TiNi SHAPE MEMORY ALLOY TENSION AT VARIOUS TEMPERATURES – INFRARED IMAGING OF SHAPE MEMORY EFFECT AND PSEUDOELASTICITY

SUMMARY

The mechanical characteristics and the infrared imaging of stress-induced martensite transformation developing in TiNi shape memory alloy (SMA) subjected to tension in various conditions with respect to the SMA austenite finish parameter have been presented. Based on the mechanical curves and their related temperature changes it was found that onset of the martensitic transformation appears at the end of the elastic part of the stress-strain curve, since the temperature starts to increase before the knee in the curve. The uniform temperature distribution observed on the specimen surface at this stage confirms that the initial martensite transformation is macroscopically homogeneous. For the shape memory effect behavior the uniform temperature distribution on the specimen surface was observed during the complete process of the SMA loading which means that the transformation process is macroscopically homogeneous. For the shape memory alloy pseudoelasticity behavior bands of higher temperature have been recorded during the specimen loading and bands of lower temperature during its unloading, manifesting localized Lüders-like deformation, caused by the transformation process. As the transformation advances, the higher temperature changes have been recorded. Taking advantages from the infrared technique a new results concerning nucleation and development of the martensite forward and reverse transformation have been obtained. Finally, some examples of the SMA new applications due to the SMA shape memory effect have been presented and discussed.

Keywords: shape memory alloy, TiNi, martensite transformation, shape memory effect, pseudoelasticity

1. INTRODUCTION TO SHAPE MEMORY ALLOYS

The development of intelligent or smart materials and their systems is highly anticipated since they have various functions, such as sensing, working and crack-healing by themselves, etc. In the field of intelligent materials, the development of shape memory alloy has attracted high attention since the unique properties of the shape memory effect (SME) and superelasticity (SE) appears (Tobushi, 2009). If we use the SME and SE in practical applications, not only large recovery strain but also high recovery stress, energy storage and energy dissipation can be obtained. Successful applications of shape memory effect are couplings, actuators in electric appliances, automobile devices, robots and smart materials, e.g. composites with polymer or metal matrix. Pseudoelasticity and high elasticity are applied to orthodontic arch wire, antennas for cellular phones, guide wires for catheters, medical instruments, orthopedic devices, etc. (Shaw 1997, Dutkiewicz 2008, Tobushi 2009).

The shape memory alloy deformation behavior under various conditions is related to many practical applications, and is summarized graphically by the three-dimensional stress-strain-temperature diagram in Figure 1.
In the Figure 1, $A_s$ and $A_f$ denote the austenite start and finish temperatures, respectively. In the yield stage of the stress-strain diagram shown in the $\sigma$-$\varepsilon$ plane, the deformation accompanied by the stress plateau appears due to the martensitic transformation. This phenomenon is called the stress-induced martensitic transformation. The strain induced at a temperature below $A_s$, recovers between $A_s$ and $A_f$ after the applied stress has been removed and the specimen heated, as seen in the $\varepsilon$-$T$ plane, showing the shape memory effect (Figs 3, 4). At a temperature above $A_f$, the martensite transformation is developing, leading to the usual superelastic loop with upper and lower plateaus (Figs 5, 7, 8).

The main features of the SME and SE are induced due to the twinning, martensitic transformation and the martensite variants reorientation. Since the shape memory alloys are very sensitive to the temperature change, effects of thermo-mechanical couplings related to the stress-induced martensite transformation responsible for their behavior and related to many effective applications can be studied on the basis of the obtained mechanical and temperature characteristics.

