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Measurement of complex resistance parameters by the method of coordinate system displacement on current

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Abstract

Possibility of complex resistance parameter measurement within a frequency range by the method of coordinate system displacement on current components is investigated.

Keywords: complex resistance parameter, measurement, calibration, algorithmic methods.

Pomiary parametrów składowych impedancji metodą przesunięcia systemu współrzędnych według prądu

Streszczenie

W pracy zbadano możliwości pomiaru parametrów impedancji metodą przesunięcia systemu współrzędnych według prądu w wybranym zakresie częstotliwości.

Słowa kluczowe: parametry impedancji, mierniki, wzorcowanie, metody algorytmiczne.

1. Introduction

The necessity of complex resistance parameter determination within a frequency range arises in many areas of science and technique. The components of complex resistances frequently comply with the particular quality characteristics of a research object, therefore their measurement accuracy is a topical task.

The analysis of previous development and existing literary sources. The methods of equilibration (compensating or bridge ones [1, 2]) provide high metrological characteristics only on fixed frequencies, as a rule, 1 kHz. Analogous disadvantage is appropriate for means [7], in which the method of phase sensitive detection is realised. The implementation of calculating technique in measuring rings [4, 5, 6, 7, 8] has given new possibilities at complex resistance parameter measurement. The possibility of substitution method employment at RLC-parameter measurement is investigated in [5]. Although the possibility of the presence of aprior information about complex input phase measurer resistance, functioning voltage value measurer and high-precision phase measurer application within a frequency range contract the areas of application and lower potential measurement accuracy.

Objective of research. Accuracy increasing of complex resistance component measurement by the method of coordinate system displacement on current.

2. Measurement scheme on the basis of mathematical correlations

Complex resistance RLC-parameter measurement schemes are synthesized due to the methods of vector value parameter measurement [11, 12, 13] and the Ome's Law on AC (1):

$$\dot{Z} = \frac{\dot{U}}{\dot{I}}; \quad \dot{g} = \frac{\dot{I}}{\dot{U}}. \quad (1)$$

A generalised structural measurement scheme (fig. 1) consists of sinusoid voltage source (SVS), commutator (C), control block (CB), analogue-to-digital converter (ADC) of a functioning voltage value, digital frequency meter (DFM), calculating device (CD), reference active resistances R_{01} , R_{02} , reference complex resistance \dot{Z}_0 .

Voltage falling on resistor R_{01} is proportional to the current value I_1 . Voltage falling on resistor R_{02} is proportional to the current value I_2 . Due to reference complex resistance \dot{Z}_0 (R_0 , $j\omega L_0$, $1/j\omega C_0$), current $i_{x0}=O_1O_2$ or $i_{y0}=O_1O_3$ will flow through \dot{Z}_0 [fig.2]. The values of synphase i_x and quadruple i_y current components in complex resistance \dot{Z} are determined from the

correlation (2) at $R_{01} \ll |\dot{Z}|$

$$i_x = \frac{i_2^2 - i_1^2 - i_{x0}^2}{2i_{x0}}; \quad i_y = \frac{i_2^2 - i_1^2 - i_{y0}^2}{2i_{y0}}. \quad (2)$$

So long as $i_{x0} = \dot{U}_{23}/R_{01}$; $i_{y0} = \dot{U}_{23}/j\omega L_0$; $i_{y0} = j\dot{U}_{23}\omega C_0$, then $g = i_x/U_{23}$, $b = i_y/U_{23}$, or $b = \sqrt{y^2 - g^2}$.

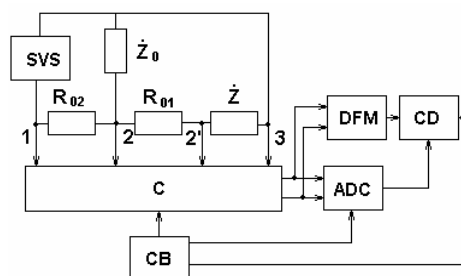


Fig. 1. Generalised structural scheme of complex resistance RLC-parameter measurer by the method of coordinate system displacement on current
Rys. 1. Schemat blokowy do pomiaru parametrów RLC impedancji metodą przesunięcia systemu współrzędnych według prądu

