

Three-phase hybrid transformer using matrix-chopper as an interface between two AC voltage sources

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(Received: 26.11.2013, revised: 12.02.2014)

Abstract: This paper deals with a three-phase power system with hybrid transformer (HT) installed between two AC sources. The main aim of this paper is analyze the basic properties of HT with active load and ability to bidirectional energy flow. The HT contains two main units – a conventional transformer with electromagnetic coupling and PWM AC line chopper connected with secondary windings with electric coupling. The HT is located between the distribution system and a Local Balancing Area (LBA) with low power local energy sources. After describing the HT circuit and three-phase, two-sources power system, the mathematical and circuit models of the AC source with HT are presented. These models are verified by means of the simulation and experimental test results obtained for a three-phase HT of about 3 kVA rated power.

Key words: hybrid transformer, power system, matrix chopper

1. Introduction

The parameters of electric energy, its quality, are very important especially from the viewpoint of the end-user. The parameters of electric energy are well known and described in [1]. Classification of AC voltage variation is shown in Figure 1. The voltage interruptions are divided into two types: short interruption (from 10 ms to 3 minutes) and long interruption (over 3 minutes) (Fig. 1).

An Expanded and centralized AC electrical system is exposed to many different faults. Moreover the energy is often transferred in the long distances (Fig. 2a). The causes and effects of distortion in AC electrical system are shown in Figure 2. In the case of dynamic variations in an AC electrical system, e.g. fast load changes, switching effects, atmospheric discharges, faults, on the consumer side, undesirable effects are generated, such as voltage dips (87.2% of all distortion in the power grid), interruptions and swells (Fig. 2b) [2, 3].

In the case of the AC voltage supply changes, both downward and upward, there is a high risk of damage to devices, which are sensitive to voltage changes, for example: computers, transceiver devices, medical systems [4-6].

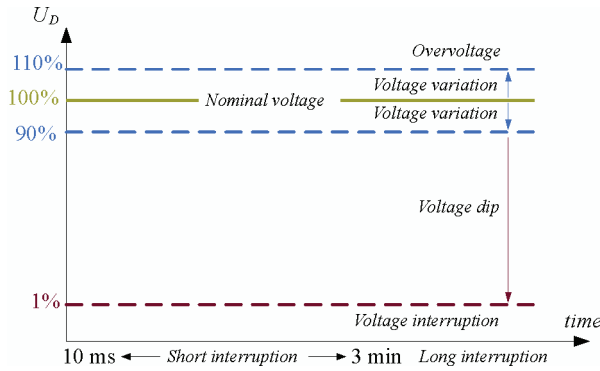


Fig. 1. Classification of voltage variation depending on size of change, U_D – declared supply voltage

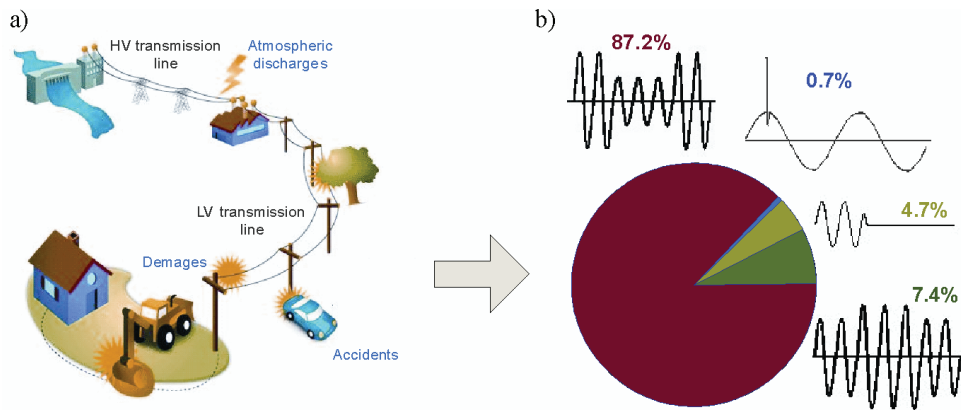


Fig. 2. Distortion in power grid – a) causes, b) effects

In the case of big plants and factories, voltage sags and swells may cause very large financial damage. The application of an AC-AC converter using Pulse Width Modulation (PWM) control strategy to build secondary supply sources (voltage sag and swell compensators and voltage regulators) mitigate unwanted detrimental effects in the supply [8-12]. Some types of AC voltage controller for compensation of deep and rapid voltage sags and overvoltages use the hybrid transformer (HT) described in [13-19]. A simplified schematic diagram of a HT connected to the AC power system is shown in Figure 3. In this case the HT unit is working with a passive load as an AC voltage controller.