2. MATERIAL AND EXPERIMENTAL PROCEDURE

The experiments have been carried out on two kinds of TiNi shape memory alloy belt specimens of $160 \times 10 \times 0.4$ mm, cut from strips; characterized by the $A_f$ temperature equal to 333 K and 283 K, respectively. The specimens have been subjected to the strain-controlled tension test on the Instron testing machine in quasi-static range of strain rates. In the course of the investigation both the mechanical characteristics and the distribution of the infrared radiation emitted by the specimen surface were registered continuously. The diagram of the experimental equipment is presented in Figure 2. The infrared camera used is a long wave type, working in the wave range of 7.5–13 $\mu$m. The matrix size is $320 \times 240$ pixels. The spatial and the temperature resolutions depend on the camera-specimen distance. In the case of the results presented here, the distance was 10 cm and the spatial resolution was 0.3 mm. Before the testing, the specimen surface was covered with a very thin layer of a carbon powder in order to make its emissivity higher and more homogeneous. The specimen mean temperature was calculated over an area of $8 \times 60$ mm, located in the central part of the specimen. The obtained stress-strain characteristics, the specimen temperature distribution and the mean temperature changes enable the study of the process of nucleation and the further development of the martensitic forward and reverse transformation, which are responsible for the shape memory alloy thermomechanical behavior. The latter is important in the SMA number of emerging practical applications.
The mean temperature, calculated from the specimen surface, is usually used in the presented curves and thermomechanical coupling analysis (Fig. 7). The measurement temperature accuracy obtained for the used infrared camera was approximately 0.2 K.

3. INFRARED IMAGING OF STRESS-INDUCED TRANSFORMATION

Investigations of the temperature variations accompanying the martensite transformation processes in shape memory alloys by infrared camera have been launched quite recently (Shaw 1997). At first, the temperature was estimated using a thermocouple, which, however, was limited to the measurement at a single chosen point. A modern infrared camera is very useful in the investigations, since it allows for monitoring of the temperature distribution on the examined specimen surface and the calculation of the mean temperature in a contact-less way over arbitrarily chosen area, segment or a number of points The stress-induced martensitic transformation manifests an exothermic character, while the reverse shows endothermic transformation, so during loading the SMA temperature increases and during unloading the temperature decreases (Show 1997, Gadaj 2002, Pieczyska 2004, 2006).

The measured temperature changes depend on the strain rate; the higher the strain rate, the higher the temperature change. The recorded maximal temperature increments were of about 4K for the strain rate $10^{-4}$ s$^{-1}$ to about 40 K for $10^{-1}$s$^{-1}$ (Pieczyska 2008). During the SMA loading process, the recorded temperature distribution was more or less uniform. It means that the process of the phase transformation, analyzed in macro-scale, was more or less homogeneous (Brinson 2004, Favier 2007, Pieczyska 2004, 2008, 2010, He 2010).

Depending on the test temperature in reference to the SMA austenite finish ($A_f$) and austenite start ($A_s$) temperature parameters, the recorded temperature distribution is more or less uniform. The stress-strain curves and the specimen temperature distributions obtained during tension of the TiNi SMA at the temperature below, at and above $A_f$ are shown in Figures 3–5, 7 and 8.

3.1. Infrared imaging of the shape memory effect

Figure 3 presents the stress-strain curve and the specimen temperature distributions obtained during tension of the TiNi SMA ($A_s=320$ K, $A_f=333$ K) performed at 295 K (below the SMA austenite start temperature, i.e. registering shape memory effect. The images presented on the right show the specimen temperature distribution recorded at the strains equal to 0.1%, 2%, 3% during loading; and 2.9% during unloading, respectively.

From the Figure 3 one can observe that the specimen temperature increases during the SMA loading and decreases

![Fig. 3. Stress-strain curve and temperature distribution on the surface of TiNi SMA tape obtained at various strains under strain rate of $1.87\times10^{-3}$ s$^{-1}$ during loading and unloading at $T < A_f$ studied by infrared thermography](image)

![Fig. 4. Stress-strain curve and temperature distribution on the surface of TiNi SMA tape at various strains under strain rate of $1.87\times10^{-3}$ s$^{-1}$ during loading and unloading at $T = A_f$ studied by infrared thermography](image)
during the unloading but that the recorded temperature distribution is uniform, i.e. the transformation process observed in macro-scale by the applied infrared equipment is homogeneous. After unloading, a great residual strain \( \approx \frac{3}{25} \) called also the shape memory effect was recorded. The specimen recovers its former size and shape during its subsequent heating at the temperature between 320 K and 333 K.