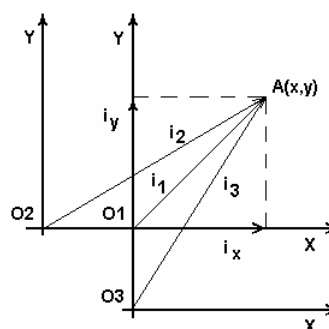


Fig. 2. Coordinate systems at the measurement of synphase and quadruple current components
Rys. 2. System współrzędnych przesunięty według prądu dla pomiarów składowych impedancji

At $R_{01} \approx \left| \dot{Z} \right|$ the considerable methodical error of the determination of g and b . The providing of $R_{01} \ll \left| \dot{Z} \right|$ is not

always practically possible. The disadvantage of $R_{01} \ll \left| \dot{Z} \right|$ condition is the fact that voltage $U_{22'} \ll U_{2'3}$, and it means that a voltmeter will work within different measurement ranges at the determination of $U_{22'}$ and U_{12} , U_{23} and $U_{2'3}$. This disadvantage could be replaced in the following way.

Let us express complex resistance $\dot{Z} = r + jx$ through conductance $Y = \frac{r}{Z^2} - j \frac{x}{Z^2} = g - jb$. The resistance between the points 2 and 3 of right branch $\dot{Z}_1 = \dot{Z} + R_{01} = (r + R_{01}) + jx = r_1 + jx_1$ could be expressed through conductance $\dot{Y}_1 = \frac{r_1}{Z_1^2} - j \frac{x_1}{Z_1^2} = g_1 - jb_1$. The synphase component i_x of current, that flows through the conductance g_1 , is equal to $i_x = \frac{i_2^2 - i_1^2 - i_{R0}^2}{2 i_{R0}}$, where $i_2 = \frac{U_{12}}{R_{02}}$; $i_1 = \frac{U_{22'}}{R_{01}}$; $i_{R0} = \frac{U_{23}}{R_0}$. We can express conductance $g_1 = \frac{i_x}{U_{23}} = \frac{r_1}{Z_1^2}$.

As a result $r_1 = g_1 * Z_1^2$; where $Z_1 = \frac{U_{23}}{i_1}$.

Since the values of resistances R_{01} and R_{02} are known, we can receive the synphase $r = (r_1 - R_{01})$ and a quadruple resistance component $\dot{Z}_x = \sqrt{Z_1^2 - r_1^2}$. At this estimation of r and x the resistance value R_{01} could be commensurable with the module of the complex resistance value \dot{Z} .

To determine the parameters x_1, x_2, x_3 of three-component complex resistances on the two frequencies ω_1 and ω_2 $Re \dot{Z}(\omega_1, x_1, x_2, x_3)$, $Re \dot{Z}(\omega_2, x_1, x_2, x_3)$, $Im \dot{Z}(\omega_1, x_1, x_2, x_3)$ and $Im \dot{Z}(\omega_2, x_1, x_2, x_3)$ are being determined. The solution of equation system [15] (3)

$$\begin{aligned} N_{11} &= Re \dot{Z}(\omega_1, x_1, x_2, x_3) \\ N_{12} &= Im \dot{Z}(\omega_1, x_1, x_2, x_3) \\ N_{21} &= Re \dot{Z}(\omega_2, x_1, x_2, x_3) \\ N_{22} &= Im \dot{Z}(\omega_2, x_1, x_2, x_3) \end{aligned} \quad (3)$$

determines the values x_1, x_2, x_3 .

3. Determination of the RLC-parameters of three-component complex resistances

Due to the principles of the method of coordinate system displacement on current at the measurement of complex resistance parameters, the generalised structural scheme of the measuring ring is being synthesized. In which an object of research as three-component complex resistance ThCR is expressed as \dot{Z} . Due to a configuration scheme, a ThCR mathematical model could be presented as the complex resistance \dot{Z} or the complex

conductance \dot{Y} . If it is easier to describe ThCR mathematically as conductance, then in the consequence of the expression $Y = g - jb$ we immediately receive the resistance expression: $\dot{Z} = r + jx = \frac{g}{Y^2} + j \frac{b}{Y^2}$.