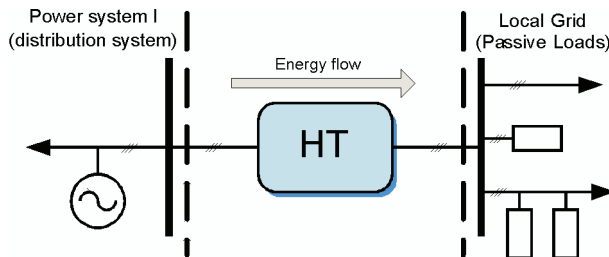


Fig. 3. Hybrid transformer installed in power system with passive load

In the case of modern AC power systems (smart grids) there are possibilities to connect low power renewable energy sources (photo voltaic panels – PV, wind generators) to low voltage AC systems. The renewable energy sources are connected to the grid by power electronic interfaces [8, 9]. Voltage fluctuations in low voltage AC power systems can be caused by turning on and turning off of renewable energy sources connected to the grid, being dependent on the condition of the source energy (wind, sun, water flow, etc.). Local AC systems (subsystems), such as residential houses, schools, academic campuses, etc., along with low power energy sources connected to a local AC subsystem is called a “Local Balancing Area” (LBA). In a LBA with low power local energy sources, during the operation of the subsystem there is a risk of change (fluctuation) in voltage amplitude in the LBA. This is caused by operational conditions (turn-on and turn-off) of energy sources connected to the LBA. In the case of a HT connected to a power system with a LBA (Fig. 4), the HT in fact is loaded by active load. For this reason it is necessary to obtain bidirectional power flow in the HT circuit.

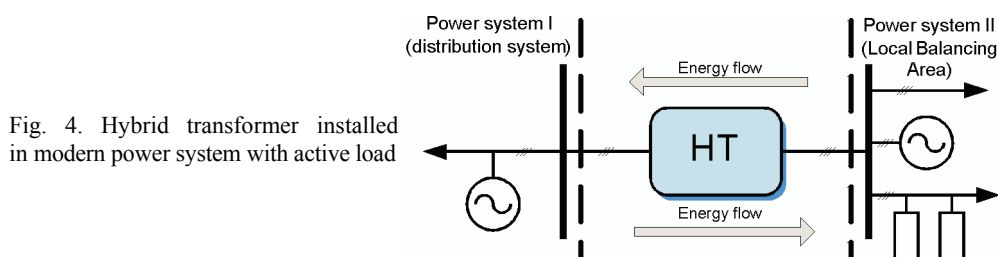


Fig. 4. Hybrid transformer installed in modern power system with active load

This paper presents the modelling and analysis of a three phase hybrid transformer using the matrix chopper described in [15] with active load (two-sided supply). The next chapter describes the topology and operation of the presented HT. Following this are chapters on the simulation and experimental test results and conclusions.

2. Description of analysed circuit

The schematic diagram of the considered HT with active load is shown in Figure 5. The circuit of the HT contains two main units. The first one is a three-phase conventional transformer (TR), with two secondary windings in each phase. The second one is a three-phase matrix chopper (MC). Primary windings are in Y-configuration. The main secondary windings (a_1, a_2, a_3) of the TR are also Y-configured and, by an input filter $L_F C_F$, are connected with the MC. Secondary phase windings (b_1, b_2, b_3) are connected in series with the output filter $L_L C_L$ of the MC. The voltages of the transformer secondary windings a_1, a_2, a_3 and b_1, b_2, b_3 are set with the ratios $p_a = 4/3$ and $p_b = 2/3$ respectively [15, 16]. Output voltages of the HT (u_{L1}, u_{L2}, u_{L3}) are the sum of secondary voltages ($p_b u_{S1}, p_b u_{S2}, p_b u_{S3}$) and the phase output voltages of the MC. The output voltages of the HT (u_{L1}, u_{L2}, u_{L3}) are controlled by means of a control unit. The voltages u_{01}, u_{02}, u_{03} are voltages of power system II (LBA) with active load (Fig. 5).

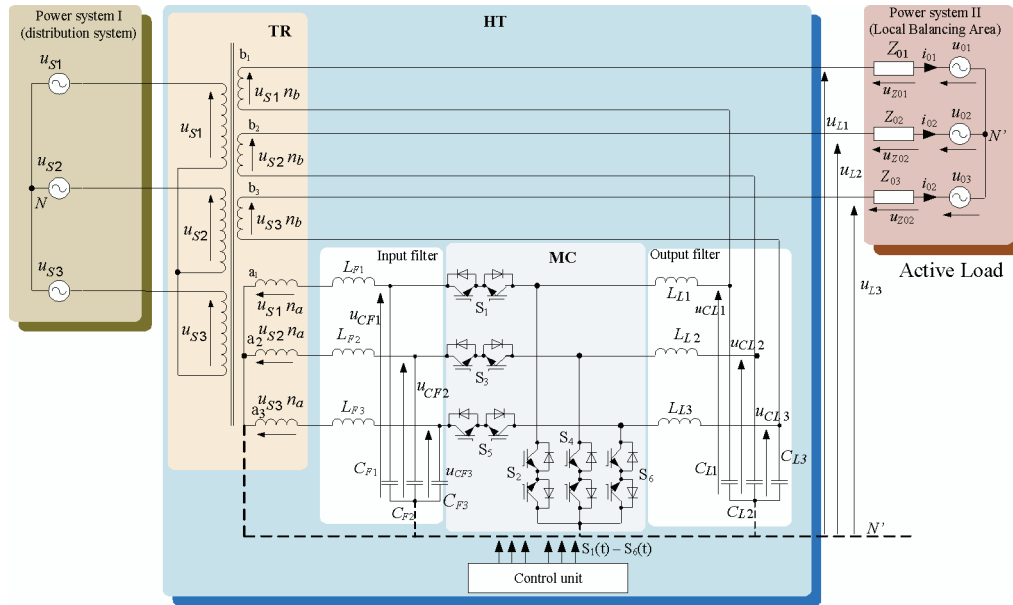


Fig. 5. Three-phase hybrid transformer using matrix chopper with active load

Exemplary idealized voltage time waveforms and voltage phasors, illustrating operation of presented HT with matrix chopper working as an AC voltage regulator are shown in Figure 6.