The stress-strain curve and the temperature distribution accompanying the SMA tension performed at \( T = A_f \) (333 K) with the strain rate equal to \( 1.87 \times 10^{-3} \text{ s}^{-1} \) is presented in Figure 4.

Looking at the Figure one can notice that the temperature distribution of the SMA loading by tension at \( T = A_f \) is not uniform, especially during the loading, manifesting that the martensite transformation process is not homogeneous. Namely, bands of the new phase, related to the higher temperatures, nucleate at various positions and grow wider thereafter on the whole specimen surface.

Moreover, one should also take into account that the results presented in Figures 3 and 4 were obtained for the similar specimen of the shape memory alloy during tension carried out with the same strain rate \( 1.87 \times 10^{-3} \text{ s}^{-1} \), however in Figure 3 the specimen was subjected to tension in the strain range of about \( 4\% \), while in Figure 4 twice higher strain range, approximately \( 8\% \), was applied.

### 3.2. Infrared imaging of the shape memory alloy pseudoelastic behavior

For the TiNi SMA characterized by \( A_f = 283 \text{ K} \) and loading by tension in room conditions (295 K) the temperature imaging is much more complex (Figs 5, 8), reflecting the much more complex transformation process. The results, presented in Figure 5, were obtained for the tension carried out with higher strain rate equal to \( 1.6 \times 10^{-2} \text{ s}^{-1} \) and within the strain range approximately \( 6\% \). For the test, a superelastic (pseudoelastic) behavior was recorded and much higher stresses over 500 MPa have been achieved in the range of the martensite forward transformation in comparison to the formerly obtained results: 150–260 MPa (Figs 3 and 4). After the unloading, only a small residual strain has been recorded (Fig. 5, left). Moreover, one can observe a localized Lüders-like deformation developing in the SMA specimen. The temperature distribution recorded on the specimen surface reflects immediately a nucleation and development of the new phases, both martensite and reverse, due to the temperature changes and significant temperature variations between the parent and the new phase. Namely, bands of significantly higher temperature, corresponding to the exothermic inhomogeneous martensite forward transformation, started from the grip area were recorded during the SMA loading, whereas bands of significantly lower temperature, corresponding to the endothermic reverse transformation, were recorded during the unloading process. It was observed that in the case of high strain rate, the transformation bands nucleate not only at the ends or center, but also at various positions and develop thereafter on the whole surface of the specimen (Pieczyska 2008, 2010, He 2010).

Sometimes the nucleation and growth of the transformation bands are so clear and significant that they can be observed directly on the surface of the specimen with the naked eye (Fig. 6). Such effects were obtained with the test for which stress-strain curve and infrared imaging are presented in Figure 5.

![Fig. 5. Stress-strain curve and temperature distribution on surface of TiNi SMA specimen at various strains under a strain rate of \( 1.6 \times 10^{-2} \text{ s}^{-1} \) during loading and unloading at \( T > A_f \) studied by infrared thermography](image)

![Fig. 6. Deformation patterns on TiNi SMA specimen surface due to phase transformations in tension test under strain rate = \( 1.6 \times 10^{-2} \text{ s}^{-1} \)](image)
Stress-strain and temperature-strain curves obtained during TiNi SMA pseudoelastic behavior with strain rate $10^{-2} \text{s}^{-1}$ is shown in Figure 7.

![Fig. 7. Stress- and temperature-strain curves obtained for TiNi tension test performed with strain rate $10^{-2} \text{s}^{-1}$](image)

Looking at the mechanical and the temperature graphs obtained for the strain rate $10^{-2} \text{s}^{-1}$ and for the strain range 8% presented in Figure 7 one can conclude that the martensite transformation during the loading processes is almost completed. Moreover, one can find from the presented data that the martensite transformation starts when the onset in temperature is recorded and the transformation is developed until the temperature does not increase (during the latest loading stage).

The temperature distributions on the specimen surface (thermograms) obtained during the test were overlapped on the stress- and the temperature-strain diagram and presented in Figure 8, (Pieczyska, 2008).

