectiveness of eliminating mercury (II)

ions from a water-based solution utilizing green algae (*Coelastrella* sp.) within an Airlift Bioreactor setup. To optimize the impact of diverse variables, a full factorial design was employed. Adsorption isotherm models such as (Langmuir Isotherm, Freundlich Isotherm, and Temkin Isotherm), Thermodynamic study, Kinetic studies such as (Pseudo first-order, Pseudo second-order), and Mass transfer adsorption models such as (Weber and Morris model, Liquid film diffusion model, and Bangham and Burt model) are employed to assess the performance of the adsorbents and optimize their efficiency.

MATERIALS AND METHODS

Stock solution preparation

Mercury chloride $HgCl_2$ was obtained commercially from (Merk), (CAS #: 7487-94-7), (EC Number: 231-299-8). It has the molecular formula $HgCl_2$. The stock solution with a concentration of 1000 mg/l was meticulously formulated by completely dissolving the precisely measured amount of $HgCl_2$ (1.3520 g) in distilled water. Subsequently, various solutions of distinct concentrations were derived from this original solution through dilution, resulting in the desired concentrations (2000 $\mu g/l$, 1000 $\mu g/l$, 750 $\mu g/l$, and 500 $\mu g/l$).

Preparation of the biomass

For approximately a century, the genus *Coelastrella* has been acknowledged and encompasses a limited array of species. *Coelastrella* species exhibit a coccoid morphology, ranging from elliptical to citriform. These microorganisms can be observed as individual unicellular microalgae or as small clusters of cells. A distinctive feature of these species lies in their intricately textured cell walls, characterized by 16–40 meridional ribs and polar thickenings. The cellular envelope comprises two layers, featuring an internal cellulose constituent and an exterior trilaminar component housing an acetolysis-resistant material¹⁴.

First and foremost, the initial step involves the preparation of the algae culture medium by utilizing NPK 20:20:20 (Table 1) as the nutrient medium. As per the research conducted by¹⁵, a concentration of 1g/L of NPK medium was employed to facilitate the growth of green algae. The assessment of the costs associated with cultivating the media was carried out by exclusively considering the concentration and price of each reagent employed in the production of 1 L of the medium. Subsequently, the medium underwent a process of sterilization through indirect heating until it reached a temperature range of 45–50 °C. Once the medium had sufficiently cooled to room temperature, the algae were introduced. The particular strain of algae was acquired from the department of biology at the College of Science, University of Baghdad. To be precise, a volume of 50 ml of algae, with a concentration of 14–16 x 10⁶ cell/ml, was incorporated into five liters of water containing the nutrient medium. The photobioreactor employed in this study was a plastic bottle with a capacity of five liters. All the necessary requirements for the growth of algae were adequately provided. Notably, one of the crucial needs of algae is light, hence, three LED lights were affixed

to each bottle. These LED lights, with a brightness of 1 k lux, were supplemented with 13-watt fluorescent bulbs to ensure the completion of the photosynthesis process. In addition to light, carbon dioxide is another essential requirement for the growth of algae. As such, carbon dioxide gas from the ambient air was effectively introduced into the bioreactor at a steady flow rate of 200 ml/min. Following a period of approximately three weeks, the algae had successfully proliferated and were subsequently harvested. The resulting biomass concentration ranged from 0.4 to 0.7 g/L.

After the cultivation process, the Algae can be converted biomass than grinding it. Extracting algae from its culture area is referred to as harvesting. The principle of separate solid-liquid processes underpins algae processing. One of the most important steps of harvesting is thickening the algae solution until it forms a thick algal slurry or cake. After that drying process take place. Finally, it was milled and sieved through a 200 mesh sieve before being employed as an adsorbent.

Table 1. Presents the composition of N:P:K

| Element | Value (%) |
|-----------------------|-----------|
| N as CH_4N_2O | 2% |
| N as NH_3 | 18% |
| P as phosphorus oxide | 20% |
| K as potassium oxide | 20% |
| Mg+Zn+Mn+Fe+Cu | >1% |

Design of experiments

Response Surface Methodology was used to optimize the four independent variables like Time (A), Temperature (B), Concentration (C) and AFR (D) for the adsorption of Hg (II) on biomass. MINITAB 18 (Full factorial design) recommended experimental design for four variables with experimental and expected response in 120 runs. Where five levels of time (10, 30, 50, 70 and 90 min), temperature levels (20, 30 and 40 °C), Concentration levels (500, 750, 1000 and 2000 $\mu g/l$), and AFR levels (200 and 300 ml/min).

Airlift reactor

The adsorption of methylene blue onto algae was in transparent perspex split-cylinder airlift reactor. The reactor was made up of a vertical cylindrical column with a diameter of 7 cm and a length of 40 cm, with baffle 35-cm length as shown in Figure (1). The temperature of the airlift reactor was measured using a temperature sensor situated at the reactor's top and kept at (20–40 °C) using a heater. The air is directed through the first side in order to transform into the riser, which was accomplished by utilizing a 25W, 2 bar pressure air compressor. The distribution of the air was achieved through the utilization of a small air-permeable stone. The reactor is securely sealed in order to prevent any external air from infiltrating the internal space, and this was accomplished by implementing a one-way valve. Figure (1) illustrates a schematic diagram depicting the operational configuration of the experimental airlift reactor. The reactor work in semi-batch mode.

Adsorption experiments

Adsorption experiments were carried out in an airlift bioreactor under various operating conditions such as

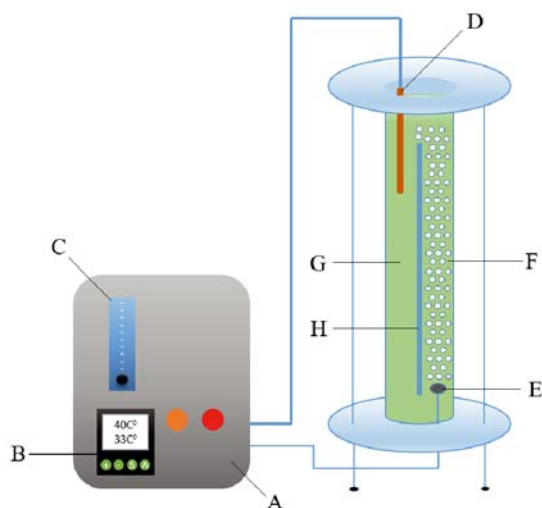


Figure 1. Schematic diagram of Airlift reactor (A – Compressor, B – Temperature controller, C – Rotameter, D – Heater, E – Sparger, F – Riser, G – Downcomer, H – split)

contact time (10–90 min), temperature (20–40 °C), air flow rate (200–300 ml/min), concentration (500–2000 µg/l), and adsorbent dose (0.1–0.7 g/250 ml). In order to optimize the adsorption conditions in the ensuing isotherm and kinetic experiments. Obtained data from the impacts of operating conditions were then used for isotherm, kinetic, and thermodynamic analyses, respectively. The remaining concentration of Hg (II) was assessed employing the atomic absorption spectrophotometer (AAS) Perkin Elmer 1100 model. The equilibrium's adsorption capacity (q_e , µg/g) and efficiency (R, %) were computed using Equation (1) and (2), respectively^{16, 17}.

$$q_e = (C_i - C_e) \frac{V}{W} \quad (1)$$

$$\text{Removal \%} = \frac{C_i - C_e}{C_i} \times 100 \quad (2)$$

where: C_i and C_e (µg/l) are the initial and final Hg (II) concentration, respectively. V is the volume of the solution (L), M is the amount of adsorbent (g).

