

Evaluation of ground pollution by hydrocarbons using Rock-Eval pyrolysis

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The exploration and utilization of petroleum are potential hazards to the environment. Successful determination of petroleum contamination in ground relies on accurate definition of the type, source and quantity of contaminant. For this purpose the Rock-Eval[®] pyrolysis was applied, which is a rapid quantitative (Bulk Rock method) and qualitative (fractional composition using Multi-Heating Rates method) technique. Results of Rock-Eval analysis of 13 samples of concrete and 2 samples of gravel taken from the different sites of the petrol station indicate the highest concentration of light hydrocarbons (gasoline and naphtha fractions), up to over 5% wt. in the direct proximity of petrol pumps. Similarly high contamination (almost 4%wt.), was found near fuel tanks. Here the highest contribution has lubricating oil fraction and the tankers providing fuels are probably the source of this pollution. In the gravel collected in the vicinity of the fuel tanks high concentration (over 5 wt.%) of non-pyrolyzable carbon (soot) was recorded, the source of which are probably diesel engines of fuel tankers supplying fuel.

Keywords: Rock-Eval, oil, lubricants, ground pollution, petrol station.

INTRODUCTION

The worldwide exploitation and application of petroleum as source of fuel, lubricants, solvents and synthetic materials causes a serious environmental hazards. Consequently, there is a need to protect the environment against these products not only by preventing their leakage, but also by developing methods to detect these substances in the ground environment. By developing effective methods for identifying a pollutant, its composition, origin and properties, it will be possible to locate the source of its emission and prevent it, stop the further spread of pollution and develop ways to remove it from natural environment. The up-to-date methods of determination of petroleum contaminations quantity and origin applies usually solvent extraction techniques^{1, 2, 3} followed by analysis (e.g. chromatographic) of extract. This method allows the determination of the content of individual paraffinic, naphthenic, olefin and aromatic hydrocarbons and NSO-containing compounds, although is time- and cost-consuming. For the quick estimation of the quantity of hydrocarbons polluting soil Fourier Transform Infrared Spectroscopy (FT-IR) can be used^{4, 5}. Alternatively, the pyrolitical techniques may be applied (e.g. Py-GC-FID or Py-GC-MS)⁶.

One of the pyrolytic methods that is suitable to analyze the hydrocarbons-polluted ground is the Rock--Eval[®] programmed pyrolysis⁷. Currently this method is routinely used for the hydrocarbon potential analysis of source rocks in the oil and natural gas exploration studies⁸⁻¹¹, recent sediments^{12, 13} or soil organic matter characterization^{14, 15}.

The purpose of this work is to present, for the first time in literature, the feasibility of the programmed pyrolysis for estimating of quantity and determination of source of ground pollution by petroleum compounds (gasoline, diesel, lubricating and heavy oils and distillation residue) using the Rock-Eval 6 apparatus with the application of the Multi-Heating Rates (MHR) method based on data received for a selected petrol station in Cracow (Poland).

MATERIALS AND METHODS

Materials

The petrol station selected for this study has been working continuously for over 40 years. The concrete driveway was not renovated and cavities are visible. 13 samples of concrete from driveway of ca. 10 grams weight each were taken at different locations (Fig. 1) using hammer. The location of the sampling points was selected to statistically cover the station's area: both the places most exposed to pollution (at distributors and underground fuel tanks) as well as on the access and exit roads. The top layer of concrete was taken up to a depth of ca. 15mm. Typically, the samples consisted of fine concrete particles. Macroscopically all samples were similar to each other. Additionally 2 samples from the top layer of gravel (ca. 10 g each – a few pieces) near the driveway was collected (Fig. 1). Each sample was placed into separate, labelled glass jar.

Methods

Collected samples were pulverised to fraction below 0.2 mm in a rotary mill. For the Rock-Eval analysis ca. 50 to 100 mg of sample was placed into a special crucible.

The screening pyrolysis was completed with a Vinci Technologies Rock-Eval 6 Turbo apparatus in Bulk Rock method using the Basic cycle for all samples. This analysis consisted of two steps. Firstly, a crucible with rock sample was loaded by autosampler into a pyrolytic oven in which in a nitrogen atmosphere (flow of 100 ml/min) was heated from 300°C (3 min isothermal) to 650°C at 25°C/min. The generated gases were splitted 50 : 50. One portion was directed to a flame ionization detector (FID) for determination of free hydrocarbon content (released at isothermal heating at $300^{\circ}C - S1$ peak) and residual hydrocarbon content (released at 300-650°C -S2 peak) and second one, after water and tars removal - to an infra-red cell (IR) for determination of CO and CO₂ produced during decomposition of organic matter (OM) and carbonates (S3, S3', S3CO and S3'CO peaks).