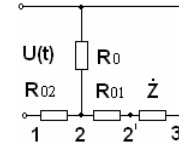


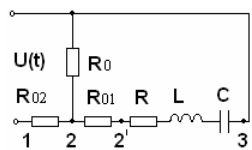
Fig. 3. Generalised scheme of a measuring ring
Rys. 3. Schemat ogólny obwodu pomiarowego

So long as measurement is being conducted on the two frequencies, we receive an equation system according to consequent and parallel RLC-schemes:

$$\begin{aligned} \dot{Z}_1 &= r_1 + jx_1; \\ \dot{Z}_2 &= r_2 + jx_2; \\ \dot{Z}_3 &= (r_1 + R_{01}) + jx_1; \\ \dot{Z}_4 &= (r_2 + R_{01}) + jx_2. \\ \dot{Y}_1 &= g_1 - jb_1; \\ \dot{Y}_2 &= g_2 - jb_2; \\ \dot{Z}_1 &= r_1 + jx_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1^2}; \\ \dot{Z}_2 &= r_2 + jx_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2^2}; \\ \dot{Z}_3 &= (r_1 + R_{01}) + jx_1; \\ \dot{Z}_4 &= (r_2 + R_{01}) + jx_2. \end{aligned}$$

Thus, due to the chosen R_0, f_1, f_2 and the measured voltage values $U_{12}, U_{23}, U_{22'}$, it is possible to determine $Z_1, Z_2, Z_3, Z_4, r_1, r_2, x_1, x_2, Y_1, Y_2, g_1, g_2, b_1$ and b_2 . These values to some extent are sufficient to determine ThCR RLC-parameters of any configuration (table 1). The results of measurement do not depend on the coefficient value of the ADC transmission of alternating voltage into a code. Its stability is required only for the time of RLC-parameter determination.

Tab. 1. Measuring ring scheme and major mathematical correlations
Tab. 1. Schematy pomiarowe i podstawowe zależności matematyczne

Nr	Measuring ring scheme and major mathematical correlations
1	 $\begin{aligned} \dot{Z}_1 &= R + j \left(\omega_1 L - \frac{1}{\omega_1 C} \right) = r_1 + j x_1; \\ \dot{Z}_2 &= R + j \left(\omega_2 L - \frac{1}{\omega_2 C} \right) = r_2 + j x_2; \\ \dot{Z}_3 &= (R + R_{01}) + j \left(\omega_1 L - \frac{1}{\omega_1 C} \right) = (R_{01} + r_1) + j x_1; \\ \dot{Z}_4 &= (R + R_{01}) + j \left(\omega_2 L - \frac{1}{\omega_2 C} \right) = (R_{01} + r_2) + j x_2; \\ C &= \frac{\omega_1^2 - \omega_2^2}{\omega_1 \omega_2 (x_1 \omega_2 - x_2 \omega_1)}; L = \frac{x_2 \omega_2 - x_1 \omega_1}{\omega_2^2 - \omega_1^2}; R = \sqrt{Z_1^2 - X_1^2}; \end{aligned}$

2

$\dot{Y}_1 = \frac{1}{R} - j\left(\frac{1}{\omega_1 L} - \omega_1 C\right) = g_1 - j b_1;$
 $\dot{Y}_2 = \frac{1}{R} - j\left(\frac{1}{\omega_2 L} - \omega_2 C\right) = g_2 - j b_2;$
 $\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1^2}; \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$
 $\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2^2}; \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$
 $R = r_1 Y_1^2;$
 $C = \frac{b_1 \omega_1 - b_2 \omega_2}{\omega_2^2 - \omega_1^2}; L = \frac{\omega_1^2 - \omega_2^2}{\omega_1 \omega_2 (b_1 \omega_2 - b_2 \omega_1)}$

3

$\dot{Z}_1 = R + j\left(\frac{\omega_1 L}{1 - \omega_1^2 L C}\right) = r_1 + j x_1;$
 $\dot{Z}_2 = R + j\left(\frac{\omega_2 L}{1 - \omega_2^2 L C}\right) = r_2 + j x_2;$
 $\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$
 $C = \frac{x_2 \omega_1 - x_1 \omega_2}{x_1 x_2 (\omega_2^2 - \omega_1^2)}; L = \frac{x_1 x_2 (\omega_2^2 - \omega_1^2)}{\omega_1 \omega_2 (x_2 \omega_2 - x_1 \omega_1)};$
 $R = \sqrt{Z_J^2 - X_J^2}$