RESULTS AND DISCUSSION

Characterization of the synthesized adsorbent

Fourier-transform Infrared Spectroscopy (FTIR) stands as a widely acknowledged method for characterizing both inherent and newly-formed functional groups resulting from chemical processes. In this investigation, an Shimadzu model 1800 instrument was employed, operating within a frequency range spanning from 400 to 4000 cm^{-1} , to acquire the IR spectra of the adsorbent before and after the adsorption procedure. The enumeration of all functional groups present on the surface of the algae biomass is detailed in Table 2. Figures 2 and 3 show the examination before and after the adsorption process.

Scanning electron microscopy (SEM)

Scanning electron microscopy (SEM) serves as an initial and essential instrument for assessing the surface morphology and fundamental physical attributes of adsorbents. The examination of sample surface morphology before and after the adsorption process was conducted through SEM analysis. SEM is particularly adept at evaluating the adsorption capacity of compounds, as the surface structure and porosity predominantly govern the

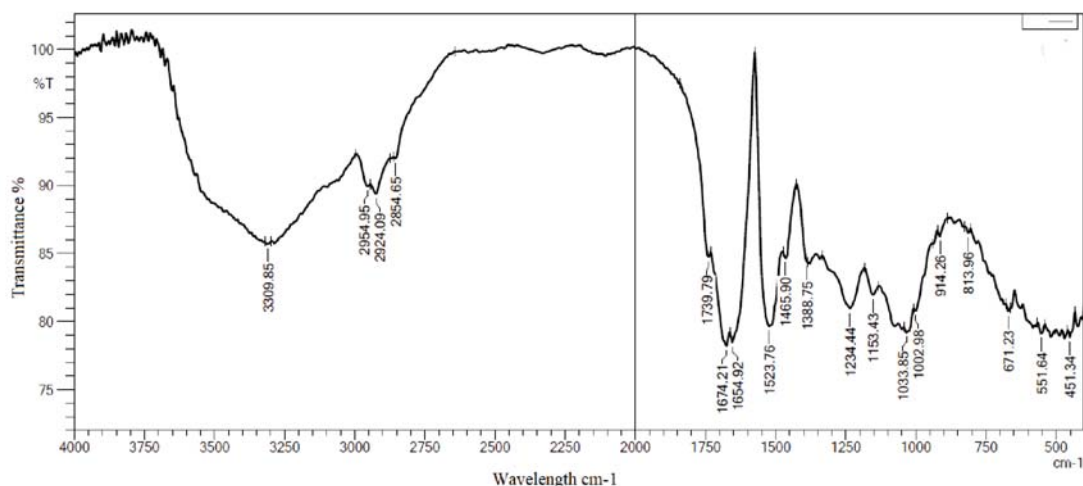


Figure 2. FTIR spectrum for algae before adsorption of mercury

Table 2. IR spectra of the adsorbent before and after adsorption process

| Wave number Before | Wave number After | Wave number Range | Vibration | Functional group present |
|--------------------|-------------------|-------------------|----------------|-----------------------------------|
| 3292.88 | 3274.84 | 3300–2500 | O-H stretching | Alcohol, phenols, Carboxylic acid |
| 2925.85 | 2924.84 | | | |
| 1638.35 | 1633.80 | 1650–1600 | C=C stretching | Conjugated alkene |
| 1535.43 | 1538.09 | 1550–1500 | N-O stretching | Nitro compound |
| 1451.52 | 1453.96 | 1450 | C-H bending | Alkane |
| 1387.26 | 1395.52 | 1420–1330 | O-H bending | Alcohol |
| 1232.28 | 1236.98 | 1275–1200 | C-O stretching | Alkyl aryl ether |
| – | 1151.46 | 1250–1020 | C-N stretching | Amine |
| – | 1076.73 | 1085–1050 | C-O stretching | Primary alcohol |
| 1039.20 | 1028.80 | 1250–1020 | C-N stretching | Amine |

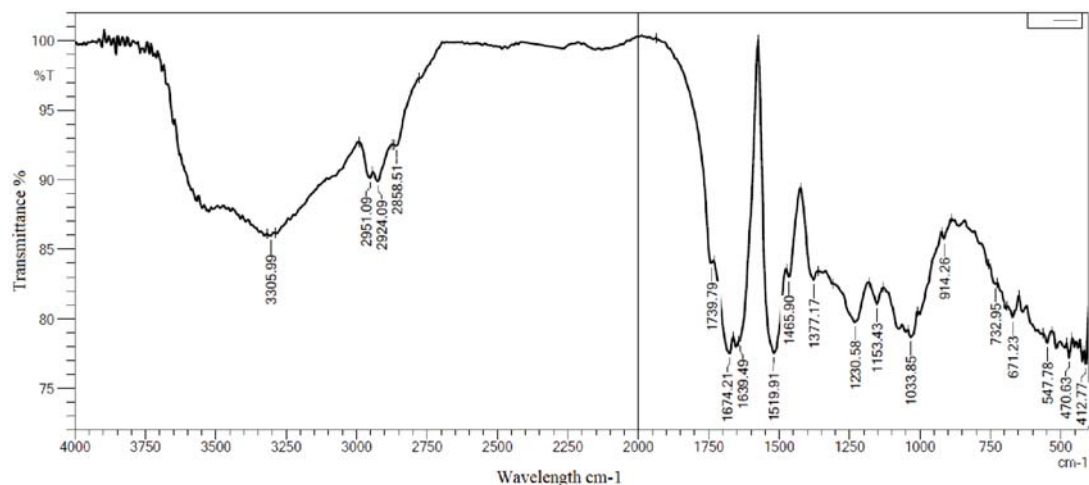


Figure 3. FTIR spectrum for algae after adsorption of mercury

adsorption capacity^{18, 19}. Figure 4 depicts SEM images of algae before and after the adsorption process. In Figure 4-a, it is evident that the structural integrity of the algae cells persists post-drying. In contrast, Figure 4-b illustrates a distinct transformation wherein the cells have disintegrated, leading to a notable deviation from the original state. The previously porous surface has transitioned to a flakier morphology exhibiting residual porosity. Consequently, the SEM imagery provides supplementary substantiation regarding the adsorption of metal ions.

Energy Dispersive Spectroscopy (EDS)

Energy Dispersive Spectroscopy (EDS) were done using thermos fisher Scanning electron microscope. Figure 5 depicts the elemental surface composition of algae obtained. The presence of C and O atoms with some impurity was confirmed by the Figure 5-a. The presence of some impurities due to the algae medium. The pattern reveals that the algal sample's composition is C – 54.3%, O – 45.3%, with the remainder being contaminants. The EDS spectra of Hg doped algae is shown in figure 5-b. According to the EDS spectrum, the synthesized Hg doped algae biomass mostly contains C, O, and Hg elements, with a composition of C – 56.2%, O – 37.8%, and Hg – 2.8%.

Statistical analysis

Response surface methodology amalgamates statistical and mathematical approaches, finding extensive utilization in optimizing variables across various applications²⁰.