Each pyrolyzed sample was then moved by autosampler to an oxidation oven where it was heated in air flow (100 ml/min) from 300°C (1 min isothermal) to 850°C at 20°C/min (5 min isothermal at final temperature). The produced CO (*S4CO* peak) and CO₂ (*S4CO₂* and *S5* peaks) were determined using an IR detector. Indices used for quantitative and qualitative evaluation of OM were calculated, i.e., pyrolytic (PC, wt.%), residual (RC, wt.%), total organic carbon content (TOC, wt.%) and production index (PI = S1/(S1 + S2)). Analytical details and formulas for calculation of PC, RC and TOC are presented elsewhere⁷.

For selected samples (the most polluted) the Multi--Heating Rates method was applied. In this method, the beginning of pyrolysis at 90°C and up to 5 independent temperature rates may be set. For the current study the temperature in the pyrolytic oven was programmed: start at 120°C (5 min of isothermal heating), increase of the temperature to 180°C at 10°C/min (5 min of isothermal heating), increase to 350°C at 15°C/min (5 min of isothermal heating), increase to 450°C at 20°C/min (5 min of isothermal heating), increase to 550°C at 25°C/ min (5 min of isothermal heating) and final heating to 650°C at 25°C/min. This procedure allows the separation of polluting hydrocarbons into 6 fractions corresponding to temperature intervals. The quantities of hydrocarbons released in individual temperature intervals have been marked as Q0, Q1, Q2, Q3, Q4 and Q5.

RESULTS

In our study 15 samples of concrete or gravel were taken at different locations at the selected gas station (Fig. 1).

Results of the *Bulk Rock* method were presented in Table 1. The free hydrocarbons content (released at 300°C, S1 peak) ranges from 0.03 to 52.1 mg/g, and residual hydrocarbons (released from 300 to 650°C, S2 peak) from 0.35 to 45.4 mg/g, respectively. Such variable contents of free and residual hydrocarbons result in PI values from 0.08 to 0.86. High content of free hydrocarbons, above 10 mg/g, was found in 3 samples: STB_1, STB_7 and STB_8, whereas so high residual hydrocarbons, in 4 samples: STB_1, STB_2, STB_9, STB_12 (Table 1). The exemplary pyrograms of samples rich in free and residual hydrocarbons are shown in Figure 2. The high



Figure 1. Sketch map of the petrol station with location of sampling sites

concentrations of hydrocarbons resulted in high, up to 5.2 wt.% of pyrolytic carbon content (Table 1). The non-pyrolysable (residual) carbon content varies from 0.13 to 5.4 wt.% and the TOC values changes from 0.2 to 5.7 wt.% (Table 1). The fraction of the pyrolytic



Figure 2. The FID-signals of the Bulk Rock method of (A) STB 2 and (B) STB 7 samples

Table 1. Se	lected parameters	and indices reco	eived during Roo	ck-Eval analysis ((Bulk Rock method)
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Sample	Type of sample	S1 [mg/g]	S2 [mg/g]	PI	PC [wt.%]	RC [wt.%]	TOC [wt.%]	PC/ TOC
STB_1	gravel	17.8	12.1	0.59	2.7	1.65	4.3	0.62
STB_2	concrete	1.02	45.4	0.02	3.9	1.62	5.5	0.71
STB_3	gravel	0.12	2.1	0.05	0.37	5.4	5.7	0.06
STB_4	concrete	0.05	0.63	0.08	0.1	0.19	0.29	0.34
STB_5	concrete	0.15	2.4	0.06	0.3	0.9	1.20	0.25
STB_6	concrete	1.11	5.0	0.18	0.6	0.55	1.15	0.52
STB_7	concrete	52.1	8.4	0.86	5.2	0.46	5.6	0.92
STB_8	concrete	30.4	5.1	0.86	3.0	0.38	3.4	0.89
STB_9	concrete	1.49	20.9	0.07	1.95	0.26	2.2	0.88
STB_10	concrete	0.39	1.24	0.24	0.21	0.27	0.48	0.44
STB_11	concrete	1.28	9.4	0.12	1.13	2.0	3.2	0.36
STB_12	concrete	4.1	20.2	0.17	2.2	0.67	2.9	0.77
STB_13	concrete	1.01	5.1	0.16	0.63	0.35	0.98	0.64
STB_14	concrete	0.05	0.35	0.12	0.07	0.13	0.20	0.35
STB_15	concrete	0.03	0.44	0.07	0.08	0.24	0.32	0.25