4

$\dot{Z}_1 = \frac{R}{1 + \omega_1^2 C^2 R^2} + j\left(\omega_1 L - \frac{R^2 \omega_1 C}{1 + \omega_1^2 C^2 R^2}\right) = r_1 + j x_1;$
 $\dot{Z}_2 = \frac{R}{1 + \omega_2^2 C^2 R^2} + j\left(\omega_2 L - \frac{R^2 \omega_2 C}{1 + \omega_2^2 C^2 R^2}\right) = r_2 + j x_2;$
 $\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$
 $C = \frac{1}{\omega_1 R} \sqrt{\frac{R - r_1}{r_1}}; L = \frac{x_1 + r_1 R \omega_1 C}{\omega_1};$
 $R = \frac{r_1 r_2 (\omega_2^2 - \omega_1^2)}{(r_2 \omega_2^2 - r_1 \omega_1^2)}$

5

$\dot{Z}_1 = \frac{R \omega_1^2 L^2}{R^2 + \omega_1^2 L^2} + j\left[\frac{R^2 \omega_1 L}{R^2 + \omega_1^2 L^2} - \frac{1}{\omega_1 C}\right] = r_1 + j x_1;$
 $\dot{Z}_2 = \frac{R \omega_2^2 L^2}{R^2 + \omega_2^2 L^2} + j\left[\frac{R^2 \omega_2 L}{R^2 + \omega_2^2 L^2} - \frac{1}{\omega_2 C}\right] = r_2 + j x_2;$
 $\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$
 $L = \frac{R}{\omega_1} \sqrt{\frac{r_1}{R - r_1}}; C = \frac{1}{\frac{r_1 R}{L} - \omega_1 x_1}; R = \frac{r_1 r_2 (\omega_2^2 - \omega_1^2)}{(r_1 \omega_2^2 - r_2 \omega_1^2)}$

6

$\dot{Y}_1 = \frac{1}{R} - j\left(\frac{1}{\omega_1 L} - \frac{1}{\omega_1 C}\right) = g_1 - j b_1;$
 $\dot{Y}_2 = \frac{1}{R} - j\left(\frac{1}{\omega_2 L} - \frac{1}{\omega_2 C}\right) = g_2 - j b_2;$
 $\dot{Z}_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1^2} = r_1 + j x_1; \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$
 $\dot{Z}_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2^2} = r_2 + j x_2; \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$
 $R = \frac{1}{r_1 Y_1^2}; L = \frac{b_1 \omega_2 - b_2 \omega_1}{b_1 b_2 (\omega_2^2 - \omega_1^2)}; C = \frac{b_1 b_2 (\omega_2^2 - \omega_1^2)}{\omega_1 \omega_2 (b_1 \omega_1 - b_2 \omega_2)};$

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$\dot{Y}_1 = \frac{R}{R^2 + \omega_1^2 L^2} + j\left[\frac{\omega_1 L}{R^2 + \omega_1^2 L^2} - \omega_1 C\right] = g_1 - j b_1;$
 $\dot{Y}_2 = \frac{R}{R^2 + \omega_2^2 L^2} + j\left[\frac{\omega_2 L}{R^2 + \omega_2^2 L^2} - \omega_2 C\right] = g_2 - j b_2;$
 $\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1^2}; \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$
 $\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2^2}; \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$
 $R = \frac{g_2 \omega_2^2 - g_1 \omega_1^2}{g_1 g_2 (\omega_2^2 - \omega_1^2)}; L = \frac{1}{\omega_1} \sqrt{\frac{R - g_1 R^2}{g_1}}; C = \frac{b_1 + \frac{g_1 \omega_1 L}{R}}{\omega_1};$

8

$$\dot{Y}_1 = \frac{R \omega_1^2 C^2}{1 + \omega_1^2 C^2 R^2} - j \left[\frac{1}{\omega_1 L} - \frac{\omega_1 C}{1 + \omega_1^2 C^2 R^2} \right] = g_1 - j b_1;$$

$$\dot{Y}_2 = \frac{R \omega_2^2 C^2}{1 + \omega_2^2 C^2 R^2} - j \left[\frac{1}{\omega_2 L} - \frac{\omega_2 C}{1 + \omega_2^2 C^2 R^2} \right] = g_2 - j b_2;$$

$$\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1^2}; \quad \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$$

$$\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2^2}; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$$

$$R = \frac{g_1 \omega_2^2 - g_2 \omega_1^2}{g_1 g_2 (\omega_2^2 - \omega_1^2)}; \quad L = \frac{1}{\frac{g_1}{R C} + b_1 \omega_1}; \quad C = \frac{1}{\omega_1 \sqrt{R - g_1 R^2}}$$