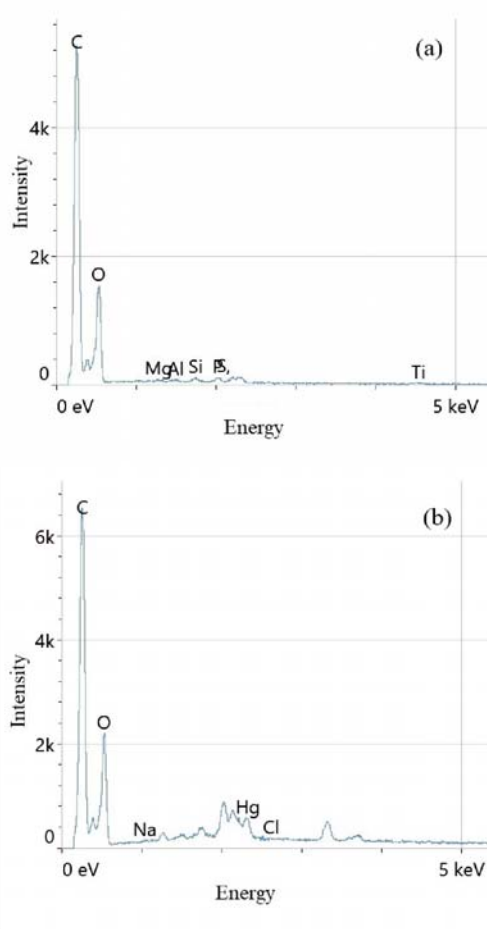


Figure 5. Energy dispersive spectroscopy before adsorption (a), and after adsorption (b) of mercury by algae

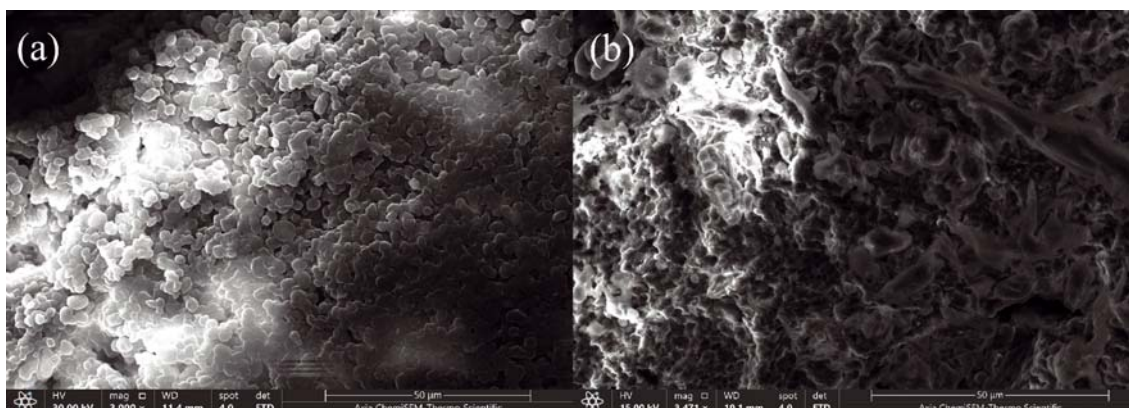


Figure 4. SEM images of algae before (a), and after (b) adsorption process of mercury

Utilizing MINITAB 18, a comprehensive investigation comprising 120 tests was recommended to scrutinize the interplay of four variables: time (A), temperature (B), concentration (C), and AFR (D). Based on the collected experimental data, establishing a relationship between the response and the encoded values of the four variables. This process yielded an empirical equation, as detailed below:

$$\begin{aligned} \text{Removal \%} = & 65.7 + 0.3937 A + 0.531 B - 0.02085 C + \\ & + 0.0213 D - 0.00900 AB + 0.000110 AC - 0.000042 AD + \\ & + 0.000343 BC - 0.000150 BD - 0.000003 CD \end{aligned} \quad (3)$$

In Equation 3, the positive sign implies a synergistic impact, whereas the negative sign indicates an antagonistic effect behavior²¹. A higher F value and a lower P value indicated the significance of each coefficient²².

Analysis of variance

The statistical significance and appropriateness of the regression model constructed through full factorial design were assessed using Analysis of Variance (ANOVA), the results of which are presented in Table 3. Fisher's F values and P values were employed in conjunction with the null hypothesis test to determine the significance of both the regression model and each individual coefficient term²³. Generally, higher F values coupled with lower P values indicate enhanced significance of the regression model and associated coefficients²⁴. As indicated in Table 3, the full factorial design model exhibits pronounced significance, evident from a substantial F value of 47.44 and an impressively low P value of 0.00. Similarly, other specific coefficients such as linear and 2-Way Interactions also demonstrate remarkable significance, with F values of 111.04 and 10.64, respectively, and P values lower than 0.01. Subsequently, components lacking statistical significance ($p > 0.05$) are eliminated from the quadratic equation. This process results in the formulation of an adjusted factorial design model, achieved through consideration of the T and P values presented in Table 3.

$$\begin{aligned} \text{Removal\%} = & 65.7 + 0.3937 A + 0.531 B - \\ & - 0.02085 C - 0.00900 AB + 0.000110 AC + 0.000343 BC \end{aligned} \quad (4)$$

The model's adequacy was determined by the correlation coefficients R^2 and R^2_{adj} . The values of R^2 and R^2_{adj} were determined to be 0.90 and 0.88, respectively, based on the ANNOVA findings.

Table 3. Present the Variance Analysis

| Source | DF | Adj SS | Adj MS | F-Value | P-Value |
|--------------------------|-----|---------|---------|---------|---------|
| Model | 10 | 8922.7 | 892.27 | 47.44 | 0.000 |
| Linear | 4 | 8353.7 | 2088.43 | 111.04 | 0.000 |
| Time (min) | 1 | 5439.2 | 5439.16 | 289.19 | 0.000 |
| Temp. (C) | 1 | 1606.2 | 1606.20 | 85.40 | 0.000 |
| Cons. (ppb) | 1 | 1272.4 | 1272.45 | 67.65 | 0.000 |
| AFR (ml/min) | 1 | 35.9 | 35.91 | 1.91 | 0.170 |
| 2-Way Interactions | 6 | 1200.2 | 200.04 | 10.64 | 0.000 |
| Time (min)*Temp. (C) | 1 | 518.4 | 518.40 | 27.56 | 0.000 |
| Time (min)*Cons. (ppb) | 1 | 375.8 | 375.79 | 19.98 | 0.000 |
| Time (min)*AFR (ml/min) | 1 | 0.4 | 0.42 | 0.02 | 0.882 |
| Temp. (C)*Cons. (ppb) | 1 | 304.5 | 304.53 | 16.19 | 0.000 |
| Temp. (C)*AFR (ml/min) | 1 | 0.4 | 0.45 | 0.02 | 0.877 |
| Cons. (ppb)*AFR (ml/min) | 1 | 0.6 | 0.64 | 0.03 | 0.854 |
| Error | 109 | 1096.2 | 18.81 | | |
| Total | 119 | 10972.8 | | | |

Three dimensional response surface plot and contour plots

Three-dimensional surface plots serve as visual depictions of regression equations, illustrating the simultaneous effect of two variables on a response while maintaining the constancy of the remaining variable²⁵. Alternatively, two-dimensional contour plots can be employed to explore the influence of any two factors through two-dimensional graphical representations. In Figures 6, 7, and 8, both 3D surface plots and their corresponding 2D contour plots are displayed, elucidating the interactive influence of individual variables on the percentage removal of Hg (II).