One can notice that transformation bands of significantly higher temperature are corresponding to the exothermic in-homogeneous martensitic forward transformation recorded during the SMA loading (thermograms 1–5), whereas bands of significantly lower temperature, corresponding to the endothermic reverse transformation, were recorded during the specimen unloading (thermograms 6–8). As the tension proceeds the band widens significantly and other bands appear, at first parallel and then inclined at the same angle but developing in the opposite direction (Pieczyska 2006). As the strain increases, more and more transformation bands appear and move towards the specimen grip. When the bands reach the grips area (Fig. 8, thermogram 4), the upswing region on both the stress- and the temperature-strain curves are observed, reflecting the more advanced stage of the transformation process. The stress and the temperature increase fast, however the temperature distribution becomes more uniform at more advanced transformation stage (5), so the transformation process seems to be more homogeneous, probably due to the transferring heat overlapping effects.

During the unloading, after passing the elastic stage (Fig. 8, thermogram 6), the reverse transition takes place. After the unloading is completed, the material almost returns to its parent austenite phase. However, the temperature drops below its initial value and the residual strains, related to a small amount of the martensitic and irreversible macro-structural changes appear, depending on the specimen history (Brinson 2004, Pieczyska 2006, Favier 2007).

The phenomena of localized Lüders-like transformations accompanying the complete loop of the TiNi SMA pseudoelasticity behavior analyzed in infrared technique have been confirmed by (Murusawa 2004, Daly 2007) by using a Digital Image Correlation (DIC) Strain Map technique.

4. NEW APPLICATIONS OF SMA SHAPE MEMORY EFFECT AND SUPERELASTICITY

Due to unique properties of shape memory alloys manifested in various conditions many projects are still developing for daily life, medicine and technology practical applications.

4.1. Solar vehicle and engine based on SMA shape memory effect

A photograph of a solar-powered car driven by a simple-pulley TiNi SMA heat engine is shown in Figure 9.

The SMA heat engine is driven by the sun light using a Fresnel lens. In the SMA heat engine, two pulleys are connected by the SMA belt which is shape-memorized into the flat plane by the heat treatment before making into a loop by welding. The car moves based on the recovery force in the SMA belt which appears by heating from the sun light focused by the Fresnel lens. From a view-point of global warming prevention, being able to use the low-temperature thermal energy around 373 K, the development of the compact and harmless clean SMA heat engine is greatly anticipated.
4.2. Shape memory alloy new engine

A design of a new shape memory alloy engine proposed by the Aichi Institute of Technology students is shown in Figure 10.

![Fig. 10. Photograph of design of SMA engine using a SME and driven by a hot water; AIT](image)

The springs made from TiNi SMA are in martensite state in room conditions. When the engine is partly put into a hot water, above the SMA $A_F$ temperature, those SMA springs which are immersed in the hot water are suddenly shrinking, and the device starts to rotate.

5. CONCLUSIONS

The mechanical characteristics, the temperature changes and the infrared imaging of stress-induced martensite transformation occurring in TiNi SMA subjected to tension in various conditions with respect to the alloy austenite finish temperature have been presented. Based on the mechanical curves and their related temperature changes it was found that an onset of the martensitic transformation appears at the end of the elastic part of the stress-strain curve, since the temperature starts increase before the knee in the curve. The uniform temperature distribution observed on the specimen surface at this stage confirms that the initial martensite transformation is macroscopically homogeneous. At higher strains, for the shape memory alloy pseudoelastic behavior, bands of higher temperature are observed during the specimen loading and bands of lower temperature during its unloading, manifesting localized Lüders-like transformation. When the transformation bands reach the grips area during the loading, an upswing effects on both the stress-strain and the temperature-strain curves are observed, reflecting the intense process of the advanced martensite transformation. For the shape memory effect behavior the uniform temperature distribution on the specimen surface is observed till the end of the loading which means that the transformation process is macroscopily homogeneous. Using a modern, sensitive and fast infrared camera enables to obtain new results of the nucleation and development of the martensite forward and reverse transformations. Due to unique properties of shape memory alloys manifested in various conditions, many practical applications are still developing, for daily life, medicine and technology.

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