S1 – Free hydrocarbons released from sample in isothermal heating at 300°C; S2 – Residual hydrocarbons generated during thermal decomposition of organic matter from 300°C to 650°C; PI – Production index; PC – Pyrolytic carbon; RC – Residual carbon; TOC – Total organic carbon

carbon in the total organic carbon content varies from 0.06 (STB_3) to 0.92 (STB_7) (Table 1).

Based on preliminary results (Bulk Rock method), samples STB_1, STB_2, STB_7, STB_8, STB_9 and STB_12, as the most polluted, were selected for analysis by the Multi-Heating Rates (MHR) method to identify the fractional composition of polluting hydrocarbons. The results of these samples analyses are presented in Table 2. The Fig. 3 shows examples of pyrograms received during Rock-Eval analysis using MHR method.

The concentration of fractions evaporating below 120°C and above 550°C are low and do not exceed 0.5 mg/g rock. The concentrations of fractions released in



Figure 3. The FID-signals of the Multi Heating Rates method of (A) STB_2 and (B) STB_7 samples

the temperature ranges of $120-180^{\circ}$ C and $450-550^{\circ}$ C are higher, and vary from 0.09 to 17.1 and from 1.1 to 5.2 mg/g rock, respectively (Table 2). The highest concentrations are observed for fractions evaporating in the temperature ranges of 180–350°C and 350–450°C: from 3.5 to 30.8 (average 13.5 mg/g rock) and from 2.5 to 28.0 (average 12.6 mg/g rock), respectively (Table 2).

DISCUSSION

The concrete is made of cement and sand which are inherently poor in organic matter. Therefore the S1 and S2 values of two concrete samples taken outside the petrol station (STB_14 and STB_15) were assumed as the background effect associated with atmospheric pollution. Their low values of S1 and S2 (ca. 0.04 mg/g and ca. 0.40 mg/g, respectively) are negligible and were considered as reference material to other samples (Fig. 4).

The distribution of hydrocarbon pollution at analyzed petrol station is presented on Figure 4. Samples containing the highest HC concentrations (up to 60 mg/g rock) were recorded in the direct proximity of petrol pumps (samples STB 7 and STB 8) and close to underground fuel tanks (sample STB_2). Also elevated concentrations of hydrocarbons were recorded in concrete on the exit road from the gas station (samples STB 9 and STB 11) being probably the result of spreading pollutants from distributors by vehicles. High concentration of hydrocarbons, with dominating share of light fractions (PI = 0.59) was recorded in gravel sample collected near to underground fuel tanks (STB 1, Fig. 4). Source of pollutants in this sample is probably the same as for sample STB 2 and are connected with fuel tanks. Because the gravel is made of porphyry, which as a igneous rock is devoid of organic matter, all recorded organic material is of anthropogenic origin. Another gravel sample (STB 3), collected in the vicinity of STB 1 and STB 2 samples (Fig. 1), is much lower polluted by pyrolyzable hydrocarbons than previously described ones (Table 1, Fig. 4), but it contains comparable amount of TOC to them (Table 1). The dominating mass of organic carbon in this sample is non-pyrolyzable residual carbon (soot), the source of which is probably fuel tankers supplying fuel. Sampling point STB 3 is located close to the exhaust outlet of parked trucks.

The applied Multi-Heating Rates method allowed determining the proportion between the gasoline fraction (up to 180°C), diesel oil (180–350°C) and heavy fractions (most of all lubricating oil, above 350°C) in organic material occurring in analysed samples (Table 3).

In the samples collected at the petrol pumps (STB 7 and STB 8) gasoline and diesel oil fractions dominate (Table 3, Fig. 5), as the result of fuels spill during refuelling of cars. Although light fractions should evaporate quickly, their concentration is considerable. This is facilitated by the roofing of the area where the fuel distributors are located and the permanent "supply" of pollutants to the ground. The sample taken in the vicinity of another fuel pump (STB 12) and from the exit way from the station (STB 9) are rich in heavy fractions (lubricating oil), evaporating at temperatures above 350°C (Fig. 5). The fraction of diesel oil does not exceed 30% and the gasoline fraction is below 3% (Table 3). These pollutants are the result of oil leaks from car engines or are the residue after partial evaporation of low-boiling gasoline and diesel oil fractions.