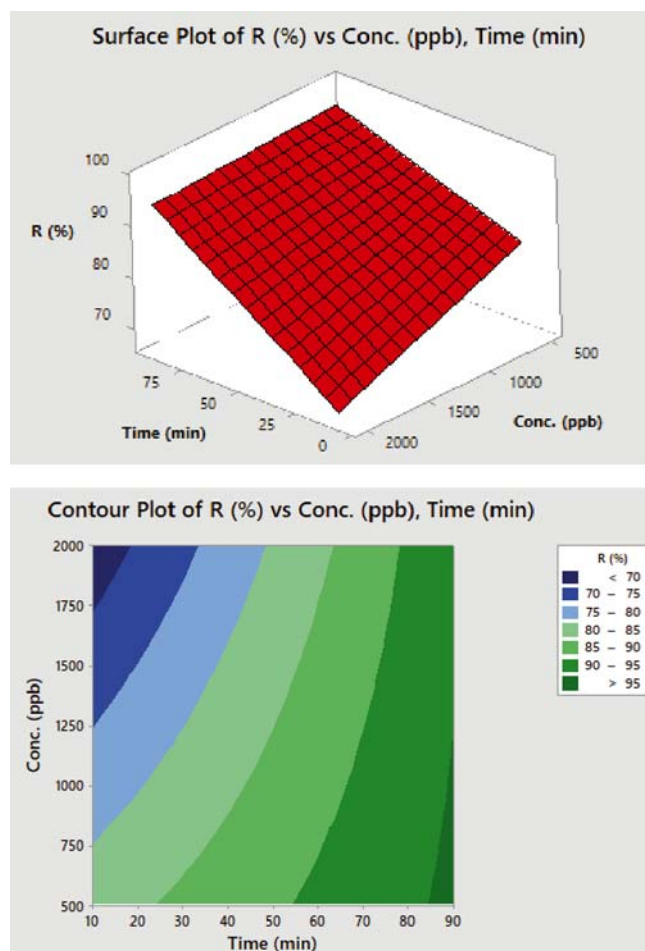


Figure 6. 3D surface plot for interactive effect of time and concentration on Removal of Hg(II) (a), 2D contour plot for interactive effect of time and concentration on Removal of Hg(II) (b)

In Figure 6, both panel (a) and (b) present the 3D surface plot and the corresponding contour plot, respectively, illustrating the interdependent effect of time and concentration on the eradication of Hg(II). It is evident from the visualization that an increase in concentration from 500 ppb to 2000 ppb leads to a decline in the percentage of Hg(II) ion removal over time. This decline can be attributed to the saturation of adsorbent sites with Hg(II) ions at a constrained concentration²⁶. Meanwhile, in Figures 7 (a & b), a discernible enhancement in the percentage removal of Hg(II) ions is showcased in tandem with an escalation in temperature, ranging from 20 to 40 °C, and a lengthening of time, spanning 10 to 90 minutes. Notably, the advancement in the percentage of Hg(II) ion removal remains modest, progressing from 91% to 97%. This trend can be elucidated by the heightened mobility of dye molecules as the temperature rises, indicating the involvement of a kinetic regulatory mechanism—a phenomenon consistently observed across various systems²⁷. Figures 8 (a) and (b) depict the 3D surface plot and its corresponding contour plot, illustrating the interplay between AFR and time regarding the reduction percentage of Hg(II) ions, while keeping the concentration constant at 750 ppb and the temperature at 30 °C. As can be observed, increasing AFR from 200 ml/min to 300 ml/min with time enhances the removal % for Hg(II) ions just marginally. This means that the effect of air flow is not directly affecting on adsorptions process.

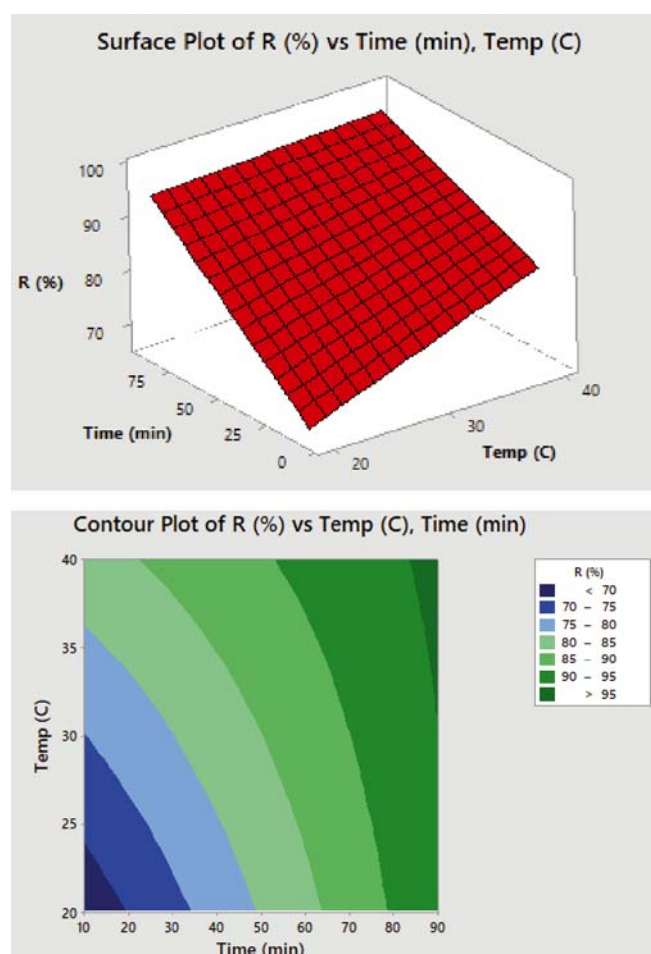


Figure 7. 3D surface plot for interactive effect of time and temperature on Removal of Hg(II) (a), 2D contour plot for interactive effect of time and temperature on Removal of Hg(II) (b)

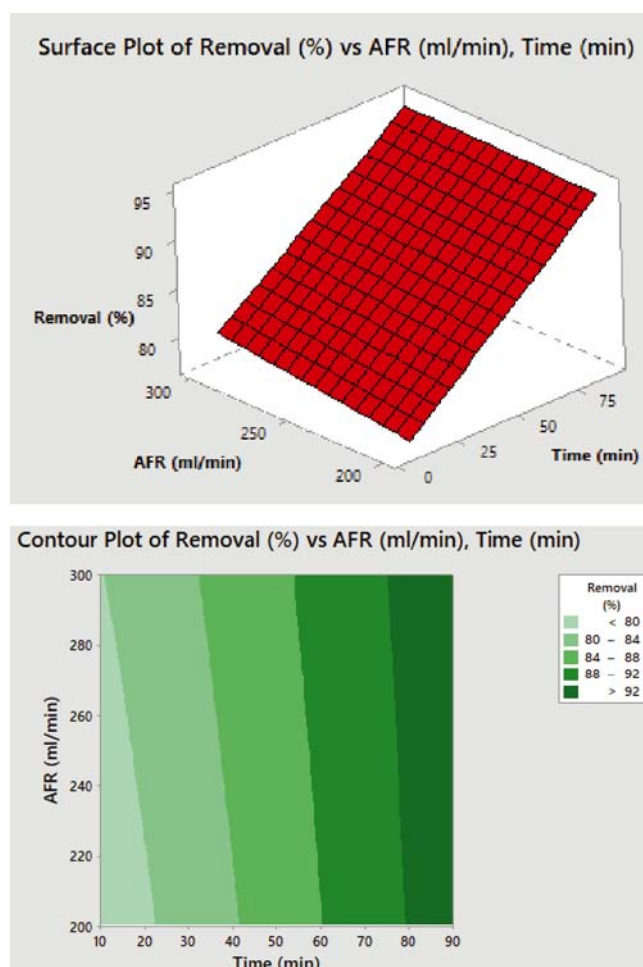


Figure 8. 3D surface plot for interactive effect of time and concentration on Removal of Hg(II) (a), 2D contour plot for interactive effect of time and concentration on Removal of Hg(II) (b)