9

$$\dot{Z}_1 = \left[R_1 + \frac{R_2 \omega_1^2 L^2}{R_2^2 + \omega_1^2 L^2} \right] + j \frac{R_2 \omega_1 L}{R_2^2 + \omega_1^2 L^2} = r_1 + j x_1;$$

$$\dot{Z}_2 = \left[R_1 + \frac{R_2 \omega_2^2 L^2}{R_2^2 + \omega_2^2 L^2} \right] + j \frac{R_2 \omega_2 L}{R_2^2 + \omega_2^2 L^2} = r_2 + j x_2;$$

$$\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$$

$$L = \frac{x_1 x_2 (\omega_2^2 - \omega_1^2)}{\omega_1 \omega_2 (x_2 \omega_2 - x_1 \omega_1)};$$

$$R_2 = \omega_1 L \sqrt{\frac{x_1}{\omega_1 L - x_1}}; \quad R_1 = r_1 - \frac{x_1 \omega_1 L}{R_2}$$

10

$$\dot{Z}_1 = \left[R_1 + \frac{R_2}{1 + R_2^2 \omega_1^2 C^2} \right] - j \frac{R_2^2 \omega_1 C}{1 + R_2^2 \omega_1^2 C^2} = r_1 + j x_1;$$

$$\dot{Z}_2 = \left[R_1 + \frac{R_2}{1 + R_2^2 \omega_2^2 C^2} \right] - j \frac{R_2^2 \omega_2 C}{1 + R_2^2 \omega_2^2 C^2} = r_2 + j x_2;$$

$$\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$$

$$C = \frac{x_1 \omega_2 - x_2 \omega_1}{x_1 x_2 (\omega_2^2 - \omega_1^2)};$$

$$R_2 = \sqrt{\frac{x_1}{\omega_1 C (1 - x_1 \omega_1 C)}}; \quad R_1 = r_1 - \frac{x_1}{R_2 \omega_1 C}$$

11

$$\dot{Z}_1 = \frac{R \omega_1^2 L_2^2}{R^2 + \omega_1^2 L_2^2} + j \left[\frac{R^2 \omega_1 L_2}{R^2 + \omega_1^2 L_2^2} + \omega_1 L_1 \right] = r_1 + j x_1;$$

$$\dot{Z}_2 = \frac{R \omega_2^2 L_2^2}{R^2 + \omega_2^2 L_2^2} + j \left[\frac{R^2 \omega_2 L_2}{R^2 + \omega_2^2 L_2^2} + \omega_2 L_1 \right] = r_2 + j x_2;$$

$$\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$$

$$R = \frac{r_1 r_2 (\omega_2^2 - \omega_1^2)}{r_1 \omega_2^2 - r_2 \omega_1^2}; \quad L_2 = \frac{R}{\omega_1 \sqrt{R - r_1}}; \quad L_1 = \frac{x_1 - \frac{r_1 R}{\omega_1 L_2}}{\omega_1}$$

12

$$\dot{Z}_1 = \frac{R}{1 + R^2 \omega_1^2 C_2^2} - j \left[\frac{R^2 \omega_1 C_2}{1 + R^2 \omega_1^2 C_2^2} + \frac{1}{\omega_1 C_1} \right] = r_1 + j x_1;$$

$$\dot{Z}_2 = \frac{R}{1 + R^2 \omega_2^2 C_2^2} - j \left[\frac{R^2 \omega_2 C_2}{1 + R^2 \omega_2^2 C_2^2} + \frac{1}{\omega_2 C_1} \right] = r_2 + j x_2;$$

$$\dot{Z}_3 = (r_1 + R_{01}) + j x_1; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$$

$$C_2 = \frac{1}{R \omega_1 \sqrt{\frac{R - r_1}{r_1}}}; \quad C_1 = \frac{1}{\omega_1 (x_1 - r_1 R \omega_1 C_2)}$$

$$R = \frac{r_1 r_2 (\omega_2^2 - \omega_1^2)}{r_2 \omega_2^2 - r_1 \omega_1^2}$$

13

$$\dot{Y}_1 = \left[\frac{1}{R_2} + \frac{R_1}{R_1^2 + \omega_1^2 L^2} \right] - j \frac{\omega_1 L}{R_1^2 + \omega_1^2 L^2} = g_1 - j b_1;$$