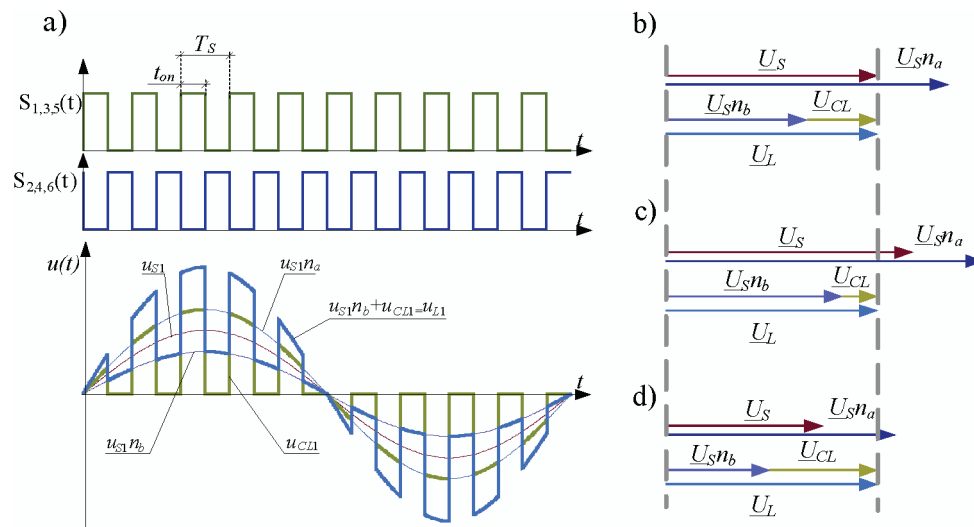


Fig. 6. Exemplary idealized voltages of HT: a) time waveforms at switching frequency $f_s = 500$ Hz, b) phasors during nominal conditions, c) during source voltage swell, d) during source voltage sag

The duty cycle of the control signal of MC switches ($S_1 - S_6$) is expressed as

$$D = \frac{t_{on}}{T_S}, \quad (1)$$

where T_S – switching period, t_{on} – turn-on time of switches S_1, S_3, S_5 .

The output voltage of MC ($u_{CL1}, u_{CL2}, u_{CL3}$) is linear depending on D [15, 16] and can be written as (2).

$$U_{CL} \cong n_a U_S D. \quad (2)$$

The output voltage of HT (u_{L1}, u_{L2}, u_{L3}) results from the addition of two voltages. The output voltage of MC ($u_{CL1}, u_{CL2}, u_{CL3}$) and secondary voltage ($u_{S1n_b}, u_{S2n_b}, u_{S3n_b}$) is induced in secondary windings of TR (b_1, b_2, b_3). Therefore load voltage of HT can be expressed as

$$U_L \cong n_a U_S D + n_b U_S. \quad (3)$$

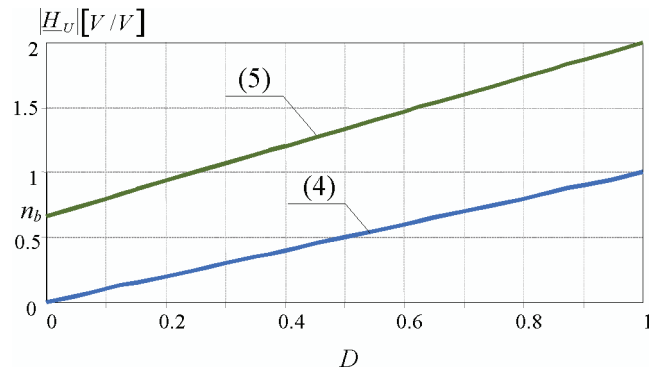
According to (2), the idealized voltage transmittance of MC can be written as (4) [15, 16] and is shown in Figure 7.

$$H_U^{MC} \cong \frac{U_{CL}}{n_a U_S} = \frac{n_a U_S D}{n_a U_S} = D. \quad (4)$$

According to (3), the idealized voltage transmittance of HT can be described by (5) and is shown in Figure 7.

$$H_U^{HT} \cong \frac{U_L}{U_S} = \frac{n_a U_S D + n_b U_S}{U_S} = n_a D + n_b. \quad (5)$$

Fig. 7. Idealized characteristics of voltage transmittances of presented HT and MC as a function of the duty cycle D



The output voltage of HT u_L is dependent on duty cycle D (Fig. 7), and for the considered circuit is controlled from $0.66u_S$ to $2u_S$ [15, 16].

Shown in Figures 8 and 9 are exemplary idealized voltage waveforms illustrating the operation of the presented circuit for various values of pulse duty factor D , in condition $U_S = U_0$ with low switching frequency $f_S = 500$ Hz. To give an operational illustration, a resistance load is used.