The effect of adsorbent dose

The effect of varying the adsorbent dosage on the adsorption of mercury ions and are shown in Figures (9) One of the most important variables influencing the biosorption process is the biomass dose, which is used to calculate the biosorbent capacity for a given initially concentration²⁸. Various amounts of algal biomass (0.1–0.7 g/250 ml) have been used in this study. It is clearly seen that the removal efficiency of Hg(II) ions increases from 30.8% to 95.7% as the algae biomass increases from 0.1 to 0.5 g/250 ml at concentration 1000 ppb and temperature 40 °C. because of a screen effect between biomass, the adsorption capacity remained constant, resulting in a block of the biomass functional groups²⁹ or because it is known that high doses of biomass produce agglomeration, which in turn decreases the intercellular distance and hence protects binding sites from contaminant exposure³⁰. Increases in biomass concentration often result in increased solute biosorption because more binding sites are available per unit of biosorbent surface area³¹. Because all sites were completely exposed to the pollutant at low biomass doses, the surfaces were saturated quicker, resulting in a larger value of q_e . Nonetheless, when the proportion of lower energy sites occupied grew with increasing doses of biomass, the availability of higher energy dropped, resulting in a lower q_e value.

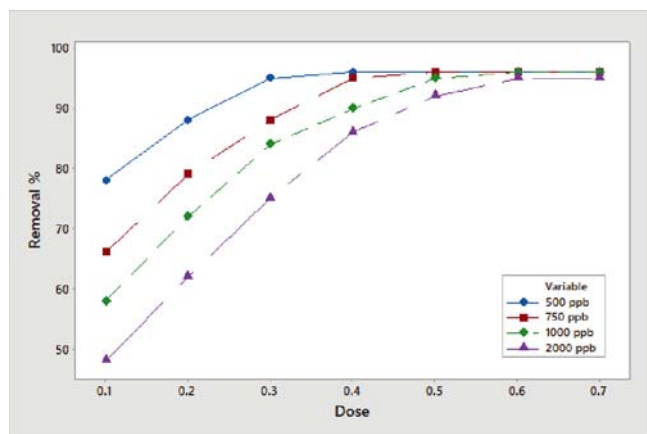


Figure 9. Effect of adsorbent dose on the rate of adsorption

Adsorption isotherms

Adsorption isotherm models were used to improve predictions of the connection between target species concentration and adsorbent surface³². To correlate the adsorption process of Hg(II) on algae, the equilibrium data was applied to three well-known adsorption models. The linear form of the isotherm models including, Langmuir³³, Freundlich³⁴, and Temkin³⁵ are given by Equation 6, 7, and 8, respectively.

Langmuir Isotherm

The Langmuir adsorption isotherm investigation involved the systematic alteration of the initial concentration of Hg(II) ranging from 500 $\mu\text{g/l}$ to 2000 $\mu\text{g/l}$, while maintaining all other parameters constant. The linear representation of the Langmuir adsorption is conveyed by Equation (5)²⁵. The Langmuir parameters were deduced from the gradient and intercept of the linear regression line established for the uptake of Hg(II) ions using green algae, as depicted in Figure 10 and summarized in Table 4. The congruence of the green algae adsorption data with the Langmuir model signifies the uniform nature of the adsorbent surface in relation to the binding of metal ions. Additionally, the high coefficient of determination (R^2) value of 0.9981 underscores a strong correspondence between the Langmuir constants and validates the assertion of monolayer adsorption of metal ions onto the adsorbent surface. Algae biomass was found to have a maximum adsorption capability of 495 g/g .

$$\frac{C_e}{q_e} = \frac{1}{q_{max}K_L} + \frac{C_e}{q_{max}} \quad (5)$$

where:

C_e is the equilibrium concentration of adsorbate ($\mu\text{g/g}$).

q_e is adsorption capacity at equilibrium ($\mu\text{g/g}$).

Table 4. Isotherm parameters

| Type of isotherm | Parameters | 20 C | 30 C | 40 C |
|------------------|---------------------------|---------|---------|----------|
| Langmuir | Q_0 ($\mu\text{g/g}$) | 432 | 474 | 495 |
| | b (L/mg) | 39.73 | 87.06 | 167.83 |
| | R^2 | 0.9951 | 0.9961 | 0.9981 |
| | R_L | 0.0324 | 0.015 | 0.00788 |
| Freundlich | K_F | 0.243 | 0.296 | 0.325 |
| | N | 4.58 | 7.77 | 10.78 |
| | R^2 | 0.9676 | 0.9374 | 0.9473 |
| Temkin | A | 0.0758 | 0.0048 | 0.000325 |
| | B | -0.0825 | -0.0523 | -0.039 |
| | R^2 | 0.9785 | 0.9513 | 0.9564 |

q_{max} is the maximum adsorption capacity ($\mu\text{g/g}$).

K_L is the Langmuir isotherm constant (L/mg).

The separation factor R_L , also recognized as the equilibrium parameter, is a dimensionless constant employed to encapsulate the fundamental attributes of the Langmuir isotherm²⁹.

$$R_L = 1 / (1 + K_L C_i) \quad (6)$$

Where: C_i is the initial concentration, K_L is the Langmuir isotherm constant (L/mg), R_L value indicates the adsorption nature to be either unfavorable if $R_L > 1$, linear if $R_L = 1$, favorable if $0 < R_L < 1$ and an irreversible if $R_L = 0$.

Freundlich Isotherm

The Freundlich parameters were calculated using the slopes and intercepts of the linear plots for Hg(II) ions uptake using green algae, as shown in Figure (11) and Table (4). The adsorption capacity and intensity were represented by the Freundlich constants K_f and n , respectively. The linear form of the Freundlich isotherm model is given by Equation (7)²⁷.

$$\log q_e = \log K_f + \frac{1}{n} \log C_e \quad (7)$$

Where: q_e = the amount of metal adsorbed per gram of the adsorbent at equilibrium ($\mu\text{g/g}$).

K_f = an approximate indicator of adsorption capacity.

$1/n$ = a function of the strength of adsorption in the adsorption process.

C_e = the equilibrium concentration of adsorbate ($\mu\text{g/l}$)³⁶.

Temkin Isotherm

$$q_e = B \ln A_T + B \ln C_e \quad (8)$$

q_e = the amount of metal adsorbed per gram of the adsorbent at equilibrium ($\mu\text{g/g}$).

A_T = Temkin isotherm equilibrium binding constant (L/g).

B = Constant related to heat of sorption (J/mol)³⁶.