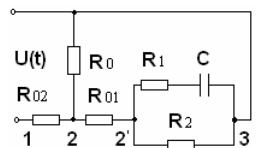
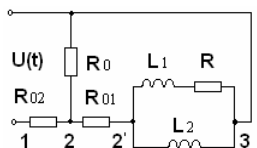
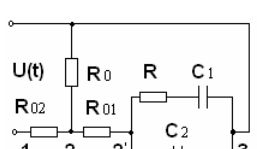
$$\dot{Y}_2 = \left[\frac{1}{R_2} + \frac{R_1}{R_1^2 + \omega_2^2 L^2} \right] - j \frac{\omega_2 L}{R_1^2 + \omega_2^2 L^2} = g_2 - j b_2;$$

$$\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1^2}; \quad \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$$

$$\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2^2}; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$$

$$L = \frac{b_1 \omega_2 - b_2 \omega_1}{b_1 b_2 (\omega_2^2 - \omega_1^2)}; \quad R_2 = \frac{1}{g_1 - \frac{b_1 R_1}{L \omega_1}};$$

$$R_1 = \sqrt{\frac{\omega_1 L (1 - b_1 \omega_1 L)}{b_1}}$$

14	 $\dot{Y}_1 = \left[\frac{1}{R_2} + \frac{R_1 \omega_1^2 C^2}{1 + R_1^2 \omega_1^2 C^2} \right] - j \frac{\omega_1 C}{1 + R_1^2 \omega_1^2 C^2} = g_1 - j b_1;$ $\dot{Y}_2 = \left[\frac{1}{R_2} + \frac{R_1 \omega_2^2 C^2}{1 + R_1^2 \omega_2^2 C^2} \right] - j \frac{\omega_2 C}{1 + R_1^2 \omega_2^2 C^2} = g_2 - j b_2;$ $\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1}; \quad \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$ $\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2}; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$ $C = \frac{b_1 b_2 (\omega_2^2 - \omega_1^2)}{\omega_1 \omega_2 (b_2 \omega_2 - b_1 \omega_1)};$ $R_1 = \frac{1}{C \omega_1} \sqrt{\frac{C \omega_1 - b_1}{b_1}}; \quad R_2 = \frac{1}{(g_1 - b_1 R_1 \omega_1 C)}$
15	 $\dot{Y}_1 = \frac{R}{R^2 + \omega_1^2 L_1^2} - j \left[\frac{\omega_1 L_1}{R^2 + \omega_1^2 L_1^2} + \frac{1}{\omega_1 L_2} \right] = g_1 - j b_1;$ $\dot{Y}_2 = \frac{R}{R^2 + \omega_2^2 L_1^2} - j \left[\frac{\omega_2 L_1}{R^2 + \omega_2^2 L_1^2} + \frac{1}{\omega_2 L_2} \right] = g_2 - j b_2;$ $\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1}; \quad \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$ $\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2}; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$ $R = \frac{g_2 \omega_2^2 - g_1 \omega_1^2}{g_1 g_2 (\omega_2^2 - \omega_1^2)}; \quad L_2 = \frac{1}{\omega_1 \left(b_1 - \frac{g_1 \omega_1 L_1}{R} \right)}; \quad L_1 = \sqrt{\frac{R - g_1 R^2}{g_1 \omega_1^2}};$
16	 $\dot{Y}_1 = \frac{R \omega_1^2 C_1^2}{1 + R^2 \omega_1^2 C_1^2} - j \left[\frac{\omega_1 C_1}{1 + R^2 \omega_1^2 C_1^2} + \omega_1 C_2 \right] = g_1 - j b_1;$ $\dot{Y}_2 = \frac{R \omega_2^2 C_1^2}{1 + R^2 \omega_2^2 C_1^2} - j \left[\frac{\omega_2 C_1}{1 + R^2 \omega_2^2 C_1^2} + \omega_2 C_2 \right] = g_2 - j b_2;$ $\dot{Z}_1 = r_1 + j x_1 = \frac{g_1}{Y_1^2} + j \frac{b_1}{Y_1}; \quad \dot{Z}_3 = (r_1 + R_{01}) + j x_1;$ $\dot{Z}_2 = r_2 + j x_2 = \frac{g_2}{Y_2^2} + j \frac{b_2}{Y_2}; \quad \dot{Z}_4 = (r_2 + R_{01}) + j x_2;$ $C_1 = \frac{1}{\omega_1} \sqrt{\frac{g_1}{R - g_1 R^2}}; \quad C_2 = \frac{b_1 - \frac{g_1}{R \omega_1 C_1}}{\omega_1}; \quad R = \frac{g_1 \omega_2^2 - g_2 \omega_1^2}{g_1 g_2 (\omega_2^2 - \omega_1^2)}$