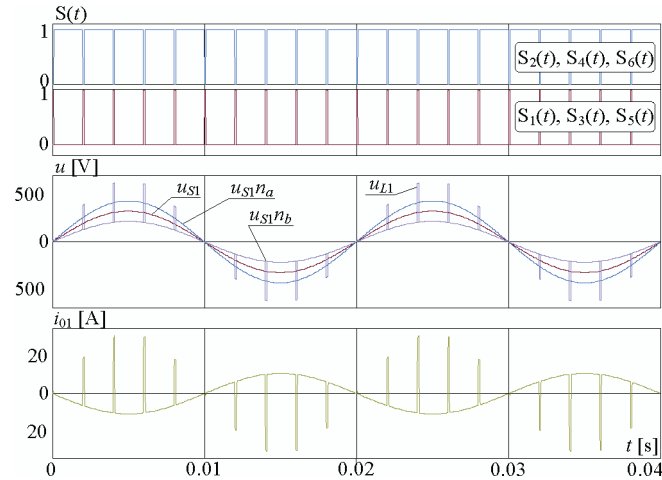


Fig. 8. Idealized voltage and current waveforms for $D = 0.1$ and $f_S = 500$ Hz, illustrating operation of analyzed HT

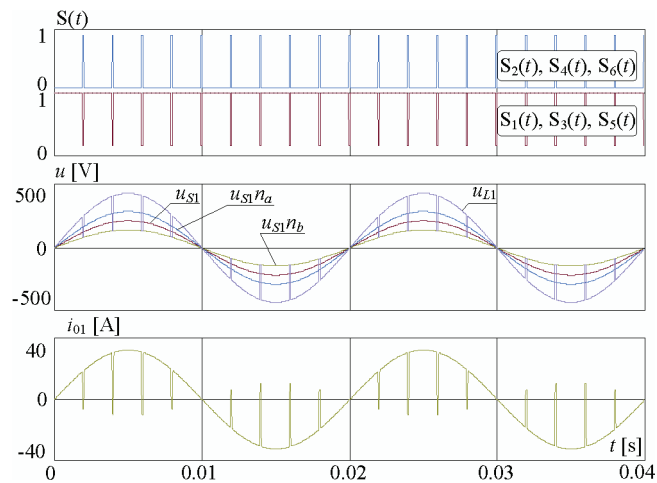


Fig. 9. Idealized voltage and current waveforms for $D = 0.9$ and $f_S = 500$ Hz, illustrating operation of analyzed HT

As is visible in Figures 8 and 9, the phase of the load current i_0 in the HT circuit is dependent on the value of pulse duty factor D . If the output voltage of the HT (U_L) is greater than the active load voltage (U_0) (Fig. 9) then the current i_0 is in phase with the output voltage of the HT. This means that energy is transferred from the source U_S to the load (from power system I to power system II). In the case when the output voltage of the HT is less than the active load voltage ($U_S < U_0$) (Fig. 8) then the current i_0 is in opposite phase in relation to the output voltage of the HT. This means that energy is transferred from the active load to the voltage source U_S (from power system II to power system I).

3. Theoretical analysis

Assuming a symmetrical and balanced circuit in the HT and a symmetrical three-phase supply source and active load source, we can show the circuit in Figure 5 as a single phase circuit [15]. Taking into account a substitute scheme of transformer [20] and an averaged circuit model of the matrix chopper [21], the single-phase schematic diagram of the considered HT, after converting all parameters of the TR to a secondary side, is shown in Figure 10.

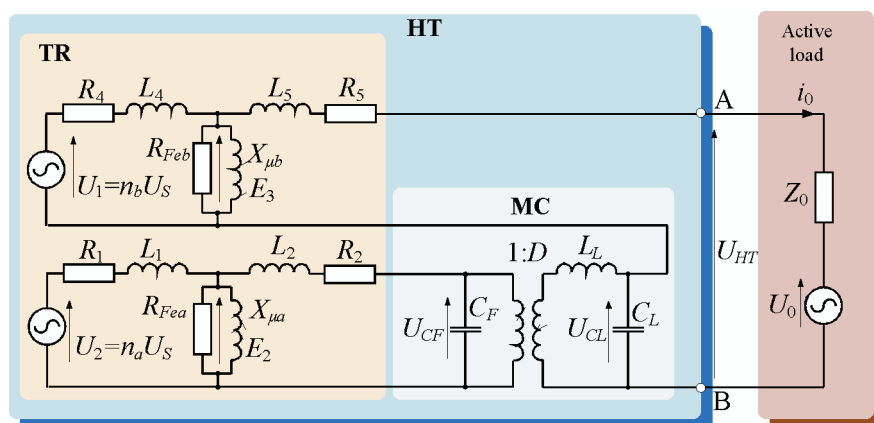


Fig. 10. Single phase model of HT with active load

Table 1. Parameters of substitute circuit of transformer TR conversion to the secondary side of TR

Parameter	Name	Value	Unit
n_a	voltage ratio	4/3	–
n_b	voltage ratio	2/3	–
R'_1	resistance of primary windings	1.12	Ω
R_2	resistance of secondary windings a	0.92	Ω
R'_{Fea}	core losses	7605	Ω
R'_4	resistance of primary windings	0.28	Ω
R_5	resistance of secondary windings b	0.163	Ω
R'_{Feb}	core losses	1901	Ω
X'_{L1}	leakage reactance	0.48	Ω
X_{L2}	leakage reactance	0.28	Ω
$X'_{\mu a}$	magnetizing reactance	6112	Ω
X'_{L4}	leakage reactance	0.036	Ω
X_{L5}	leakage reactance	0.081	Ω
$X'_{\mu b}$	magnetizing reactance	1528	Ω
U_S	supply voltage	230/400	V
U_1	secondary voltage	$n_b U_S$	V
U_2	secondary voltage	$n_a U_S$	V
S	apparent power	10	kVA

The parameters of the transformer TR after conversion to the secondary side are collated in Table 1.