Table 2. Results of Rock-Eval pyrolysis (Multi Heating Rates method)

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Fraction	Q0	Q1	Q2	Q3	Q4	Q5	QT
Temperature interval	0–120°C	120–180°C	180–350°C	350-450°C	450–550°C	550–650°C	
STB_1	0.01	1.77	18.1	9.4	2.1	0.12	31.5
STB_2	0.01	0.09	5.4	28.0	5.2	0.19	38.9
STB_7	0.42	17.1	30.8	3.9	1.71	0.07	54.0
STB_8	0.23	10.0	16.7	2.5	1.07	0.04	30.6
STB_9	0.04	0.25	3.5	18.3	1.66	0.05	23.8
STB_12	0.03	0.61	6.8	13.7	2.5	0.05	23.7

Q0, Q1, Q2, Q3, Q4, Q5 – quantity of hydrocarbons released during given temperature interval; QT – Total quantity of hydrocarbons; all values in mg/g rock



Figure 4. Distribution of the total concentration of hydrocarbons in ground samples (Bulk Rock method)



Figure 5. Fraction composition of hydrocarbons polluting ground in selected sites of the petrol station

The contamination recorded near fuel tanks (almost 4 wt.%, sample STB_2) is dominated by heavy fractions (Table 3, Fig. 5). The source of pollution in this area may be both nearby fuel tanks (during filling – fuel spill and leaks of lubricating oil from engines and car tanker instrumentation), as well as passing cars. The neighbouring STB_1 sample is significantly enriched in lower boiled fractions (especially diesel oil) to the STB_2 sample. These pollutants are the result of the

rain rinsing the most water-soluble hydrocarbons from vicinity of fuel tanks (site STB_2), and depositing them in the gravel next to the driveway (site STB_1, Fig. 5); the area around fuel tanks is not covered, therefore it is open to weather conditions.

CONCLUSIONS

The performed analyses show the possibility of using the Rock-Eval method for quickly estimate the amount

Table 3. Fraction composition of hydrocarbon pollutants

		Fraction [mg/g]		Fraction composition [%]			
Sample name	Gasoline	Diesel oil	Heavy fractions (lubricating oil)	Gasoline	Diesel oil	Heavy fractions (lubricating oil)	
	0–180°C	180–350°C	350–650°C	0–180°C	180–350°C	350–650°C	
STB_1	1.78	18.1	11.6	5.7	57.4	36.9	
STB_2	0.10	5.4	33.4	0.3	14.0	85.8	
STB_7	10.3	16.7	3.6	33.6	54.5	11.9	
STB_8	17.5	30.8	5.7	32.4	57.0	10.6	
STB_9	0.29	3.5	20.0	1.2	14.6	84.2	
STB 12	0.64	6.8	16.3	27	28.7	68.6	

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and fractional composition of hydrocarbon pollutants in grounds most exposed to hydrocarbon degradation (hydrocarbon mines, refineries, tanks, trans-shipment and petrol stations). Due to short time of analysis (ca. 1.5 hr), high sensitivity (0.01 mg HC/g rock) and small necessary sample (ca. 100 mg) it can be used to determine even traces of pollutants as alternative to long-lasting extraction using organic solvents. In addition to analyzing the amount and fractional composition of pyrolyzable hydrocarbons, this method allows to determine the amount of carbon occurring in the form of dust (soot, coke) or recent organic debris, which is not detected by extraction methods. Due to the necessary preparation of sample for analysis (homogenization, grinding), the determination of the low-boiling fractions content and composition may be erroneous. The accurate results are obtained by analyzing heavier fractions (C_{15+}) .

Because the pyrolytical analysis is not selective, during heating of sample, there are decomposed and released all organic compounds evaporated/cracked at given temperature. Therefore, special attention must be paid to samples containing residual organic matter, not related to hydrocarbon contamination (eg. organic debris dispersed in soil or other sediments^{12–15}) and before determining the amount and type of contamination, it is necessary to perform background analysis for samples collected from the same type of ground not contaminated with petroleum products.

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