4. Conclusions

The results of RLC-parameter measurement by the method of coordinate system displacement on current are independent of an ADC transmission coefficient value that is especially important at measurement conduction within the range of frequencies. A RLC-parameter measurement error to a great extent is determined from the correlation of g and b and commensurability of $1/R_0$ and g , as well as ωC_0 and b along with ADC decimal gradation. At the absence of aprior information about values g i b it is expediently to conduct test measurement on purpose to specify the values $1/R_0$ and ωC_0 . At the considerable difference of g and b it is needed to change frequency ω at which $g \approx b$.

5. References

- [1] Grynevych F.B. Avtomaticheskiye mosty peremennogo toka. Novosibirsk, 1964.
- [2] Kneller V.J. Avtomaticheskiye izmereniya sostavliayushchih kompleksnyh soprotivleniy. - M.; L.; Energiya, 1967.
- [3] Kneller V.J., Borovskiyh P.P. Opredeleniye parametrov mnogoelementnyh dvuhpolyusnykov. - M.: Energoizdat, 1986.
- [4] Dobrovinskiy I.R., Lomtev E.A. Proektirovaniye YYC dlya izmereniya parametrov elektrycheskyh cepey. - M.: Energoatomizdat, 1997.
- [5] Dobrovinskiy I.R., Bondarenko L.N., Blinov A.V. Povysheniye tochnosti izmereniy parametrov dvuhpolyusnykov. - Izmeritelnaya tehnika. - 2003, №7, c.49-53.
- [6] Modern impedance measurement techniques. Bate Alan. Electron. World, 2003, 109, №1803, c.52-59.
- [7] PC-based devices for immitance control of multidimensional objects. Pohodylo E., Stolyarchuk P., Chyrka M. IEEE Trans. Instrum. and Meas. 2002, 51, №5, c.1132-1135.
- [8] Teoreticheskiye osnovy postroyeniya i tehniceskaya realizaciya mnogofunkcyonalnyh preobrazovatelye kompleksnogo soprotivleniya na baze adaptivnogo podhoda. Avtoref. dis. na soisk. uch. stepeni dokt. tehn. nauk. Agamalov J.R. In-t problem upr. RAN, Moskva, 2003, 46 c.
- [9] Strukturno-algorytmicheskiye metody synteza sredstv invariantnogo izmereniya parametrov elektrycheskiy cepey. Avtoref. dis. na soisk. uch. stepeni dokt. tehn. nauk. Svystunov B.L. Penz. gos. un-t, Penza, 2004, 47c.
- [10] Grybok M. Algorytmichni metody vymiryuvannya parametrov skalyarnykh velychyn. - Vymiryvalna tehnika ta metrologiya, 2001, №58.
- [11] Grybok M. Intelektualni metody vymiryuvannya parametrov vektornykh velychyn, Visnyk DU „Lvivska politehnika”, „Komp'yuterni systemy proektuvannya. Teoriya i praktyka”, 2001, №415.
- [12] Grybok M. Vymiryuvannya parametrov dvokomponentnykh kompleksnykh oporiv metodom zmishchennya systemy koordynat po skladovykh oporu i providnosti. // Visnyk DU „Lvivska politehnika”, 2002, №445.
- [13] Grybok M. Vymiryuvannya parametrov dvokomponentnykh kompleksnykh oporiv metodom zmishchennya systemy koordynat po skladovykh naprugy i strumu. // Vymiryvalna tehnika ta metrologiya, 2002, №59.
- [14] Grybok M. Vymiryuvannya parametrov paralelnykh RLC-shem metodom zmishchennya systemy koordynat po strumu. Visnyk DU „Lvivska politehnika”, „Avtomatyka, vymiryuvannya ta keruvannya”, 2006, №551.
- [15] Grybok M. Vymiryuvannya parametrov trykomponentnykh kompleksnykh oporiv metodom zmishchennya systemy koordynat. Dodatok do naukovy-tehnichnogo zhurnalu VAK Ukrayiny „Standartyzaciya, sertyfikaciya, yakistj” – Harkiv, 2006.