On the basis of Thevenin's method, and according to Figure 10, we can very simply obtain the simplify substitute circuit of the analyzed HT with substitute source (Fig. 11).

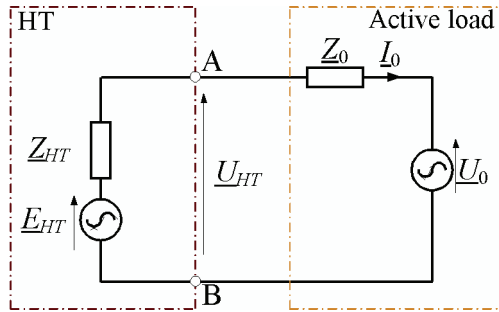


Fig. 11. Simplified equivalent circuit of considered HT with active load

The equivalent source and equivalent impedance of the analysed HT from Figure 11 in complex form are defined as (6) and (7).

$$\underline{Z}_{HT} = \frac{(106.6 - j244.8) + (0.44 - j317.3)D^2}{(-132.75 - j111.84) + D^2}, \quad (6)$$

$$\underline{E}_{HT} = (0.99 + j0.00016)U_1 - \frac{(49.5 + j133.3)U_2}{(-48.47 - j133.15) + D^2}, \quad (7)$$

where U_1 and U_2 are voltages being converted to the secondary side of the transformer TR (Fig. 10, Table 1).

The static characteristics of (6) and (7) and the phase of magnitude of \underline{E}_{HT} as a function of duty cycle D are shown in Figures 12 and 13.

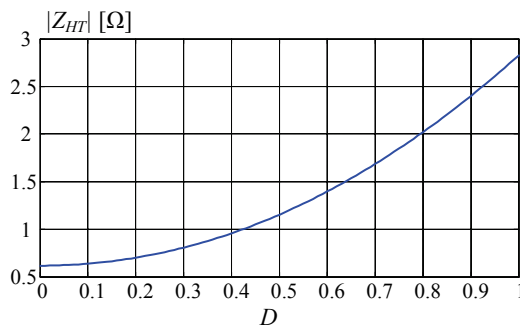


Fig. 12. The magnitude of impedance of HT as a function of D

As is visible in Figure 12 the magnitude of the impedance of the HT is dependent on duty cycle D and is changeable in the range 0.6-2.75 Ω . Assuming a supply RMS line voltage of 3×230 V, the range of change of output voltage is from 153 V ($H_{U(D=0)} = 2/3$) – 460 V ($H_{U(D=1)} = 2$) (in accordance with the voltage transmittance of the HT (5) and Fig. 7).

Fig. 13. The magnitude of the output voltage of HT as a function of D

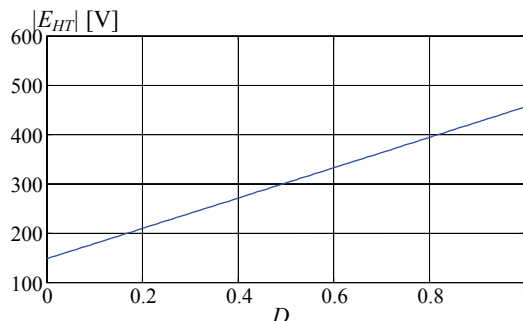
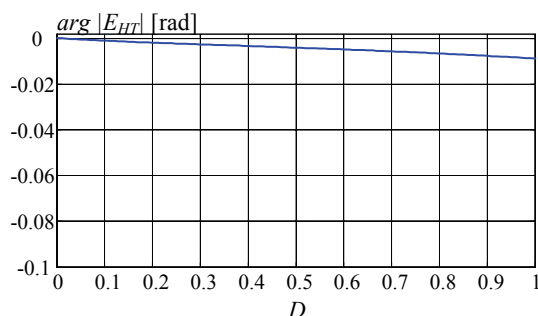


Fig. 14. The phase of output voltage as a function of D



In Figure 13 we can see the static characteristics of the substitute source $|E_{HT}|$ as a function of duty cycle D . Phase shifting E_{HT} voltage (Fig. 14) is caused by passive elements of input and output filters in MC topology and by reactance elements of TR (Fig. 10).