The selection of a suitable model is determined by the presence of a high regression coefficient R^2 ³⁷. The derived parameters and the linearly fitted graph depicting the Temkin adsorption isotherm model are furnished in Table 4 and Figure 12. It is important to highlight that the configuration of the adsorption isotherm can provide substantial insights into the underlying adsorption mechanism. Collectively, as demonstrated, the Langmuir model offers a superior elucidation of the Hg(II) adsorption on algae, exhibiting a more substantial R^2 value compared to both the Freundlich and Temkin models. The Langmuir model's linear fitting yielded a maximum monolayer adsorption capacity of 750 $\mu\text{g/g}$ at 40 °C and

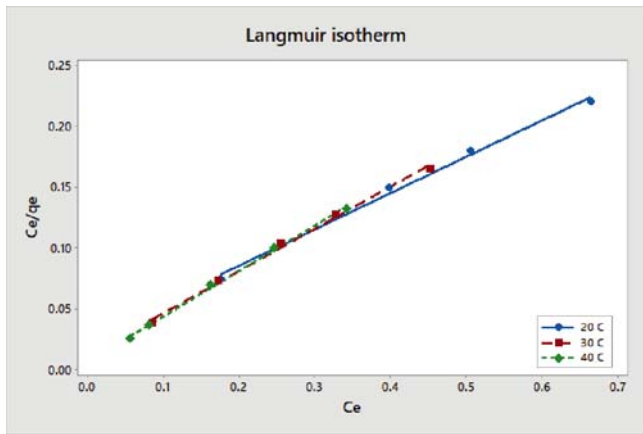


Figure 10. Langmuir isotherm plot for the adsorption of Hg(II) onto algae biomass

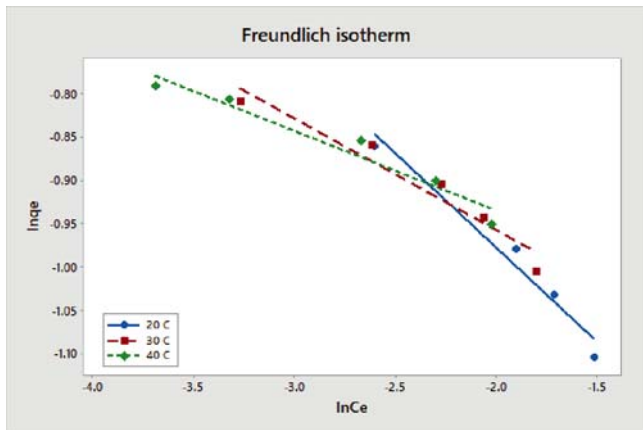


Figure 11. Freundlich isotherm plot for the adsorption of Hg(II) onto algae biomass

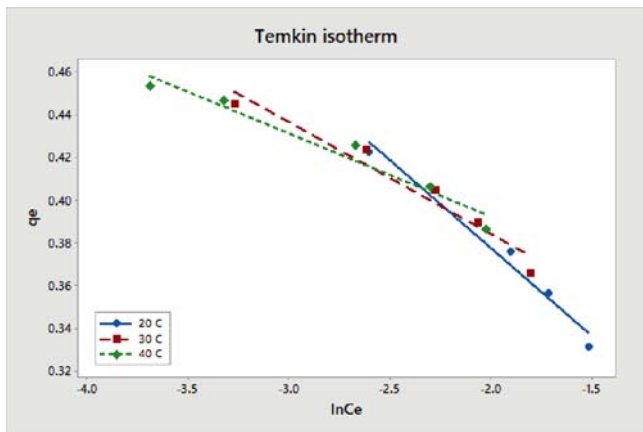


Figure 12. Temkin isotherm plot for the adsorption of Hg(II) onto algae

an initial concentration of 2000 ppb, signifying the favorable nature of the adsorption phenomenon.

Thermodynamic study

Thermodynamic parameters were manipulated within the temperature range of 20–40 °C, while maintaining initial Hg(II) ion concentrations at 750 ppb, and optimizing AFR and dose conditions. The thermodynamic attributes characterizing the absorption of Hg(II) ions by the algae biomass are organized in Table 5. Enthalpy and entropy values were extracted from the inclination and y-intercept of the $\ln K_C$ against $1/T$ graph, depicted in Figure 13. The obtained ΔH° value (40.62 kJ/mol) indicates an endothermic nature of the adsorption pro-

cess. The negative ΔG° values (–4.893 to –8.011 kJ/mol), signify the spontaneous nature of bioadsorption. The positive ΔS° value (154.86 J/mol K) implies heightened disorderliness at the solid/liquid interface during the bioadsorption of Hg(II) onto the algae biomass.

$$K_C = \frac{q_e}{C_e} \quad (9)$$

$$\Delta G^\circ = -RT \ln K_C \quad (10)$$

$$\ln K_C = \left(\frac{\Delta S^\circ}{R} \right) - \left(\frac{\Delta H^\circ}{RT} \right) \quad (11)$$

Where: K_C is the represents equilibrium constant of the adsorption, T is the temperature in K, and R is the gas constant.

Table 5. Thermodynamic parameters for the removal of Hg(II) by algae biomass

| T (K) | ΔG° (kJ/mol) | ΔH° (kJ/mol) | ΔS° (J/mol) |
|--------|---------------------------|---------------------------|--------------------------|
| 293.15 | –4.893 | 40.62 | 154.86 |
| 303.15 | –5.981 | | |
| 313.15 | –8.011 | | |

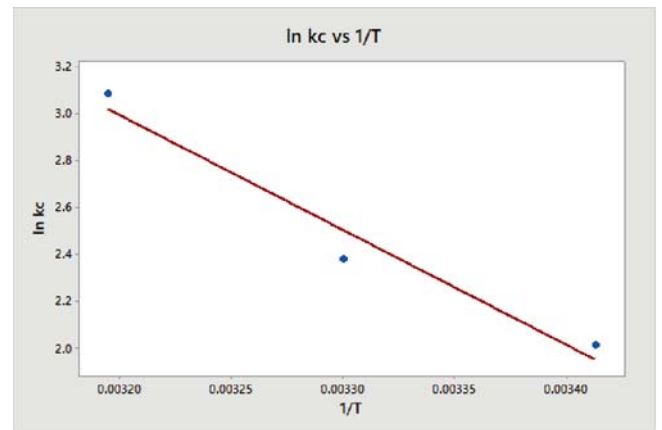


Figure 13. Van't Hoff plot for the removal of Hg(II) by algae bioadsorbent

Kinetic studies

The pseudo first and second-order kinetic models were used to explore the adsorption process of Hg(II) ions on the surface of algae with initial metal concentrations ranging from 500 to 2000 ppb.

Pseudo first-order

$$\log(q_e - q_t) = \log q_e - K_1 \frac{t}{2.303} \quad (12)$$

Where K_1 = the rate constant of adsorption

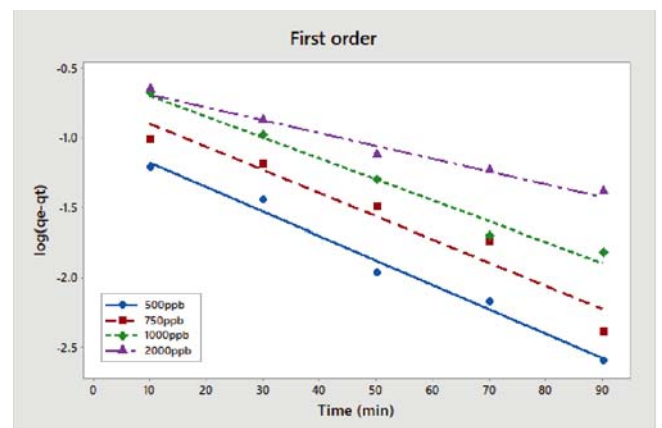


Figure 14. Pseudo-first-order kinetic model

Pseudo second-order

$$\frac{t}{q_t} = \frac{1}{K_2 q_e^2} + \frac{t}{q_e} \quad (13)$$

Where K_2 = the rate constant of pseudo-second-order kinetic model.