4. Simulation and experimental tests results

A) Simulation results

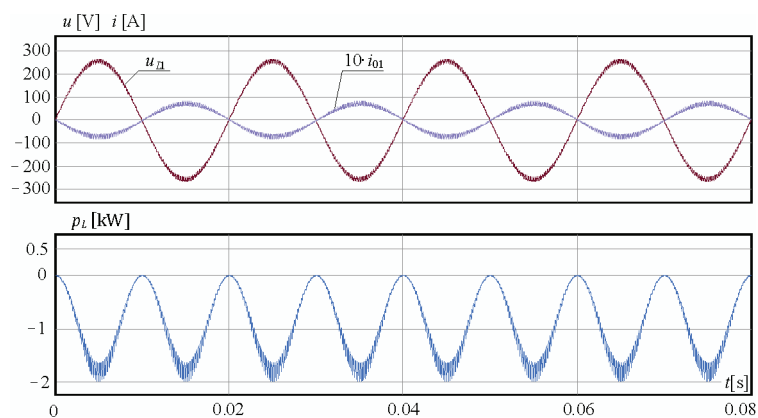
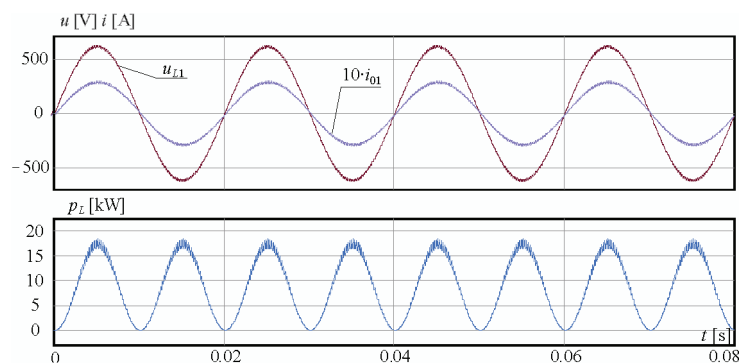
The parameters of the simulation circuit of the analysed HT with active load are collated in Table 2. The presented simulation results were obtained from the dedicated simulation program PSim. In the simulation model was used idealized passive components and ideal switches. Therefore, the simulation model was operated without dead time.

As is visible in Figs. 15 and 16, the output voltage of the HT (U_L) is dependent on duty cycle D . In the case when the output voltage U_L is less than the active load voltage U_0 ($U_L < U_0$) the current i_{01} in the HT circuit is in the opposite phase in relation to the source voltage u_{S1} . For this reason the instantaneous power p_L has negative value (Fig. 15). This means that energy is transferred from source voltage U_0 . If $U_L > U_0$ (Fig. 16), then instantaneous power p_L is positive. This means that energy is transferred from source voltage U_S .

In the case when source voltage U_L is equal to load voltage U_S (Fig. 17) the current $I_0 \approx 0$ and the averaged value of power $P \approx 0$. This means that energy is not transferred in these conditions.

Table 2. Parameters of simulation circuit

Parameter	Name	Value	Unit
n_a	voltage ratio	4/3	–
n_b	voltage ratio	2/3	–
U_S	source voltage	230/400	V
f	supplying frequency	50	Hz
$L_{F1} = L_{F2} = L_{F3}$	input filter inductance	1	mH
$C_{F1} = C_{F2} = C_{F3}$	input filter capacitance	10	μF
$L_{L1} = L_{L2} = L_{L3}$	output filter inductance	1	mH
$C_{L1} = C_{L2} = C_{L3}$	output filter capacitance	10	μF
$ Z_{01} = Z_{02} = Z_{03} $	load impedance	10	Ω
U_0	load source voltage	230/400	V
f_S	switching frequency	5	kHz
S	apparent power	10	kVA

Fig. 15. Simulation waveforms of voltage, current and power for duty cycle $D = 0.1$ Fig. 16. Simulation waveforms of voltage, current and power for duty cycle $D = 0.9$

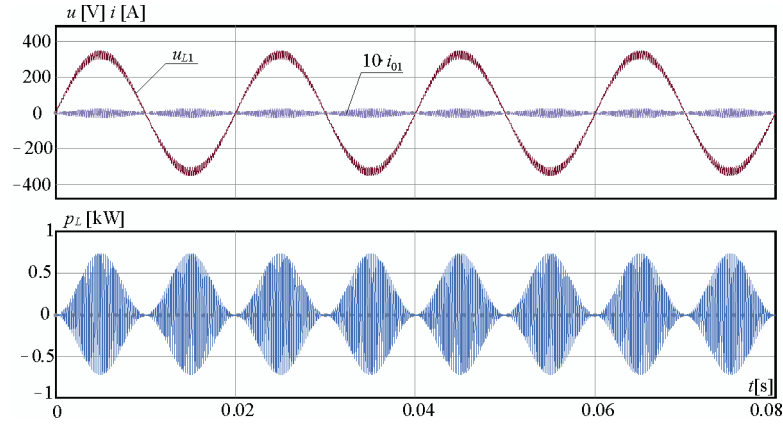


Fig. 17. Simulation waveforms of voltages, currents and instantaneous power for $D = 0.25$

B) Experimental results

A three-phase, 1-kVA prototype has been built and tested in an open-loop control condition. The parameters of the experimental model are shown in Table 3.

Table 3. Parameters of experimental circuit

Parameter	Name	Value	Unit
n_a	voltage ratio	4/3	–
n_b	voltage ratio	2/3	–
U_S	source voltage (rms)	3×50	V
f	supplying frequency	50	Hz
$L_{F1} = L_{F2} = L_{F3}$	input filter inductance	1	mH
$C_{F1} = C_{F2} = C_{F3}$	input filter capacitance	10	μF
$L_{L1} = L_{L2} = L_{L3}$	output filter inductance	1	mH
$C_{L1} = C_{L2} = C_{L3}$	output filter capacitance	10	μF
$ Z_{01} = Z_{02} = Z_{03} $	load impedance	30	Ω
U_0	load source voltage	3×50	V
f_S	switching frequency	5	kHz
IGBT	transistors	IRG4PHUD	–
S	apparent power	10	kVA

The matrix chopper is controlled via a PWM control strategy. The switching frequency is set to 5 kHz, and the “dead time” for commutation is set at $0.7 \mu\text{s}$. The bidirectional switches are implemented with two IRG4PHUD IGBTs connected in emitter-to-emitter configuration. For reasons of safety the AC input rated voltage was $50 V_{\text{RMS}}$. The output voltages of considered HT are depend on duty cycle D and can be adjusted flexible from a value smaller than source voltages (Fig. 18a) to about two times greater than source voltages (Fig. 18b).

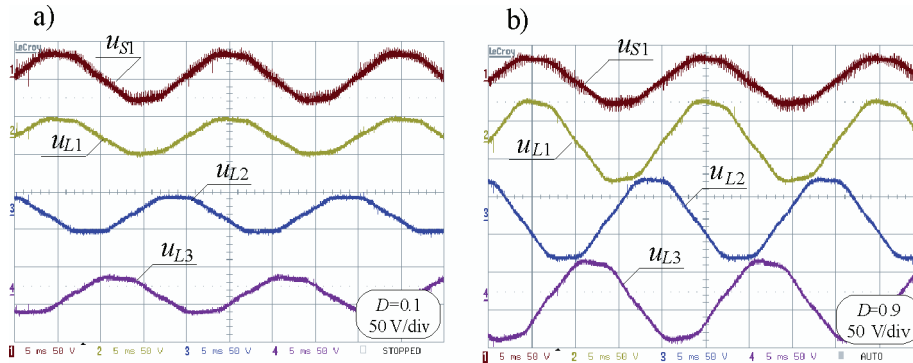


Fig. 18. Experimental line voltage waveforms of HT, for various value of duty cycle: a) $D=0.1$, b) $D=0.9$

The voltages, currents and instantaneous power waveforms for various values of duty cycle D and for $U_S = U_0$ are shown in Figures 19-21.

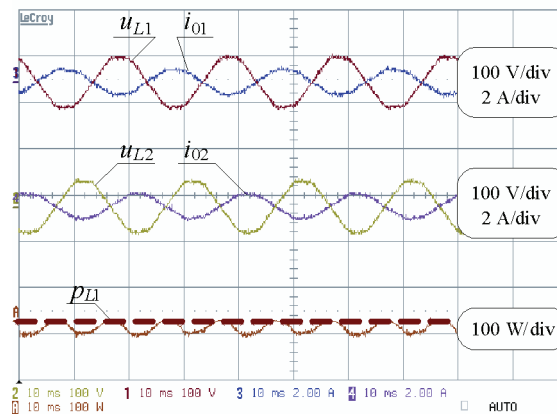


Fig. 19. Experimental waveforms of voltages, currents and power for duty cycle $D=0.1$

As is visible in Figs 19-21, the instantaneous power can be either positive (Fig. 21) or negative (Fig. 19) in value. If the averaged value of instantaneous power p (active power) has a positive value then energy is transferred from source voltage U_S to load voltage U_L , and opposite when p has a negative value. The acquired experimental results validate the theoretical and simulation analysis.

5. Conclusions

In this paper a three phase hybrid transformer using a matrix chopper with unsynchronized active load has been presented. The circuit and operation have been described, and the main characteristics and waveforms have been shown.

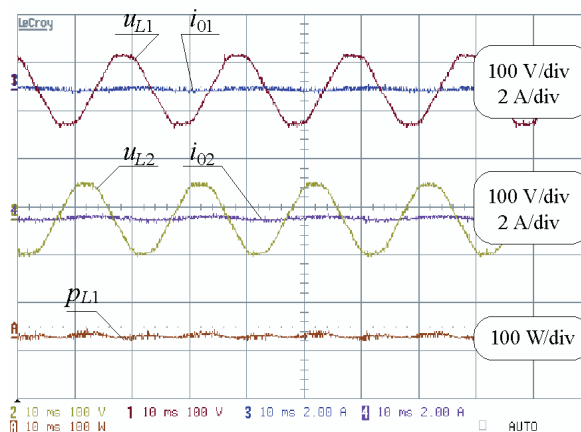


Fig. 20. Experimental waveforms of voltages, currents and power for duty cycle $D = 0.25$

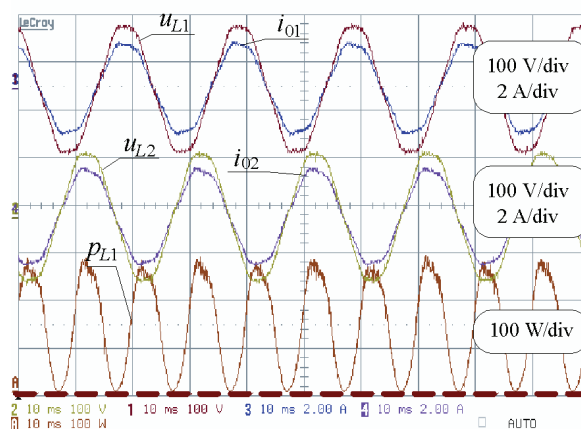


Fig. 21. Experimental waveforms of voltages, currents and power for duty cycle $D = 0.9$