Understanding the adsorption mechanism and the potential controlling steps in terms of rate is essential for designing effective waste effluent treatment strategies. Various kinetic models are available for characterizing adsorption kinetics, with the pseudo-first-order and pseudo-second-order models being commonly employed. To assess the validity of these models, correlation coefficients (R^2) were employed.

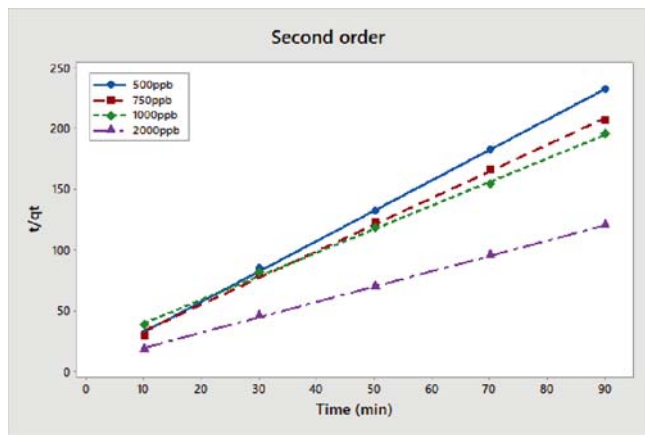


Figure 15. Pseudo-second-order kinetic model

Figures 14 and 15 portray the plots for the pseudo-first-order and pseudo-second-order kinetic models, respectively, illustrating the uptake removal of Hg(II) ions from its aqueous solution by the algal biosorbent. The collected data indicated that the pseudo-second-order model better described the adsorption system compared to the pseudo-first-order model. As outlined in Table 6, the correlation coefficient of the second-order kinetic model surpassed that of the pseudo-first-order model. This concordance underscores that the pseudo-second-order kinetic model effectively characterizes the obtained kinetic data and signifies that the adsorption of Hg by algae follows a natural chemisorption process.

Mass transfer adsorption models

The adsorption mechanism comprises multiple sequential processes, rather than a singular step, encompassing several pivotal stages. Consequently, the uptake of Hg from a solution by algae can be categorized into three distinct phases: (1) the external mass or boundary layer diffusion model, (2) the internal mass diffusion model, and (3) the chemical reaction occurring at the surface. Given that phase 3 is characterized by rapid responsiveness within the adsorption process, phases 1 and 2 assume the role of rate-limiting steps. The contribution of these rate-determining phases, whether they operate

individually or collectively, is integral to the progression of the reaction^{38, 39}.

Weber and Morris model

The Weber and Morris model, rooted in Fick's second law of mass transfer, is commonly employed in the context of the adsorption process to elucidate the mechanism of mass transfer from the exterior surface of the adsorbent to its internal pores⁴⁰. The intraparticle diffusion coefficient, as expressed by Equation 14, is derived through the utilization of the linearized form of the Weber-Morris model equation.

$$q_t = K_{imd} t^{0.5} + C \quad (14)$$

where:

q_t = the adsorption capacity at the time

t = time

K_{imd} = Weber and Morris diffusion coefficient

C = boundary layer thickness

by plot q_t against $t^{0.5}$ (Fig. 16) calculated all parameters by slope and intercept.

Figure 16 illustrates the presence of three discernible adsorption phases, substantiating the assertion that the binding of Hg to algae is governed by a comprehensive three-stage mechanism across the spectrum of examined Hg concentrations. In the initial stage (section 1 in Fig. 16), spanning up to 5.5 in x-axis (time), a linear trajectory is observed across all concentrations, indicating the influence of boundary layer diffusion as Hg molecules adhere to the algae's surface. The subsequent phase (section 2 in Fig. 16), encompassing the interval between 5.5 and 7 (min)^{0.5}, manifests a consistent linear alignment with all concentrations, attributable to the diffusion of Hg molecules through pores onto the algae. The last stage (section 3 in Fig. 16) of adsorption from 7 to 10 (min)^{0.5} revealed linear graphs for all concentrations, confirming that the adsorption process had achieved equilibrium and that all active sites of algae were completely saturated with Hg molecules. Table 2 details the computed values of the rate constant (K_{imd}),

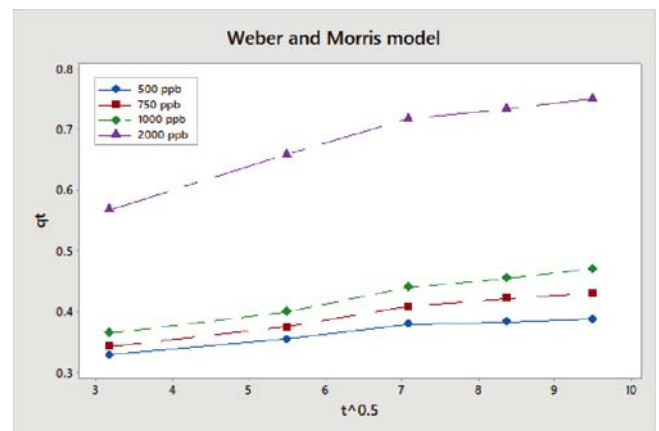


Figure 16. Weber and Morris model

Table 6. Pseudo-first-order kinetic model pseudo-second-order kinetic model

| C_i µg/l | q_e exp µg/g | q_e cal µg/g | K_1 Min ⁻¹ | R^2 | q_e cal µg/g | K_2 (g/mg · min) | R^2 |
|---------------|-------------------|-------------------|----------------------------|-------|-------------------|-----------------------|-------|
| 500 | 390 | 98.8 | 0.0403 | 0.984 | 398 | 0.9053 | 0.996 |
| 750 | 440 | 184.1 | 0.0382 | 0.940 | 454 | 0.4511 | 0.998 |
| 1000 | 475 | 286.4 | 0.0346 | 0.982 | 514 | 0.1883 | 0.999 |
| 2000 | 750 | 353 | 0.0211 | 0.976 | 745 | 0.2682 | 0.999 |

boundary layer thickness (C), and correlation coefficient (R²) deduced from the linear plots of qt against (t)^{0.5}.

As indicated in Table 7, the rate constant (K_{imd}) and boundary layer thickness (C) values exhibited an upward trend with the escalation of Hg content from 500 to 2000 µg/l. The elevation in Hg(II) concentration led to a corresponding increase in the C value, underscoring the significant role played by boundary layer thickness in the adsorption process, thereby influencing the adsorption capacity of algae. Notably, the C values demonstrated an ascent from 301 to 487 µg/g with the augmentation of Hg(II) concentration from 500 to 2000 µg/l, thus highlighting an intensified prevalence of the boundary layer diffusion mechanism under conditions of elevated concentration⁴¹.