This prototype was operated using a control strategy based on the PWM modulation of the IGBTs. The described solution allows the possibility for bidirectional energy flow in a power system with active load. The acquired experimental results validate theoretical and simulation analysis. Theoretical analysis, in compare to simulation and experimental tests, was based on averaged circuit model (stationary model). The non-stationary simulation model was constructed with bidirectional ideal switches and idealized passive elements. The theoretical, simulation and experimental test results are consistent. Future research will be focused on the analysis of the HT with an active load and closed-control loop and possibility to control energy transfer in low voltage power systems under conditions of source and load voltage fluctuations.

Acknowledgement

The project has been funded by the National Science Centre granted on the basis of decision number DEC-2011/03/B/ST8/06214

References

- [1] Standard EN 50160, Voltage Characteristics of Public Distribution Systems.
- [2] Conrad, L., Little, K., Grigg, C., *Predicting and preventing problems associated with remote fault – clearing voltage dips*. IEEE Trans. on Ind. Applications 27(1): 167-172 (1991).
- [3] Milanović J., Hiskansen I., *Effect of load dynamics on power system damping*. IEEE Trans. on Power System 10(2): 1022-1028 (1995).
- [4] Djokic Z., Desment J., Vanalme G. et al., *Sensitivity of personal computer to voltage sags and short interruptions* IEEE Trans. on Power Delivery 20(1): 375-383 (2005).
- [5] Bollen M., Zang L., *Analysis of voltage tolerance of ac adjustable – speed drives for three phase balanced and unbalanced sags*. IEEE Trans. on Ind. Applications 36(3): 904-910 (2000).
- [6] Falce A., Matas G., Da Silva Y., *Voltage sag analysis and solution for an industrial plant with embedded induction motors*. Proc. Ind. Applications Conference 4: 2573-2578 (2004).
- [7] Honrubia-Escribano A., Gómez-Lázaro E., Molina-García A., Fuentes J.A., *Influence of voltage dips on industrial equipment: Analysis and assessment*. Elsevier, Electrical Power and Energy Systems 41: 87-95 (2012).
- [8] Strzelecki R., Benysek G., Jarnut M., *Energy balancing system for end-user customers*. Electrical Review 84: 17-19 (2008).
- [9] Strzelecki R., Benysek G., Jarnut, M., *Power Quality Conditioners with Minimum Number of Current Sensors Requirement*, Electrical Review 84: 295-298 (2008).
- [10] Jang D., Choe G., *Step-up/down ac voltage regulator using transformer with tap changer and PWM ac chopper*. IEEE Trans. on Ind. Electronics 45(6): 905-911 (1998).
- [11] Fedyczak Z., Frąckowiak L., Jankowski M., Kempski A., *Single – phase serial ac voltage controller based on bipolar PWM ac matrix – reactance chopper*. Proc. 11th European Conference on Power Electronics and Applications, Dresden (2005).
- [12] Aeloiza E., Enjeti P., Moran L., Pite I., *Next generation distribution transformer: to address power quality for critical loads*. Proc. PESC'03, IEEE 3: 1266-1271 (2003).
- [13] Kaniewski J., *Single phase hybrid transformer using matrix converter* (in Polish). Electrotechnical News, pp: 46-48 (2006).
- [14] Fedyczak Z., Kaniewski J., *Single phase hybrid transformer using bipolar matrix – reactance chopper*. (In Polish), Electrical Review, pp: 80-85 (2006).
- [15] Fedyczak Z., Kaniewski J., *Modeling and analysis of hybrid transformer using matrix converter*. Proc. CPE Conf., Gdańsk (2007).
- [16] Kaniewski J., *Analysis and study of properties of the hybrid transformers*. Ph.D. dissertation, University of Zielona Góra Press. (In Polish) (2011).
- [17] Kaniewski, J., *Practical application of series active compensators*. [In:] Benysek G., Pasko M. (Ed.), *Power theories for improved power quality*. Springer, pp.: 187-210 (2012).
- [18] Kaniewski J., *Modeling and analysis of three-phase hybrid transformer using buck-boost MRC*. Proc. 7th international conference-workshop Compatibility and Power Electronics – CPE 2011, Tallinn, Estonia, 202-207 (2011).
- [19] Kaniewski, J., Fedyczak, Z., Benysek, G., *AC voltage sag/swell compensator based on three-phase hybrid transformer with buck-boost matrix-reactance chopper*. IEEE Trans. on Ind. Electronics, manuscript accepted for publication, September 19, (2013).
- [20] Jeziński, E., *Transformers – Theoretical Fundamentals*. (In Polish), WNT Warszawa (1965).
- [21] Fedyczak Z., *PWM AC voltage transforming circuits*. (In Polish) University of Zielona Góra Press (2003).
- [22] Kaniewski, J., Fedyczak, Z., Klytta et al., *Implementation of a three-phase hybrid transformer using a matrix chopper*. Proc. 13th European Conference on Power Electronics and Applications, Barcelona, Hiszpania (2009).