Liquid film diffusion model

As per this proposition, a liquid layer composed of adsorbate molecules envelops the surface of the adsorbent. This adsorbate film holds pivotal significance in the adsorption process³⁹. In accordance with the Weber-Morris model, both film diffusion and pore diffusion mechanisms could potentially influence the mass transfer dynamics pertaining to the adsorption of Hg onto algae. Through the application of Equation 15, the assessment of diffusion coefficients (K_{fd}) and R² values was conducted, and the determined model parameters were compiled in Table 7 with the aid of slope and intercept analysis.

$$\ln\left(1 - \frac{q_t}{q_e}\right) = -K_{lf} t \quad (15)$$

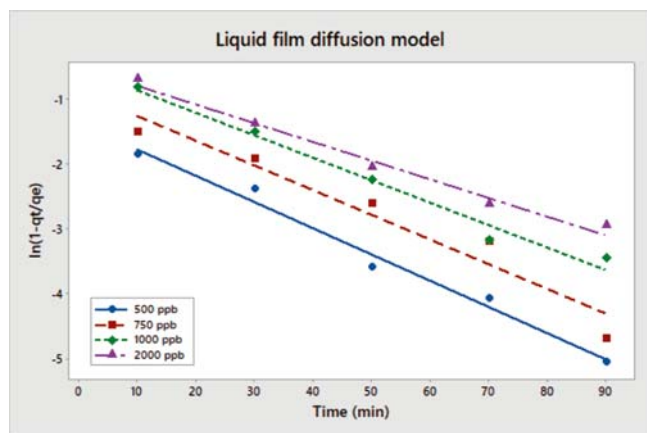


Figure 17. Liquid film diffusion model

Where:

q_t = adsorption capacity at time t,

q_e = adsorption capacity at equilibrium, t time

K_{lf} = liquid film diffusion rate constant,

by plot $\ln(1 - q_t/q_e)$ against t (Fig. 17) calculated liquid film diffusion rate constant by slope.

This shows that film diffusion is not just a rate-limiting phase in the adsorption of Hg molecules onto algae.

Bangham and Burt model

In specific adsorption systems, pore diffusion exclusively governs the rate-controlling stage. The utilization of the Bangham and Burt models offers a means to ascertain whether the adsorption process is regulated by pore diffusion or not⁴². Equation 16 presents the linearized expression of the Bangham and Burt model:

$$\log \log \left(\frac{C_i}{C_i - q_t m} \right) = \log \left(\frac{K_b m}{2.303 V} \right) + \alpha_2 \times \log t \quad (16)$$

Where C_i is initial concentration, m is the mass of adsorbent, V is the volume of Hg solution, q_t is the adsorption capacity at time t, K_b and α_2 are the Bangham constants, which were calculated by plot $\log \log \left(\frac{C_i}{C_i - q_t m} \right)$ against $\log t$ (Fig. 18) revealed that experimental data did not well fitted with this model. The evidence indicated a strong concordance between the experimental outcomes and this proposed model. The values for the model constant and R² are presented in Table 7. Across all concentrations, the R² values indicate that the progression of Hg molecule diffusion into the pores

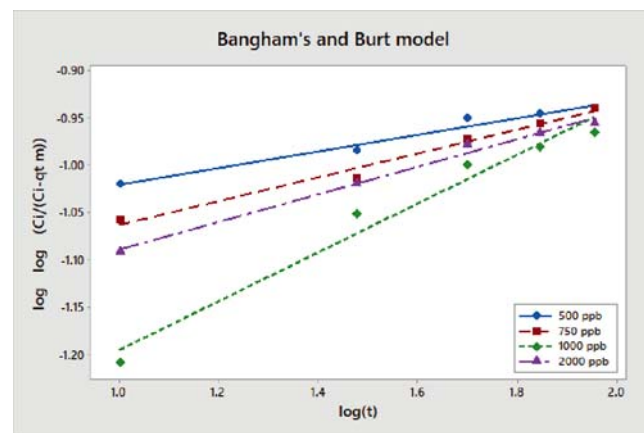


Figure 18. Bangham's and Burt model

Table 7. The values of the rate constant (K_{imd}) and boundary layer thickness (C)

| Mass transfer models | Mass transfer model parameter | | | |
|-----------------------------|-------------------------------|------------------|----------------|----------------|
| | Concentration µg/l | K _{imd} | C | R ² |
| Weber and Morris model | 500 | 0.0095 | 0.301 | 0.9472 |
| | 750 | 0.0151 | 0.294 | 0.9914 |
| | 1000 | 0.0317 | 0.182 | 0.9453 |
| | 2000 | 0.0293 | 0.488 | 0.9547 |
| Liquid film diffusion model | Concentration µg/l | K _{lf} | | R ² |
| | 500 | 0.0403 | | 0.9847 |
| | 750 | 0.0382 | | 0.9914 |
| | 1000 | 0.0346 | | 0.9822 |
| Bangham's and Burt model | Concentration µg/l | K _b | α ₂ | R ² |
| | 500 | 0.1490 | 0.088 | 0.9750 |
| | 750 | 0.0932 | 0.125 | 0.9829 |
| | 1000 | 0.0374 | 0.288 | 0.9822 |
| 2000 | 0.0557 | 0.146 | 0.9990 | |

of the algae significantly influences the rate, serving as a key controlling factor. Moreover, this diffusion process is influenced by boundary layer diffusion, either in isolation or in conjunction with both layer and pore diffusion mechanisms.

Table 7 illustrates that the rate constant (Kimd) values and boundary layer thickness (C) values exhibited an increase as the concentration of Hg content escalated from 500 to 2000 $\mu\text{g/l}$.

Comparison Between green algae biomass and another adsorbent

Table 8 compares the adsorption capacities of numerous adsorbents with those of the present study. The tabulated data illustrates that the existing adsorbent exhibits a notably elevated adsorption capacity towards Hg(II) in contrast to alternative adsorbents.

Table 8. Comparison of adsorption capacities for adsorption of Hg(II) ions using various low-cost adsorbents

| Adsorbent | Adsorption capacity | References |
|---------------------------------------|-----------------------|------------|
| Cellulose xanthate | 600 $\mu\text{g/g}$ | 11 |
| Xanthate | 1100 $\mu\text{g/g}$ | |
| Undyed bamboo pulp | 9.2 mg/g | 43 |
| Undyed sawdust | 8.5 mg/g | |
| Undyed jute | 7.6 mg/g | |
| ACFs-SH | 11–14 mg/g | 44 |
| POSS-SH | 12.9 mg/g | 45 |
| Apatite II (TM) | 38 mg/g | 46 |
| Sulfur-functionalized silica | 47.5 mg/g | 45 |
| BTESPT-SGs and MPTMS-SGs | 93.32 and 102.37 mg/g | 47, 48 |
| Algal biomass <i>Coelastrella</i> sp. | 750 $\mu\text{g/g}$ | This study |

CONCLUSION

In this investigation, the utilization of an environmentally friendly adsorbent, namely green algae, proved effective in the removal of the highly hazardous metal, Mercury, from simulated aqueous solutions. The efficacy of metal ion removal is notably contingent upon the specific adsorption conditions employed. The attainment of equilibrium in the adsorption of Hg(II) ions was achieved within a time frame of 90 minutes, under the conditions of a 40 °C temperature and a flow rate of 300 ml/min. The applicability of the Langmuir isotherm model and the pseudo-second-order kinetic model was demonstrated in effectively describing the adsorption data for Hg(II), revealing a maximum adsorption capacity of 750 $\mu\text{g/g}$. This study underscores the considerable potential of green algae biomass as a promising adsorbent for the removal of Hg(II). High removal efficiency encourage researchers to apply green algae to improve wastewater contaminated by heavy metal rather than Hg(II).

ACKNOWLEDGMENTS

We extend our sincere gratitude to the Chemical Engineering Department at the University of Technology-Iraq in Baghdad, Iraq, for their invaluable support and provision of space and necessary facilities that enabled the successful completion of this work.

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